

Cover Sheet for

ENVIRONMENTAL CHEMISTRY METHOD

Pesticide Name: Pyrethiobac-Sodium

MRID #: 433172-14

Matrix: Water

Analysis: HPLC/UV

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433172-14

Study Title

**ANALYTICAL METHOD FOR THE DETERMINATION OF
KIH-2031 (DPX-PE350) IN WATER USING
COLUMN-SWITCHING LIQUID CHROMATOGRAPHY**

Data Requirement

U.S. EPA Pesticide Assessment Guidelines
Subdivision N, 166, not required at this time

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Date Study Completed

July 19, 1994

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Laboratory Project ID

AMR 2746-93

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**ANALYTICAL METHOD FOR THE DETERMINATION OF
KIH-2031 (DPX-PE350) IN WATER USING
COLUMN-SWITCHING LIQUID CHROMATOGRAPHY**

Sheldon R. Sumpter and Brock A. Peterson

ABSTRACT

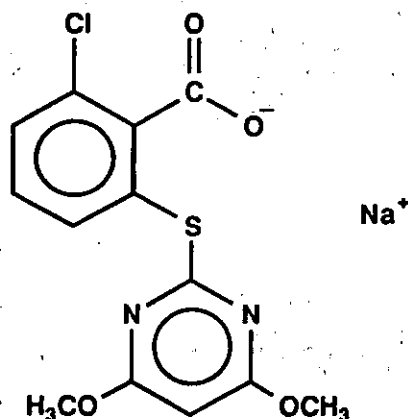
An analytical method was developed and is described for the determination of KIH-2031 (sodium 2-chloro-6-[(4,6-dimethoxypyrimidin-2-yl)thio]benzoate, DPX-PE350) extracted from water. DPX-PE350 is extracted from 200 mL of water using a graphitized carbon, solid-phase extraction cartridge. The instrumental method is based on the use of column-switching HPLC with UV absorbance detection at 254 nm. The method detection limit for DPX-PE350 in water is 0.051 ppb (0.051 ng/mL).

The chromatographic separation requires one high-pressure switching valve which places two analytical columns in series. The first column is used as a "clean-up" column from which DPX-PE350 is transferred to the second column. The transfer begins just before the mean elution time of DPX-PE350 standards. After transfer of the analyte to the second column, the valve is switched to allow flow through the first column only to allow elution (clean-up) of other matrix components. Following clean-up, the valve is switched to allow flow to pass through the both columns and the analytical separation of DPX-PE350 is performed.

The average recovery (\pm standard deviation), as determined using HPLC/UV, for 23 water samples was $93 \pm 12\%$ giving a relative standard deviation of 13% for water samples fortified at the 0.1- to 50-ppb levels. The validity of this method was confirmed by standard ^{14}C methodology; extraction efficiency recoveries ranged from 84 to 102% and the average recovery (\pm standard deviation) for 7 samples was $96 \pm 6\%$ giving a relative standard deviation of 6%. This method meets U.S. EPA Subdivision N, 166, Pesticide Assessment Guideline criteria.

INTRODUCTION

This analytical method was developed to satisfy U.S. EPA registration requirements for Staple® Herbicide. This method determines residues of DPX-PE350 extracted from water. Staple® Herbicide is used to control broadleaf weeds in cotton. The formulated product contains 85% by weight KIH-2031 (sodium 2-chloro-6-[(4,6-dimethoxypyrimidin-2-yl)thio]benzoate, DPX-PE350). KIH-2031 is referred to as DPX-PE350 in this report. The chemical structure for DPX-PE350 is shown below:



DPX-PE350

Bates (see Reference 1) has determined the following physico-chemical properties for DPX-PE350:

Melting Point:	233.8-234.2°C
Solubility:	
Water	728 g/L
Methanol	270 g/L
Acetone	812 mg/L
Acetonitrile:	347 mg/L
Partition Coefficient, n-octanol/pH 7 water:	0.14
Dissociation Constant, pK _a	2.34

DPX-PE350 was extracted from 200 mL of fortified water by passing the water through a graphitized carbon solid-phase extraction cartridge. After rinsing the cartridge with solutions that selectively removed interfering matrix, DPX-PE350 was eluted from the cartridge.

For HPLC analysis, the following procedure was used. A 0.2-mL sample was injected on a Zorbax® SB-CN column. A valve was switched at a window of transfer that was determined from the average elution time of DPX-PE350 standards eluting off the SB-CN column. This procedure transferred DPX-PE350 from Column I to a second column, a Zorbax® SB-C18 column. After DPX-PE350 was transferred to the second column, the valve was switched to allow the mobile phase to flow through the first column only which allowed elution (clean-up) of other matrix components. Following solvent clean-up, the valve is switched to allow mobile phase to flow through both columns. The analytical separation of DPX-PE350 was performed on the second column with both columns in series.

EXPERIMENTAL

Equipment

Equivalent equipment may be substituted unless otherwise indicated.

Liquid Chromatograph

HPLC System, Waters (Millipore, Inc., Milford, Mass.):

- Pump control module, Waters;
- Three pumps, Waters, Model 510; Note: a three pump, high-pressure mixing HPLC system is not required for this method; a single pump, low-pressure mixing HPLC system will work too.
- Photo diode array detector, Waters, Model 996;
- Raytest, Ramona 5LS radioisotope detector with 370- μ L flow cell volume, glass scintillator (Raytest USA Inc., Pittsburgh, Penn.)
- Millennium 2010 v2.00 software run on a NEC 486/33 computer, Waters;
- Auto injector, Waters, Model 717 equipped with a 2.5-mL syringe;
- Temperature control module, Waters;
- Column heater module, Waters; and
- Six-port switching valve, (Valco Inst., Houston, Tex., Model E60, #EC6W)

HPLC Columns

- Pre-Column 1 DuPont Zorbax® SB-CN 4.0 x 12.5 mm, 5- μ Reliance Cartridge Guard Column, #820674-916 and column end-fittings, #820529-901 (MAC-MOD Analytical Inc., Chadds Ford, Pa.), **do not substitute.**
- Column 1 DuPont Zorbax® SB-CN 4.6 x 150 mm, 5- μ analytical column, #883975-905 (MAC-MOD Analytical Inc., Chadds Ford, Pa.), **do not substitute.**
- Column 2 DuPont Zorbax® SB-C₁₈ 4.6 x 250 mm, 5- μ analytical column, #880975-902 (MAC-MOD Analytical Inc., Chadds Ford, Pa.), **do not substitute.**

Solid-Phase Extraction Apparatus

Solid-phase extraction manifold, #5-7044M, with disposable Teflon® solvent guides, #5-7059 (Supelco, Bellefonte, Pa.).

Solid-Phase Extraction Cartridges and Adapters

6-mL Envi-Carb tubes #5-7094M (Supelco, Bellefonte, Penn.), **do not substitute.** 75-mL reservoir #1213-1030 and adapter #1213-1003 (Varian Sample Preparation Products, San Fernando, Calif.).

Evaporator

N-Evap® Model 111 laboratory sample evaporator/nitrogen manifold fitted with Teflon®-coated needles (Organomation Associates, South Berlin, Mass.). Unit is attached to a dry, clean nitrogen source.

Mobile Phase Filters and Vacuum Filter Apparatus

Use 0.45- μ m pore, Cat. No. HATF 047 00, Type HA filters for pH 3, 30 mM potassium phosphate buffer. Use 0.5- μ m pore, Cat. No. FHUP 047 00, Type FH filters for acetonitrile. The Millipore vacuum filter apparatus used to filter and degas mobile phases consists of a glass filter holder, #XX1004700, a ground glass base with stopper, #XX1004702, a funnel cover, #XX2504754, and a 1-L filter flask, #XX1004705 (Millipore, Inc., Milford, Mass.).

Sample Water Filters

For sample water that has not been filtered, use Whatman # 3 Filter # 28456-065 (VWR Scientific Co., Bridgeport, N.J.). For water samples that have been extracted and cleaned up, use Millipore SJHVL04NS, 0.45- μ m Type HV filters (Millipore, Inc., Milford, Mass.).

Syringes

2.5-mL disposable plastic syringe, Part No. Z11685-8 (Aldrich Chemical Co., Milwaukee, Wis.); Hamilton 100- and 500- μ L syringes, #80600 and #80800, respectively (Hamilton, Reno, Nev.).

pH Meter

Beckman Model PHI 11 (Beckman Instruments, Inc., Fullerton, Calif.).

Balances

Mettler A163 analytical balance (Mettler Instrument Corp., Hightstown, N.J.).

Ultrasonic Bath

Branson Model 2200 ultrasonic bath (VWR Scientific Co., Bridgeport, N.J.).

Mixer

Vortex Genie 2 (VWR Scientific Co., Bridgeport, N.J.).

Pipettes

Pipetman #P-1000 adjustable pipette and EDP-Plus pipette #EP-10ML (Rainin, Emeryville, Calif.).

Graduated Cylinders

Kimax 10-, 100-, 250-, 500-, and 1000-mL graduated cylinders, #24713-503, #24713-111, #24713-144, #24713-166, #24713-188, respectively (VWR Scientific Co., Bridgeport, N.J.).

Volumetric Flasks

Pyrex 25-, 100-, 200-, 500-, 1000-mL volumetric flasks, #29619-212, #29619-234, #29619-245, #29619-267, and #29619-278, respectively (VWR Scientific Co., Bridgeport, N.J.).

Water Filtering Apparatus

Porcelain Buchner funnel, 100-mm diameter, #30310-120 (VWR Scientific Co., Bridgeport, N.J.) with a Neoprene No. 7 stopper, #59589-256 (VWR Scientific Co., Bridgeport, N.J.), and a 500-mL filter flask, # 29415-100 (VWR Scientific Co., Bridgeport, N.J.).

Autosampler Vials

Waters 4-mL vials #72710 with low volume glass inserts and springs #72704 (Millipore, Milford, Mass.).

Pyrex Centrifuge Vial

Pyrex, conical, graduated, 15-mL centrifuge vial with stopper, #21048-027 (VWR Scientific Co., Bridgeport, N.J.).

(Klein
45776
60501)
4/14/96
Pr. imp. ph.

Reagents and Standards

Equivalent reagents may be substituted for those listed below. To determine if substituted reagent impurities interfere with DPX-PE350, appropriate amounts of the solvents should be injected into the HPLC using the chromatographic conditions specified in this report for DPX-PE350.

Water

Deionized water passed through a Milli-Q® UV Plus water purification system #ZD60 115 UV (Millipore, Bedford, Mass.).

Potassium Phosphate, Monobasic, Crystal (KH₂PO₄)

Baker analyzed potassium phosphate, monobasic, crystal reagent, #3246-05 (J. T. Baker, Phillipsburg, N.J.).

Dichloromethane (DCM)

EM Omni Solv®, residue grade dichloromethane, #DX0831-1 (EM Science, Gibbstown, N.J.). **Warning** - dichloromethane is a suspected carcinogen. Use in a fume hood.

Methanol (MeOH)

EM Omni Solv®, HPLC-grade methanol, #MX0488-1 (EM Science, Gibbstown, N.J.).

Acetonitrile (ACN)

EM Omni Solv®, HPLC-grade acetonitrile, #AX0142-1 (EM Science, Gibbstown, N.J.).

Acetone

EM Omni Solv®, HPLC-grade acetone, #AX0116-1 (EM Science, Gibbstown, N.J.).

Ammonium Carbonate [(NH₄)₂CO₃]

Baker Analyzed Reagent, reagent-grade ammonium carbonate #0642-01 (J. T. Baker, Inc., Phillipsburg, N.J.).

Phosphoric Acid (H₃PO₄)

Baker Analyzed Reagent, reagent-grade, concentrated phosphoric acid, #0260-01 (J. T. Baker, Inc., Phillipsburg, N.J.).

Hydrochloric Acid (HCl)

Reagent-grade 12 M hydrochloric acid, #9535-01 (J. T. Baker, Inc., Phillipsburg, N.J.).

Sodium Azide, Practical

Baker sodium azide, practical, #3V015-05 (J. T. Baker, Inc., Phillipsburg, N.J.). See warning in *Preparation of Solutions* section of this report.

Formic Acid

EM Suprapur® formic acid, #11670-1 (EM Science, Gibbstown, N.J.).

Acetic Acid

Baker Analyzed glacial acetic acid, #9524-00 (J. T. Baker, Inc., Phillipsburg, N.J.).

DPX-PE350

Reference substance used for HPLC analysis: analytical standard grade DPX-PE350, Lot #4, 98.7% pure (prepared by Kumiai/Ihara Chemical Co. for DuPont Agricultural Products, Global Technology Division, E. I. du Pont de Nemours and Company).

Radioactive DPX-PE350, NEN #2764-067, HOTC #370, 99.0% pure. Specific Activity: 70.210 $\mu\text{Ci}/\text{mg}$. Radiolabel location: pyrimidine-2- ^{14}C .

Water Samples

This method was developed and validated using water from the following sources:

Wilson Run, New Castle County, Delaware,

Brandywine River, New Castle County, Delaware, and

Groundwater from well in Edgecombe County, North Carolina.

Preparation of SolutionspH 3. 30 mM Potassium Phosphate Buffer

Add 7.21 g KH_2PO_4 , 0.2 g sodium azide (optional, see warning below), and 0.40 mL of 85% H_3PO_4 to 2.0 L of fresh HPLC-grade water in a beaker and dissolve the salt using a magnetic stirrer. Adjust the pH to 3.00 with 85% H_3PO_4 if the pH is higher than pH 3.00 or with 50% KOH if the pH is lower than pH 3.00. This solution should be prepared fresh weekly and should be filtered daily before use with a 0.45- μm pore filter.

Warning - Sodium azide is combustible, shock sensitive, and can explode. Sodium azide is a health hazard and should not be swallowed, inhaled, or absorbed through the skin, and should be disposed of properly. *Potassium phosphate buffers with sodium azide should not be put down the drain.* Read the material safety data sheet for this compound before use. Sodium azide is used in this method as a growth inhibitor for bacteria. It does not need to be used if the phosphate buffer is filtered daily, prepared fresh weekly, and stored in the dark. If sodium azide is not used, the solvent lines from the reservoir to the pump should be purged with acetonitrile weekly to control bacterial growth.

0.01 M Ammonium Carbonate

Dissolve 0.78 g of $(\text{NH}_4)_2\text{CO}_3$ in about 800-mL distilled water and dilute to 1.00 L in a volumetric flask. This solution should be made weekly.

0.1 M Hydrochloric Acid

Pipet 8.33 mL 12 M HCl into 1-L volumetric flask and bring to volume with Milli-Q® water. This solution should be made weekly.

90% Dichloromethane/10% Methanol

With 1000-mL graduated cylinder, measure 900 mL of dichloromethane and add to 1-L volumetric flask. With 100-mL graduated cylinder, measure 100 mL of methanol and add to the 1-L flask. Do not adjust the volume to 1-L mark. This solution should be made weekly.

0.1 M Formic Acid in 90/10 DCM/MeOH

Pipet 0.755 mL of EM Science Suprapur® formic acid into 200-mL volumetric flask. Bring to volume with 90% DCM/10% MeOH. This solution should be made weekly.

0.004 M Acetic Acid in 90/10 DCM/MeOH

Pipet 23 μL of Baker glacial acetic acid into a 100-mL volumetric flask and bring to volume with 90/10 DCM/MeOH. A new solution should be prepared weekly.

0.10 M Acetic Acid

Pipet 2.85 mL of Baker glacial acetic acid into 500-mL volumetric flask and bring to volume with Milli-Q® water. A new solution should be prepared weekly.

20% Acetonitrile/ 80% 0.10 M Acetic Acid

With 100-mL graduated cylinder, measure 100 mL of acetonitrile and add to a 500-mL volumetric flask. With a 500-mL graduated cylinder, measure 400 mL of 0.1 M acetic acid into the 500-mL volumetric flask. Do not adjust the volume to the 500-mL mark. Shake vigorously to mix. A new solution should be prepared weekly.

HPLC Eluents

Eluent A: 100% acetonitrile;

Eluent B: 100% pH 3, 30 mM phosphate buffer;

Eluent C: 100% Milli-Q® water.

Mobile phases should be thoroughly degassed daily. Solvents are degassed by filtering them through a Millipore® vacuum filtering apparatus while sonicating the apparatus. If a low-pressure mixing HPLC is used, mobile phases should be sparged at 30 mL/min.

Standards

Use Class A volumetric flasks when preparing standard solutions.

Stock Standard Solution

Prepare a standard stock solution by accurately weighing 10 mg of DPX-PE350 into a 100-mL volumetric flask on an analytical balance. *Record the weight of the standard used to make the stock solution.* Dissolve the standard in approximately 75 mL of HPLC-grade methanol. After dissolving, bring the solution to 100.00-mL volume using HPLC-grade methanol. This standard solution is stable for approximately 6 months when stored at approximately 4°C. The concentration of this solution is 100-µg/mL DPX-PE350 in methanol.

Intermediate Standard Solution

Prepare an intermediate standard solution by pipetting 1.00 mL of the 100-µg/mL DPX-PE350 stock standard into a 100-mL volumetric flask. Bring to volume using HPLC-grade methanol. The concentration of this solution is 1-µg/mL DPX-PE350 in methanol. This standard solution is stable for approximately 6 months stored at approximately 4°C.

Chromatographic Standard Solutions

The 1-µg/mL DPX-PE350 in methanol fortification solution is used to prepare the chromatographic standards. Prepare the standards by pipetting volumes of the 1-µg/mL intermediate standard solution of DPX-PE350 into a 25-mL volumetric flask, as shown in the following table:

Desired Standard Concentration ($\mu\text{g/mL}$)	Volume of 1 $\mu\text{g/mL}$ Standard Required (mL)
0.500	12.5
0.250	6.25
0.200	5.00
0.100	2.50
0.0500	1.25
0.0250	0.625
0.0100	0.250
0.00500	0.125
0.00100	0.0250

Evaporate the methanol (to dryness) in each of the 25-mL volumetric flasks the using an N-Evap. Add 20% acetonitrile/80% 0.10 M acetic acid to the volumetric flasks and dilute to 25.00 mL. These standard solutions are stable for approximately 6 months at 40°C, but they should be prepared fresh weekly and stored at 4°C.

Fortification Standard Solutions

In most circumstances, the 1- $\mu\text{g/mL}$ intermediate standard solution should be used for fortifications of samples analyzed by HPLC.

Analytical Procedure

Storage and Preparation of Water Samples

Water samples are stored at 4°C or frozen until analysis. Samples should be warmed to room temperature and thoroughly mixed before use one day before they are extracted.

Water Fortification Procedure

To fortify filtered water samples, add 200 mL of water to a 250-mL graduated cylinder. Add to the 200-mL water sample the required volume of fortification standard to achieve the appropriate fortification level (see table below). For HPLC method validation and quality control, samples can be fortified using the following table:

<u>Volume of Standard</u>	<u>Standard Conc.</u>	<u>Sample Volume</u>	<u>Fortification Level</u>
<u>(mL)</u>	<u>($\mu\text{g/mL}$)</u>	<u>(mL)</u>	<u>(ppb)</u>
0.020	1.0	200	0.10
0.040	1.0	200	0.20
0.100	1.0	200	0.500
0.200	1.0	200	1.00
0.0100	100	200	5.00
0.0200	100	200	10.0
0.1000	100	200	50.0

Extraction Procedure

At a minimum, a sample set should consist of an unfortified and a fortified water sample. A sample set of six water samples, including unfortified and fortified samples, should be run. One, or more water samples may be extracted and cleaned up by doing the following:

1. Allow frozen or chilled water sample to come to room temperature. This step should be started the day before the extraction is to be done.
2. Filter each water sample through a 9-cm Whatman No. 3 filter paper using a clean Buchner funnel.
3. Using a clean, 250-mL graduated cylinder labeled with appropriate sample identification, measure 200 mL of sample water. *Record volume for sample.*
4. Fortify water sample (if applicable) by adding "X" μL of the 1- $\mu\text{g/mL}$ DPX-PE350 intermediate standard solution to the water (see the table on the previous page for the amount added to the water). *Record the volume and concentration of the fortification standard used.*
5. Using a clean, 10-mL graduated cylinder, add 5-mL (± 1 mL) of 0.10 M formic acid in 90% DCM/10% MeOH to an Envi-Carb tube installed on the solid phase vacuum manifold. Pull the solution through the Envi-Carb tube at a 3-5 mL/min flow rate. Pull air through the tube for 5 min after the solution has passed through.
6. Rinse the 10-mL graduate used in Step 5 with HPLC grade acetone and discard the rinse to waste. *This graduated cylinder should be rinsed with acetone before it is used to measure a new rinse or elution solution for each of the following steps.*

7. Using the 10-mL graduate, add 7 mL (± 1 mL) of 0.1 M HCl to the Envi-Carb tube. Pull the solution through the Envi-Carb tube at a 3-5 mL/min flow rate. Pull air through tube for 2-3 seconds after 0.1 M HCl has passed through the packing.
8. Using the 10-mL graduate, add 5 mL (± 1 mL) of Milli-Q® water to the Envi-Carb tube and pull 2-3 mL through the packing at a flow rate of 3-5 mL/min.
9. Label the Envi-Carb tube with appropriate sample identification.
10. Attach a clean, Varian 1213-1030, 75-mL reservoir to the Envi-Carb tube using a Varian 1213-1003 adapter and add the 200-mL water sample to the reservoir. Pull the water sample through the Envi-Carb tube at a 3-5 mL/min flow rate. When the graduated cylinder is empty of sample water, rinse the graduate with approximately 10-mL Milli-Q® water and add to the reservoir. After all of the sample has passed through the reservoir, but not through the Envi-Carb tube, rinse the 75-mL reservoir with approximately 5 mL Milli-Q® water. Pull the final amount of water through the Envi-Carb packing until the first air bubble appears below the packing. Then, stop the flow and disconnect the reservoir and adapter from the Envi-Carb tube. Water pulled through the Envi-Carb tube goes to waste.
11. Using the 10-mL graduate, add 7 mL (± 0.1 mL) of 0.01 M ammonium carbonate to the Envi-Carb tube packing. Pull the solution through the packing at a 3-5 mL/min flow rate. Pull air through the packing for 1 min after the ammonium carbonate solution passes through the Envi-Carb tube. Solution pulled through the Envi-Carb tube goes to waste.
12. Using an autopipet, add 1.0 mL of methanol to the Envi-Carb tube. Pull the methanol through the packing at a flow rate similar to that in Step 11. Pull air through the packing for 5 min, after methanol passes through the Envi-Carb tube. Solution pulled through the Envi-Carb tube goes to waste.
13. Using the 10-mL graduate, add 6 mL (± 0.1 mL) of 4 mM acetic acid in 90% DCM/10% MeOH to the Envi-Carb tube. Pull the solution through the packing at a 3-5 mL/min flow rate. Pull air through the packing for 10-20 seconds after the solution passes through the Envi-Carb tube. Solution pulled through the Envi-Carb tube goes to waste.

14. Using the 10-mL graduate, add 5 mL (± 0.1 mL) of 0.10 M formic acid in 90% DCM/10% MeOH to the Envi-Carb tube. Pass the solution through the tube at a 3-5 mL/min flow rate, collecting the solution that passes through in a clean, appropriately labeled Pyrex, graduated, conical, centrifuge vial.
15. Evaporate the DCM/MeOH/formic acid solution to dryness in an N-Evap with the water bath at 40°C using nitrogen gas.
16. The sample may be stored in a capped, centrifuge vial, in a refrigerator at approximately 4°C for at least two weeks before analysis.
17. Bring sample up in 20% acetonitrile/80% 0.1 M acetic acid to a final volume of 1.00 mL. *Record the final volume used.* Vortex mix sample for 10 seconds, sonicate for 2 minutes, and vortex mix for 10 seconds. Filter sample using the Millipore SJHVL04NS HV, 0.45- μ m filter connected to a plastic disposable syringe.
18. Analyze the sample using column-switching HPLC.

When possible, samples should be run from low to high concentration of DPX-PE350. For samples having unknown concentrations, sample vials should be loaded on an auto sampler in a nonsystematic fashion. Samples should be intermixed with standards (bracket every 2-3 samples with a standard). When possible, standard concentrations should be selected to bracket expected DPX-PE350 levels in the samples analyzed. A sample response should be within the responses of two standards analyzed in a sample set of water samples. A standard should be the first and last sample analyzed in each sample set.

At a minimum, a sample set should consist of an unfortified and a fortified water sample and six standards having concentrations that bracket the fortification level. A sample set of six water samples, including unfortified and fortified samples, should be run.

Before a set of chromatographic standards are used to determine the amount of DPX-PE350 in a water sample, they should be analyzed using HPLC to assure that they have been prepared properly. A 0.200-mL injection volume on the SB-CN column of each standard should generate a linear response from the UV detector set at 254 nm. Standards prepared from week to week should generate similar response factors. A six-point calibration curve should be used with standard concentrations in the range of the samples when possible.

Liquid Chromatography

The HPLC system components have already been described in the **Equipment** section of this report. Representative conditions for the HPLC method are shown in the following table:

Wavelength	254 nm
Column Temperature	40.0°C
Injection Volume	0.200 mL
HPLC Dwell Volume	4.5 mL
Mobile Phase A	100% ACN
Mobile Phase B	100% pH 3, 30 mM phosphate buffer
Mobile Phase C	100% Milli-Q® water

Multi-dimensional HPLC is used with the columns conditioned using the above procedure. (For a review of multi-dimensional, column-switching HPLC, see References 2 and 3.) A diagram of the column-switching valve arrangement is shown in Figure 1, where Column I and Column II are Zorbax® SB-CN and Zorbax® SB-C18 analytical columns, respectively. Tables I.A and I.B describe typical pump and column-switching timing sequences.

The following discussion describes the column-switching routine and how the technique is performed.

With the switching valve in Position 1, the effluent from Column I leaves the column through the switching valve, enters a bypass loop, flows back through the switching valve, and then flows to the detector. With the valve in Position 2, the effluent from Column I goes (via the valve) to Column II, back to the valve, and then to the detector. *All tubing connecting the switching valve to the analytical columns and detector should be 0.005-inch internal diameter tubing to minimize dead volume.* Either stainless steel or PEEK tubing can be used.

Before injection, the valve is put in Position 1, so that the HPLC flow bypasses Column II. Pump 20% ACN/80% pH 3, 30 mM potassium phosphate buffer at 1.0 mL/min through Column I only. A linear gradient is run from 20 to 43% acetonitrile in five minutes. When DPX-PE350 starts to elute from Column I, the valve is switched to Position 2 in order to trap the peak on Column II. After the peak is collected at the head of Column II, the valve is switched back to Position 1.

The switching valve time (the "window of transfer", or "time window", or "cut window") is determined immediately before the analysis of a sample set is started. Determine the time window by injecting a DPX-PE350 standard three times (a 250-ng/mL DPX-PE350 standard can be used) on Column I only. Run a

mobile phase linear gradient from 20 to 43% acetonitrile in five minutes at 1 mL/min for each injection. **The column temperature should be checked to confirm that the column oven is working.** Calculate the mean retention time of the three DPX-PE350 standard injections. Set the switching valve time window at ± 0.25 minutes of the mean retention time for DPX-PE350.

Typical DPX-PE350 baseline peak widths for 0.250- μ g/mL standards injected should range from 0.4 to 0.6 min, depending on the SB-CN guard and analytical columns used. The retention time (through Column I) relative standard deviation ($RSD = 100 * \text{Std. Dev.} / \text{Mean}$) for the standards injected should be no greater than 1%. In some circumstances, depending on the HPLC instrumentation, premixed solvents may be required to generate reproducible retention times.

When the mean retention time is being determined for standards eluting from Column I, the peak shape of DPX-PE350 should be observed. If the peak tails badly or recoveries are poor, the pre-column and/or analytical column may need to be replaced before further analysis.

If new analytical columns are to be used or if columns have not been used for a day or more, they should be conditioned using the following procedure:

A 100% ACN mobile phase is passed through both columns at 1 mL/min. The baseline is monitored during this process until a stable baseline is observed.

Next, the columns are conditioned in the mobile phases that are used for the sample analysis. Column II (the SB-C18 column) is conditioned with 43% acetonitrile/57% pH 3, 30 mM potassium phosphate buffer for 30 min at 1 mL/min by passing the mobile phase through both columns. Then, the valve is switched to Position 1 and Column I is conditioned with 20% acetonitrile/80% pH 3, 30 mM potassium phosphate buffer for 5 min at 2 mL/min.

After conditioning the columns, the auto sampler is purged with 20% acetonitrile/80% pH 3, 30 mM potassium phosphate buffer for 3 min at 1 mL/min.

Injection of several water samples into the guard (pre-column) and SB-CN analytical column may affect the peak shape and retention time of DPX-PE350. If peak tailing is observed when standards elute from the SB-CN column, the SB-CN guard column (pre-column) is replaced. If peak

tailing continues after changing the guard column, then the analytical column should be replaced.

When a pre-column is replaced, it is purged with 100% ACN for 5 min at 2 mL/min before connecting the pre-column to the analytical column. After conditioning the pre-column, the pre-column and SB-CN analytical column are purged with 100% ACN for 5 min at 2 mL/min and the column oven chamber is reequilibrated to 40.0°C. Then, the pre-column and analytical column are conditioned with 20% ACN/80% pH 3, 30 mM potassium phosphate buffer for 5 min at 2 mL/min.

The following column-switching routine is used to separate DPX-PE350 from coextracted compounds (see Figure 1 and Tables I.A and I.B). A 0.20-mL sample is injected into Column I. The initial mobile-phase concentration is 20% ACN/80% pH 3, 30 mM potassium phosphate buffer at a flow rate of 1 mL/min. The solvent delay time is about 1.8 min on Column I.

At the beginning of the time window (the time window is approximately 10 minutes from the point of injection), the valve is switched from Position 1 to Position 2 and DPX-PE350 is transferred to Column II. At the end of the time window, the valve is switched from Position 2 to Position 1. The mobile phase gradient is allowed to finish on Column I and after completion of the gradient, Column I is maintained at 43% acetonitrile/57% pH 3, 30 mM potassium phosphate buffer to clean out the column.

After cleaning Column I, the valve is switched to Position 2, to elute DPX-PE350 from Column II using the 43% ACN/57% pH 3, 30 mM potassium phosphate buffer mobile phase. DPX-PE350 elutes from Column II at a retention time of about 24 min from the start of the run. After DPX-PE350 elutes from Column II, 75% ACN/25% Milli-Q® water is passed through both columns at 1 mL/min for 15 min to more rigorously clean off Column I and to clean off Column II.

After cleaning off the columns, they are conditioned at their initial conditions. To accomplish this, a 43% ACN/57% pH 3, 30 mM potassium phosphate buffer is passed through both columns at 1.3 mL/min to set Column II at the conditions required for the next separation. Then, the valve is switched to Position 1 and 20% ACN/80% pH 3, 30 mM potassium phosphate buffer is passed through Column I only at 2 mL/min for 5 min. The flow rate is reduced to 1 mL/min and the system is allowed to run for another one minute. At this time, Column I and Column II are both ready for the next injection.

8.22
Table I.B
75-20-25
5 minutes

Calculations

Trace levels of DPX-PE350 found in water samples are determined using the procedure discussed below.

Generate a peak height (μV) vs. known concentration (ng/mL) plot of external DPX-PE350 standards injected. Generate a linear least squares fit calibration curve for the data. The equation for the line is $y = mx + b$, where y is the peak height, x is the concentration of DPX-PE350 (ng/mL), m is the slope of the line ($\mu\text{V}/\text{ng/mL}$), and b is the y , (ordinate) intercept (μV). The solution to the equation for this line gives the concentration of DPX-PE350 found (ng/mL) corresponding to the experimentally observed peak height (μV).

Using the experimentally observed peak height to determine the concentration found from the calibration curve, the ppb DPX-PE350 found in a water sample is calculated.

ppb found

The parts per billion (ppb) DPX-PE350 found in water samples is given by:

$$\text{ppb Found} = \frac{(1000 \text{ ng} / \mu\text{g})(\text{Conc. Found, } \mu\text{g} / \text{mL})(\text{Final Vol., mL})}{\text{Sample Volume, mL}}$$

where Conc. Found is the concentration found and Final Vol. is the final volume of the sample.

Fortification Level (ppb)

The fortification level (ppb) is the amount of DPX-PE350 added to 200 mL of water sample which is given by:

$$\text{Fort. Level, ppb} = \frac{(1000 \text{ ng} / \mu\text{g})(\text{VFS, mL})(\text{CFS, mL})}{\text{Sample Volume, mL}}$$

where Fort. Level is the fortification level, VFS is the volume of the fortification standard that was added to the water, and CFS is the concentration of the fortification standard.

Recovery

The recovery is given by

$$\% \text{ Recovery} = 100 \left(\frac{\text{ppb found}}{\text{Fortification level, ppb}} \right)$$

Sample Calculations

Using the data for NC 100ppt2/6-23, North Carolina, water sample that was extracted June 23, 1994 (see Data Sheet 6 in Appendix I), the following sample calculations were prepared:

$$\text{ppb Found} = \frac{(1000 \text{ ng} / \mu\text{g})(0.0200 \mu\text{g} / \text{mL})(1.00 \text{ mL})}{200 \text{ mL}} = 0.100 \text{ ppb}$$

$$\text{Fort. Level} = \frac{(1000 \text{ ng} / \mu\text{g})(0.0200 \text{ mL})(1.00 \mu\text{g} / \text{mL})}{200 \text{ mL}} = 0.100 \text{ ppb}$$

$$\% \text{ Recovery} = 100 \left(\frac{0.100 \mu\text{g} / \text{mL}}{0.100 \mu\text{g} / \text{mL}} \right) = 100$$

Cleaning Procedures

All glassware can be cleaned by means of any approach that is consistent with trace organic analysis.

Generally, the following is done. Glass items are initially rinsed with acetone (technical grade), followed by a thorough scrubbing with an aqueous soap solution (prepared in tap water). Then, glassware is rinsed with tap water, followed by another acetone rinse.

RESULTS AND DISCUSSIONDetector Response

DPX-PE350 absorbs ultraviolet light at 254 nm. This wavelength is used in this method. The UV detector response at 254 nm was linear over the range of standards analyzed, 10-250 ng/mL (see Figure 2).

Sample Chromatograms

Figure 3 shows a chromatogram from a 250-ng/mL DPX-PE350 standard using the column-switching method described in the **EXPERIMENTAL** section of this report. This figure has the cut time (i.e., time window) and column clean-up and analysis times labeled. Figures 4-8 show typical chromatograms resulting from 0.200-mL injections of standards, and cleaned-up unfortified and fortified water samples. The chromatograms for the unfortified samples demonstrate that the extraction and clean-up method is effective; there are no interfering peaks detected for the Wilson Run stream, Brandywine River, and North Carolina groundwater samples.

Recoveries by HPLC/UV Analysis

After extraction, water samples fortified with DPX-PE350 were analyzed by HPLC using UV detection. The data are found in Appendix I (Data Sheets 1-7).

Tables II and III summarize recovery data obtained for water fortified with DPX-PE350. Recoveries were acceptable over the fortification range employed (0.1-50 ppb). The average recovery (\pm standard deviation) for all of the fortified samples at all levels is $93 \pm 12\%$; the RSD is 13%. Recoveries for the 23 samples analyzed range from 65 to 113%.

Determination of MDL

After examining method validation runs of unfortified and fortified water samples using this method, the method detection limit, MDL, was estimated to be 0.100-ppb DPX-PE350 in water. This estimate is the fortification level that generates a 10:1 signal-to-noise ratio compared to the measured average signal-to-noise at DPX-PE350's retention time for unfortified water samples. Table IV shows peak heights at the retention time of DPX-PE350 for fourteen unfortified samples. The mean noise is calculated to be 26 μ V. A water sample generating a 260- μ V signal should have approximately 0.100-ppb DPX-PE350.

Eight 200-mL water samples were fortified at the estimated MDL of 0.100 ppb to calculate the actual MDL and the 95% confidence limits. Water samples from three different sources were used: Brandywine River (BW) water; Wilson Run (WR) stream water; and North Carolina (NC) groundwater. The following data were obtained:

Sample I.D.	% Recovery	ppb Found
NC 100ppt(1) 6/23	100	0.100
NC 100ppt(2) 6/23	115	0.115
WR 100ppt(1) 6/23	100	0.100
WR 100ppt(2) 6/23	75	0.075
NC 100ppt(1) 6/23	90	0.090
NC 100ppt(2) 6/23	105	0.105
BW 100ppt(1) 6/23	75	0.075
BW 100ppt(2) 6/23	65	0.065
Avg. \pm Std. Dev. (n=8)	91 \pm 17	0.091 \pm 0.017

Using the values from this table, the actual MDL was determined as shown below:

Fortification value	0.100 ppb
Average amount found	0.091 ppb
Standard Deviation, S_c	0.017 ppb
Number of samples, n	8
Degrees of freedom, df	7
Student's t (see Ref. 4)	3.00 (using t for $1 - \alpha = 0.99$)

$$\text{Actual MDL} = t \times S_c$$

$$= 3.00 \times 0.017 \text{ ppb}$$

$$= 0.051 \text{ ppb}$$

$$(0.01 \mu\text{g/mL in terms of concentration found})$$

The 95% confidence limits, the lower confidence limits (LCL), and upper confidence limits (UCL), were calculated as shown below:

χ^2 (P = 0.025)	16.0 (see Ref. 5)
χ^2 (P = 0.975)	1.69 (see Ref. 5)
Number of samples, n	8
Degrees of freedom, df	7

$$\text{LCL} = (\text{MDL}) \sqrt{\frac{\text{df}}{\chi^2_{(P=0.025)}}} = 0.034 \text{ ppb}$$

$$UCL = (MDL) \sqrt{\frac{df}{\chi^2_{(P = 0.975)}}} = 0.104 \text{ ppb}$$

The average (\pm standard deviation) recovery for the eight samples fortified at 0.100 ppb is $91 \pm 17\%$ with an RSD of 19%. Recoveries for the eight 200-mL water samples that were fortified, extracted, and analyzed at the 0.100-ppb level ranged from 65 to 113%. Since the estimated MDL (0.100 ppb) falls within the 95% confidence limit-range (0.034 to 0.104 ppb), the calculated MDL (0.051 ppb) is valid.

A plot of measured *vs.* known ppb for the samples analyzed by HPLC/UV is shown in Figure 9. This plot demonstrates the acceptable variability of the recoveries at the various fortification levels.

¹⁴C Method Validation

The ability of this method to extract DPX-PE350 from aged water with sediment was examined. Seven 230-mL, North Carolina, groundwater samples with sediment were fortified with 100.0 μ L of 1.18- μ g/mL [¹⁴C]DPX-PE350 standard (0.513 ppb). After allowing the fortified samples to stand from 24 to 48 hours at room temperature, they were extracted and analyzed using Steps 2 through 18, except Step 4 (fortification step), of the *Extraction Procedure* of this report.

Tables V.A and V.B list the recoveries determined from the photodiode array and the radioisotope detectors, respectively. Data for this study are found in Appendix I (see Data Sheets 8 and 9). The average recoveries \pm standard deviation, for seven samples and RSD values are $100 \pm 6\%$ (RSD = 6) and $96 \pm 6\%$ (RSD = 6) for the photodiode array and radioisotope detector data, respectively. Recoveries of the aged samples range from 94 to 109% and 84 to 102% for the data obtained using the photodiode array and radioisotope and detectors, respectively.

Results generated using the photodiode array detector and radioisotope detectors generated similar recoveries that confirm DPX-PE350 is efficiently extracted from water, aged 24 to 48 hours with sediment in the water. The high recoveries from both detectors indicate that DPX-PE350 is efficiently extracted, that it is stable through the extraction and clean-up procedures and that DPX-PE350 retention times are stable, so that quantitative analysis can be performed.

The standard curve generated by the photodiode array detector and the curve generated using the radioisotope detector are linear. Figure 10 shows a typical calibration curve generated by [^{14}C]DPX-PE350 standards using the radioisotope detector.

Figure 11 shows chromatograms from the radioisotope detector for an unfortified water sample and a fortified groundwater sample with sediment that was aged 24 hours. The peak at 12 minutes is partially due to the effect of column switching generating a response at the radioisotope detector. The change in signal due to column switching shows up later in the chromatogram from the radioisotope detector than in the chromatogram generated by the photodiode array detector (as shown in Figure 3) because the radioisotope detector is connected in-line after the diode array detector flow cell.

Timing

The time required for sample preparation and analysis is dependent on the number of samples being analyzed at one time. Frozen water samples should be thawed the day before analysis. Normally, six samples were run in a sample set, taking 3 to 4 hours for sample clean-up. HPLC automated runs required 51 minutes per sample to complete; thus, six samples required 5.1 hours to analyze.

Method Ruggedness

This method has been developed to be rugged in the extraction and analysis steps. Reagent quantity and concentration limits are specified in the extraction procedure. This assures that DPX-PE350 is retained and eluted from the Envi-Carb tubes that are used to extract the DPX-PE350 from the water and to clean up the sample. Additionally, different batches of Envi-Carb tubes were used yielding similar recoveries during the development of this method indicating that the packing has batch-to-batch reproducibility.

The method uses reversed-phase liquid chromatography with UV detection, both of which are well understood and known to be stable and reliable. This method is designed to be run on relatively simple, conventional, and commercially available HPLC equipment (auto sampler, UV detector; and one switching valve). Automation allows unattended analysis. The analytical columns that should be used are specified. Zorbax® SB-CN and SB-C18 columns are used to assure that this method works as

described and so that column stability is satisfactory at the mobile-phase pH used.

This method was tested using water samples with sediment present that were fortified with [^{14}C]DPX-PE350 and aged from 24 to 48 hours. This allowed the compound to be analyzed by both UV and radioisotope detectors after extraction and clean-up. Water fortified at 0.100 ppb and extracted using the Envi-Carb tubes generated acceptable recoveries that are similar for both detectors. The high recoveries from both detectors indicate that DPX-PE350 is efficiently extracted, that it is stable through the extraction and clean-up procedure, and that DPX-PE350 retention times are stable, so that quantitative analysis can be performed.

CONCLUSIONS

This analytical method is suitable for the measurement of DPX-PE350 extracted from water at an MDL of 0.051 ppb and it meets the criteria put forth in EPA Subdivision N, 166, Pesticide Assessment Guidelines.

ACKNOWLEDGMENTS

The authors wish to thank Edward C. Nathan for calling to our attention the use of graphitized carbon for sample clean-up. This packing has proved to be a significant improvement over other solid-phase packings that we had been using.

CERTIFICATION**ANALYTICAL METHOD FOR THE DETERMINATION OF
KIH-2031 (DPX-PE350) IN WATER USING
COLUMN-SWITCHING LIQUID CHROMATOGRAPHY**

We, the undersigned, declare that the work described in this report was performed under our supervision, and that this report provides an accurate record of the procedures and results.

Report by:

Sheldon R. Sumpter
Sheldon R. Sumpter
Study Director

19 July 1994
Date

Approved by:

Diane M. Stanley for SSG
Sidney S. Goldberg
Research Supervisor

19 July 1994
Date

Date Study Completed:

July 19, 1994

Storage Location of Records and Final Report:

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Experimental Station
Wilmington, Delaware 19880-0402

TABLES I.A AND I.B **TYPICAL HPLC PUMP AND COLUMN-SWITCHING TIMING SEQUENCE**

Table I.A. Times and values for column switching

#	Time (min)	Event	Function	Explanation
1	0.00	Event 3	On	Start run through Column I only
2	0.00	Event 4	Off	
3	10.26	Event 4	On	Start column switch; DPX-PE350 is transferred
4	10.26	Event 3	Off	
5	10.76	Event 3	On	End-column switch; Clean Column I
6	10.76	Event 4	Off	
7	15.00	Event 4	On	Start analytical separation on Column II
8	15.00	Event 3	Off	
9	44.90	Event 3	On	Set Column I to initial conditions
10	44.90	Event 4	Off	

The Waters pump control module has four external contact closure (TTL to GND) events that are activated using the Millennium 2010 software. The values of Event 3 and Event 4 (on and off times) control the Valco column switching valve: Event 3 off, Event 4 on = valve in Position 1; Event 3 on, Event 4 off = valve in Position 2. The Valco valve wiring is hooked up in the following way to the pump control module: red-coated wire to Event 3-slot 5, black-coated wire to Event 4-slot 7, and green-coated wire to Event 3-slot 6. A jumper wire connects Event 3-slot 6 to Event 4-slot 8. If both events are turned on at the same time, the valve continues to rotate; therefore, flow through the system stops.

Table I.B. Times and values of mobile-phase gradients and flow rate using the Waters Pump Control Module (PCM)

#	Time (min)	Flow (mL/min)	%A	%B	%C	Curve Type	Explanation
1	0.00	1.00	20.0	80.0	0.0	0	Start linear gradient on Column I only
2	5.00	1.00	43.0	57.0	0.0	6	Isocratic conditions to clean off Column I
3	25.00	1.00	75.0	0.0	25.0	11	Clean off Columns I and II
4	30.00	1.30	43.0	57.0	0.0	11	Set Column II at initial cond.
5	45.00	2.00	20.0	80.0	0.0	11	Set Column I at initial cond.
6	50.00	1.00	20.0	80.0	0.0	11	Set at initial flow rate

Curve Type 0 on the Waters HPLC system is the starting condition for the analysis. Curve Type 6 on the Waters HPLC system is a linear gradient that starts at the time listed on line 1 and ends at the time listed on line 2. Curve Type 11 on the Waters HPLC system is a step gradient that begins at the time listed on the line that the curve is specified. Mobile phases A, B, and C are 100% ACN and 100% pH 3, 30 mM potassium phosphate buffer, and Milli-Q® water, respectively.

TABLE II
RECOVERIES FOR FORTIFIED WATER SAMPLES

Table II. Recoveries of DPX-PE350 from water samples

<u>Sample</u>	<u>Data Sheet</u>	<u>Fortification Level (ppb)</u>	<u>ppb Found</u>	<u>% Recovery</u>
0.1 ppb				
NC 100ppt1/6-23	6	0.100	0.100	100
NC 100ppt2/6-23	6	0.100	0.113	113
WR 100ppt1/6-23	6	0.100	0.100	100
WR 100ppt2/6-23	6	0.100	0.075	75
NC 100ppt1/6-24	7	0.100	0.089	89
NC 100ppt2/6-24	7	0.100	0.106	106
BW 100ppt1/6-24	7	0.100	0.078	78
BW 100ppt2/6-24	7	0.100	0.065	65
Average:				91
Std. Dev.				17
% RSD				18
n = 8				
0.2 ppb				
WR S1/5-10	1	0.202	0.170	84
WR S2/5-10	1	0.202	0.171	85
0.5 ppb				
NC-1 S1/6-3	3	0.513	0.515	100
NC-1 S2/6-3	3	0.513	0.497	97
NC-1 FS/6-3	3	0.513	0.505	98
NC-1 S1/6-8	5	0.513	0.555	108
NC-1 S2/6-8	5	0.513	0.560	109
NC-1 S3/6-8	5	0.513	0.492	96
NC FS/6-8	5	0.513	0.482	94
Average:				100
Std. Dev.				6
% RSD				6
n = 7				
0.6 ppb				
NC S1/5-20	2	0.590	0.555	94
NC S2/5-20	2	0.590	0.560	95
10 ppb				
WR S1/6-7	4	2.02	1.95	97
WR S2/6-7	4	2.02	1.56	77
50 ppb				
WR S3/6-7	4	10.1	8.63	85
WR S4/6-7	4	10.1	8.90	88

TABLE III
RECOVERIES OF FORTIFIED WATER SAMPLES

Table III. Recoveries of DPX-PE350 extracted from 200 mL of water

<u>Sample</u>	<u>Data Sheet</u>	<u>Fortification Level (ppb)</u>	<u>ppb Found</u>	<u>% Recovery</u>
WR S1/5-10	1	0.202	0.170	84
WR S2/5-10	1	0.202	0.171	85
NC S1/5-20	2	0.590	0.555	94
NC S2/5-20	2	0.590	0.560	95
NC-1 S1/6-3	3	0.513	0.515	100
NC-1 S2/6-3	3	0.513	0.497	97
NC-1 FS/6-3	3	0.513	0.505	98
WR S1/6-7	4	10.10	9.760	97
WR S2/6-7	4	10.10	7.790	77
WR S3/6-7	4	50.50	43.16	85
WR S4/6-7	4	50.50	44.48	88
NC-1 S1/6-8	5	0.513	0.555	108
NC-1 S2/6-8	5	0.513	0.560	109
NC-1 S3/6-8	5	0.513	0.492	96
NC FS/6-8	5	0.513	0.482	94
NC 100ppt1/6-23	6	0.100	0.100	100
NC 100ppt2/6-23	6	0.100	0.113	113
WR 100ppt1/6-23	6	0.100	0.100	100
WR 100ppt2/6-23	6	0.100	0.075	75
NC 100ppt1/6-24	7	0.100	0.089	89
NC 100ppt2/6-24	7	0.100	0.106	106
BW 100ppt1/6-24	7	0.100	0.078	78
BW 100ppt2/6-24	7	0.100	0.065	65
Average:				93
Std. Dev.				12
% RSD				13
n = 23				

TABLE IV
PEAK HEIGHTS OF UNFORTIFIED WATER SAMPLES

Table IV. Peak heights of unfortified water samples

Sample	Data Sheet	Peak Height (μ V)*
WR C1/5-10	1	37
WR C2/5-10	1	32
NC C1/5-20	2	17
NC C2/5-20	2	19
NC-1 FC/6-3	3	15
NC-1 C1/6-3	3	30
NC-1 C2/6-3	3	31
WR C1/6-7	4	33
WR C2/6-7	4	27
NC FC/6-8	5	36
NC Control/6-23	6	25
WR Control/6-23	6	18
NC Control/6-24	7	13
WR Control/6-24	7	37
Average		26
Std. Dev.		9
n = 14		

MDL = 0.051 ppb (Conc. Found = 0.01 μ g/mL)

*Peak height and retention time at elution time of DPX-PE350 for unfortified water samples using diode array detector.

TABLES V.A AND V.B

COMPARISON OF [¹⁴C]DPX-PE350 RECOVERY DATA

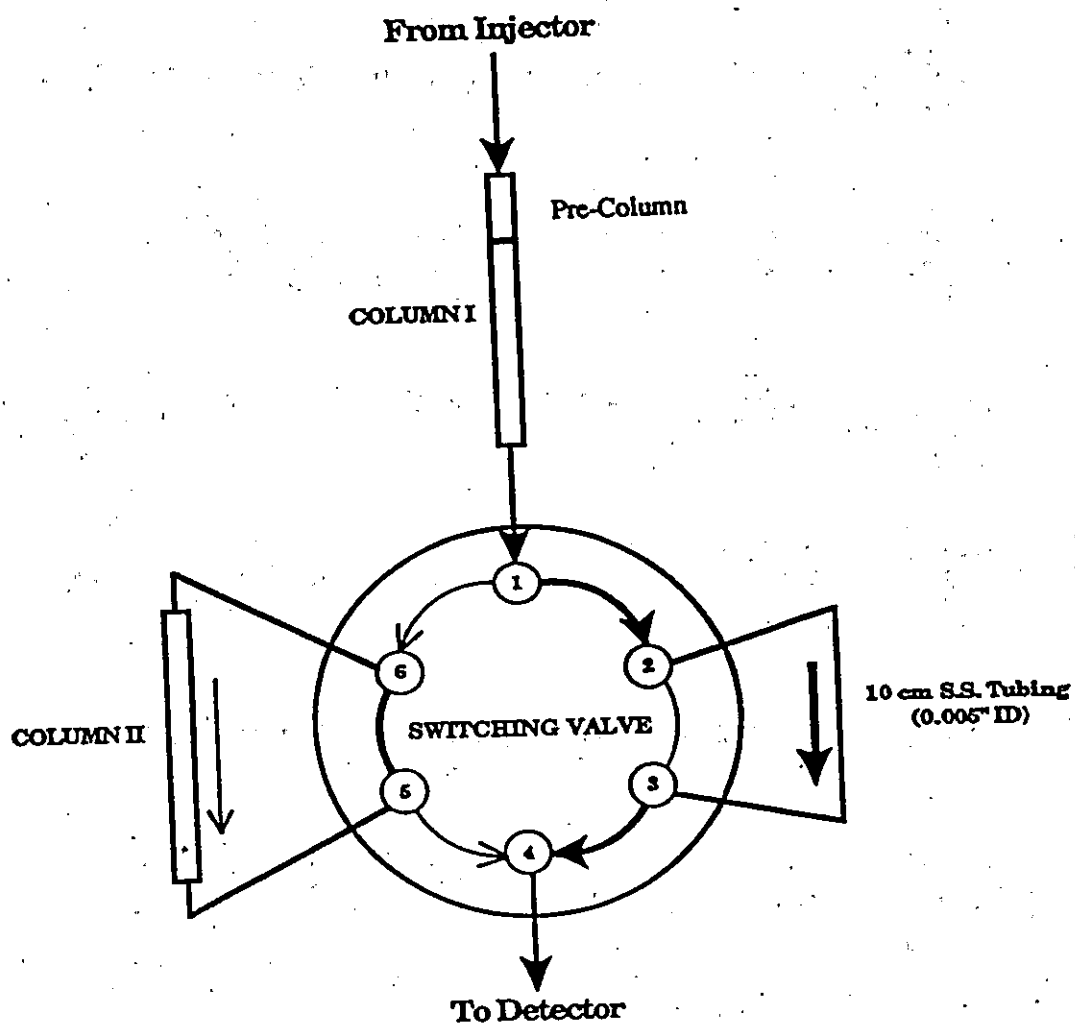
Table V.A. Recovery data using photodiode array detector

Sample	Data Sheet	Fortification Level (ppb)	ppb Found	% Recovery
NC-1 S1/6-3	3	0.513	0.515	100
NC-1 S2/6-3	3	0.513	0.497	97
NC-1 FS/6-3	3	0.513	0.505	98
NC-1 S1/6-8	5	0.513	0.555	108
NC-1 S2/6-8	5	0.513	0.560	109
NC-1 S2/6-8	5	0.513	0.492	96
NC FS/6-8	5	0.513	0.482	94
Average:				100
Std. Dev.				6
% RSD				6
n = 7				

Table V.B. Recovery of data using radioisotope detector

Sample	Data Sheet	Fortification Level (ppb)	ppb Found	% Recovery
NC-1 S1/6-3	8	0.513	0.496	97
NC-1 S2/6-3	8	0.513	0.500	97
NC-1 FS/6-3	8	0.513	0.523	102
NC-1 S1/6-8	9	0.513	0.508	99
NC-1 S2/6-8	9	0.513	0.503	98
NC-1 S2/6-8	9	0.513	0.429	84
NC FS/6-8	9	0.513	0.483	94
Average:				96
Std. Dev.				6
% RSD				6
n = 7				

**FIGURE 1
PLUMBING DIAGRAM FOR COLUMN SWITCHING**



Flow path - valve Position 1:
(Event 3 = on, Event 4 = off)



Flow path - valve Position 2:
(Event 3 = off, Event 4 = on)

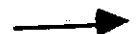
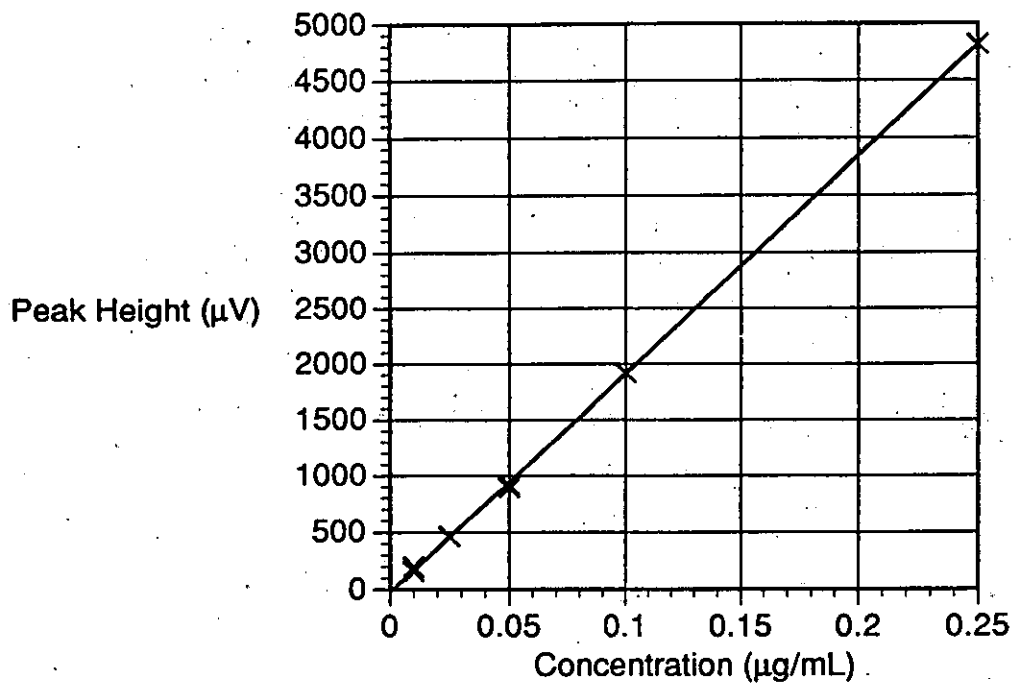


FIGURE 2
STANDARD CURVE FOR DPX-PE350 STANDARDS



$$f(x) = 1.936669E+4 \cdot x + -2.979686E+1$$
$$R^2 = 9.997399E-1$$

FIGURE 3
CHROMATOGRAM OF A 250-NG/ML DPX-PE350 STANDARD

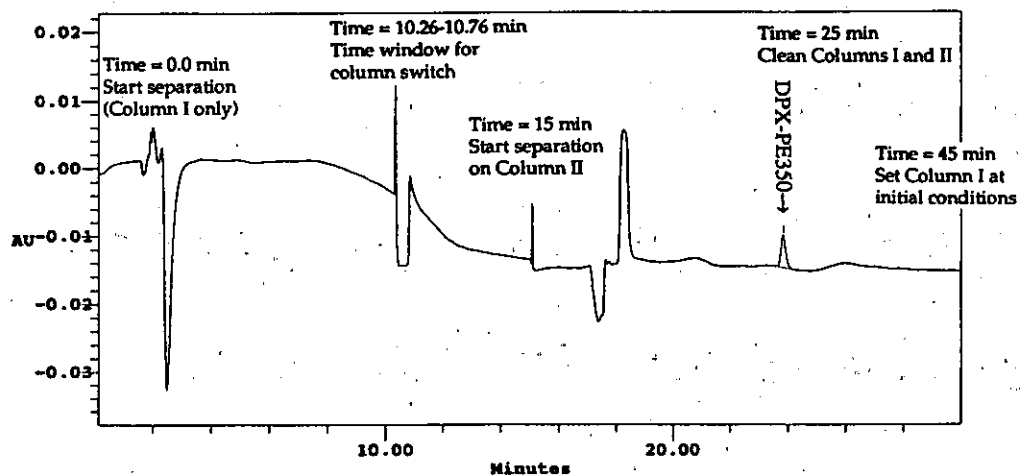
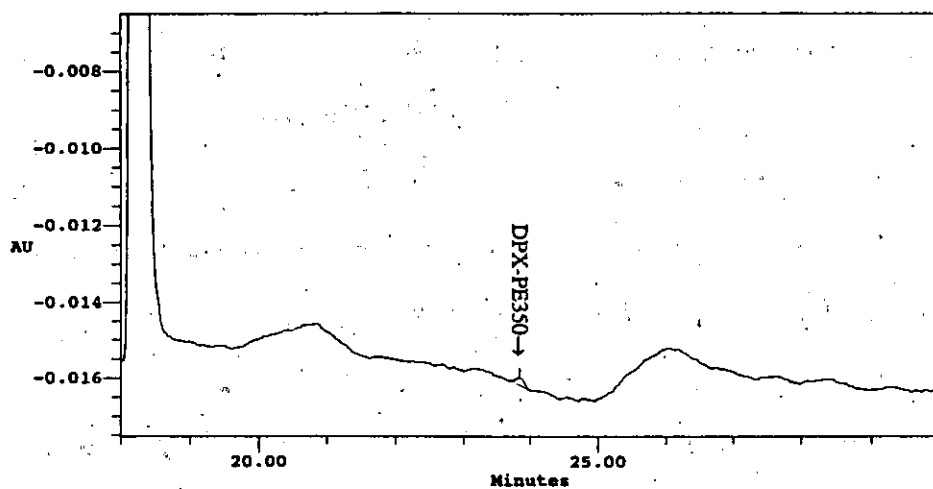


FIGURE 4
CHROMATOGRAMS OF DPX-PE350 STANDARDS

- A. A 0.200-mL injection of a 10-ng/mL DPX-PE350 Standard.
Chromatographic conditions are described in the text.



- B. A 0.100-mL injection of a 100-ng/mL DPX-PE350 Standard.
Chromatographic conditions are described in the text.

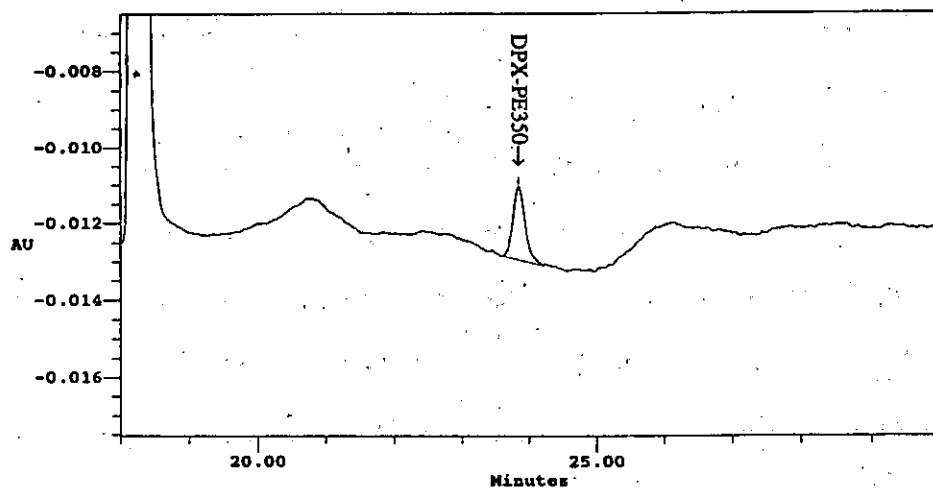
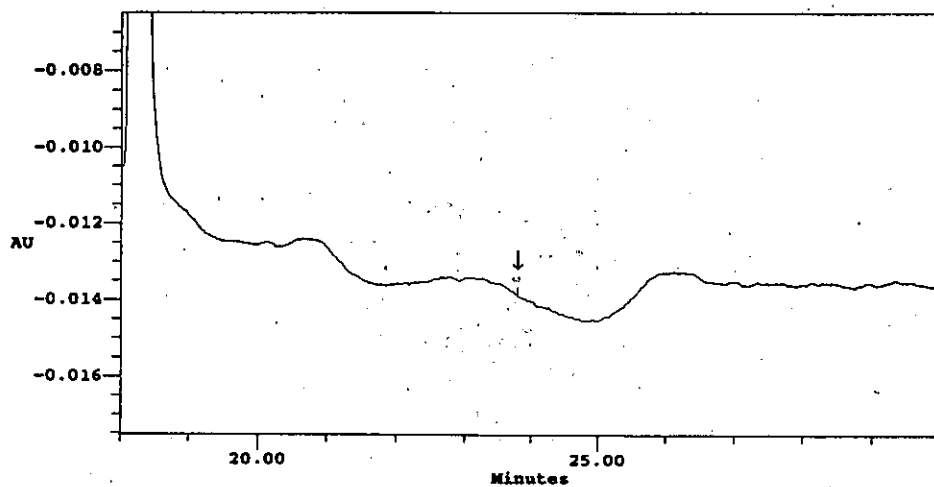


FIGURE 5
CHROMATOGRAMS OF BRANDYWINE RIVER (BW) WATER SAMPLES

- A. Unfortified water sample, BW Control/6-24, see Data Sheet 7 in Appendix. The arrow indicates the retention time of DPX-PE350. Chromatographic conditions are described in the text.



- B. Water sample fortified at 0.100 ppb, BW 100ppt/6-24, see Data Sheet 7 in Appendix. The arrow indicates the retention time of DPX-PE350. Chromatographic conditions are described in the text.

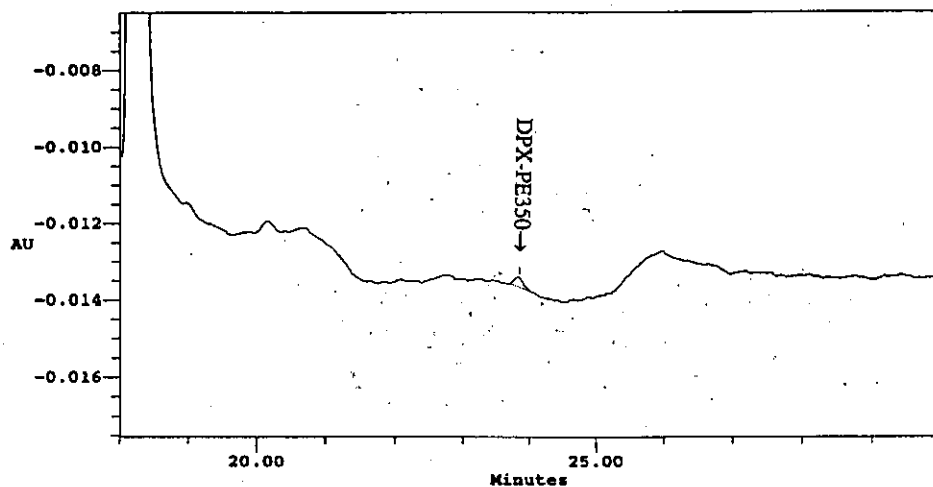
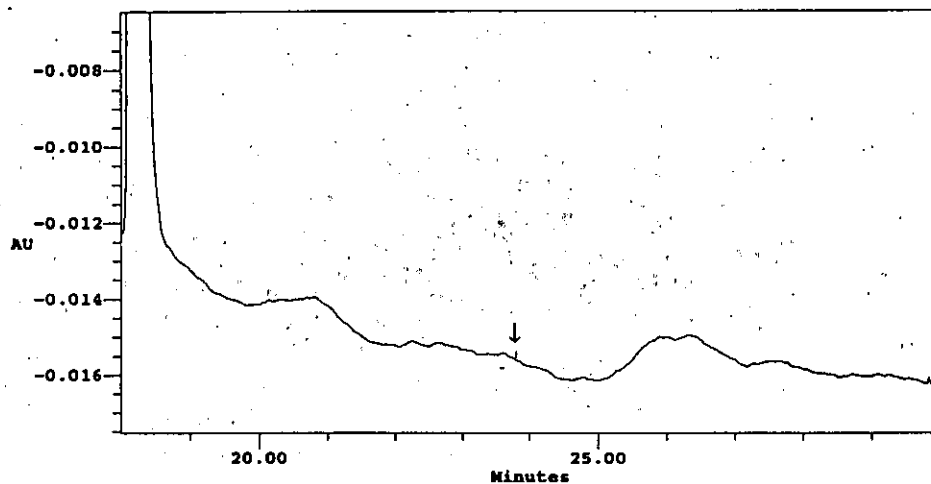


FIGURE 6
CHROMATOGRAMS OF WILSON RUN (WR) STREAM WATER SAMPLES

- A. Unfortified water sample, WR Control/6-23, see Data Sheet 6 in Appendix. The arrow indicates the retention time of DPX-PE350. Chromatographic conditions are described in the text.



- B. Water sample fortified at 0.100 ppb, WR 100ppt/6-23, see Data Sheet 6 in Appendix. Chromatographic conditions are described in the text.

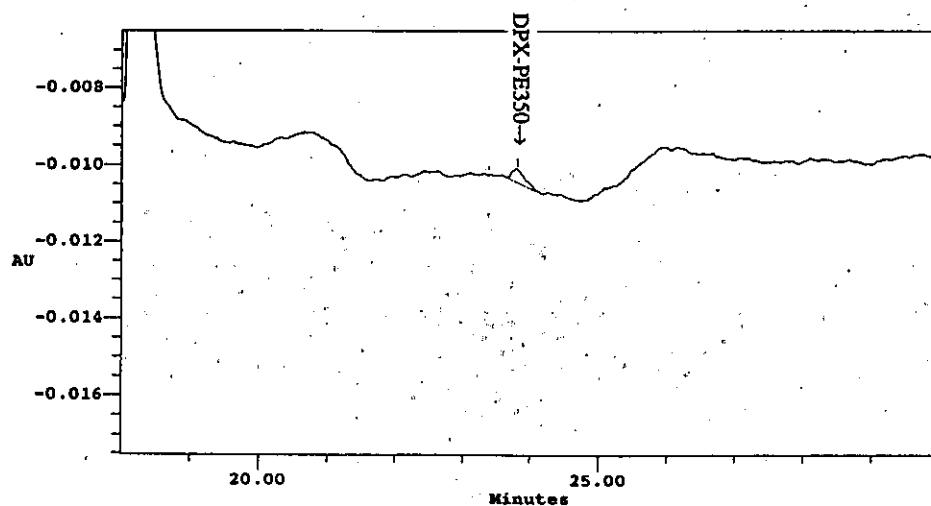
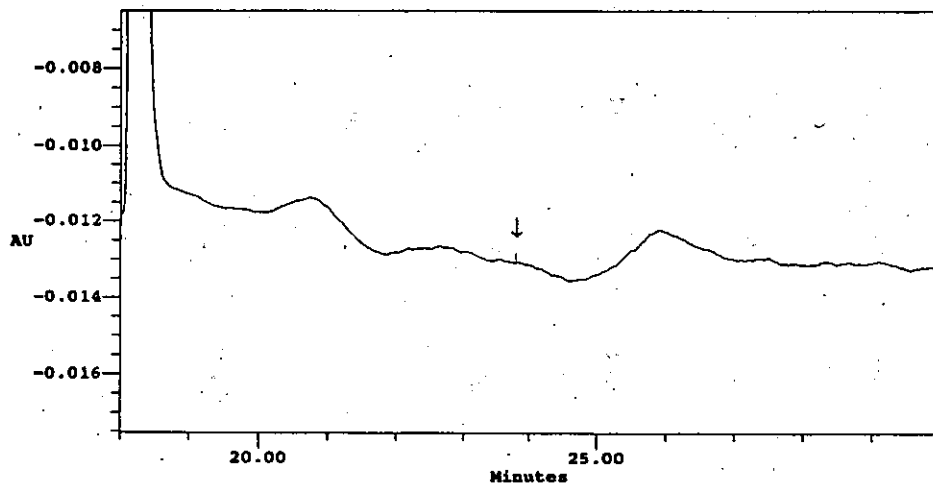


FIGURE 7
CHROMATOGRAMS OF WILSON RUN (WR) STREAM WATER SAMPLES

- A. Unfortified water sample, WR C1/5-10, see Data Sheet 1 in Appendix. The arrow indicates the retention time of DPX-PE350. Chromatographic conditions are described in the text.



- B. Water sample fortified at 0.200 ppb, WR S1/5-10, see Data Sheet 1 in Appendix. Chromatographic conditions are described in the text.

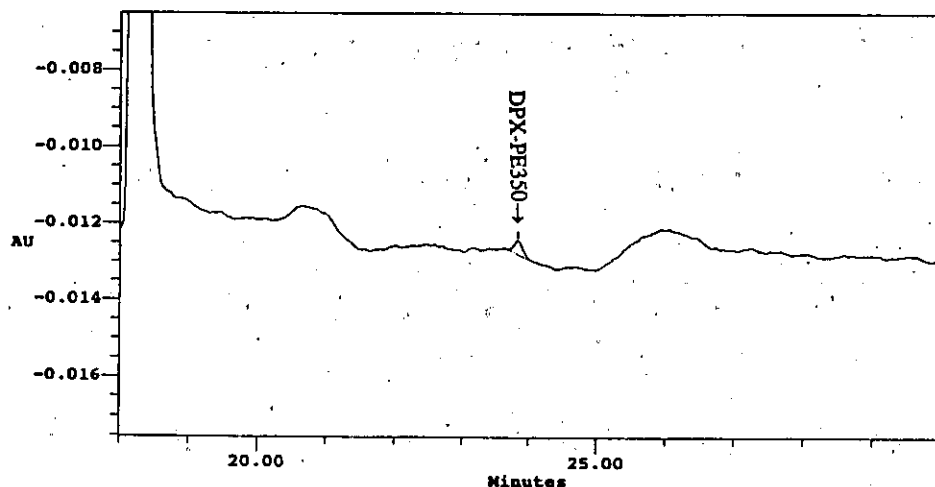
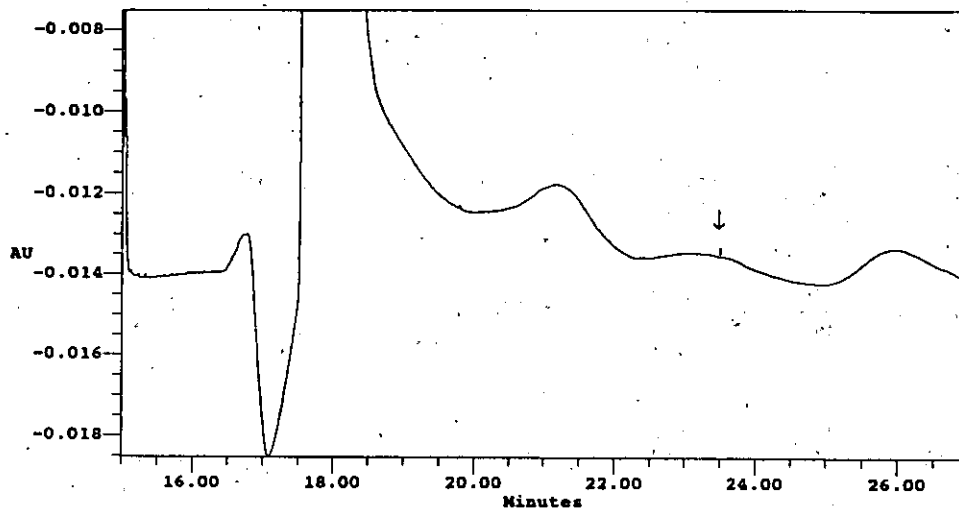


FIGURE 8
CHROMATOGRAMS OF NORTH CAROLINA (NC) GROUNDWATER SAMPLES

- A. Unfortified water sample, NC Control/6-23, see Data Sheet 6 in Appendix. The arrow indicates the retention time of DPX-PE350. Chromatographic conditions are described in the text.



- B. Water sample fortified at 0.100 ppb, NC 100ppt/6-23, see Data Sheet 6 in Appendix. Chromatographic conditions are described in the text.

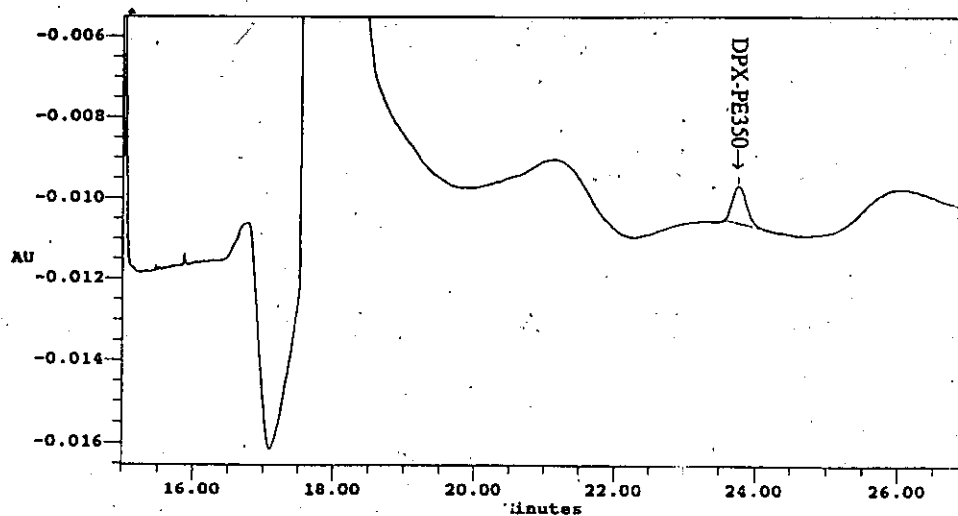
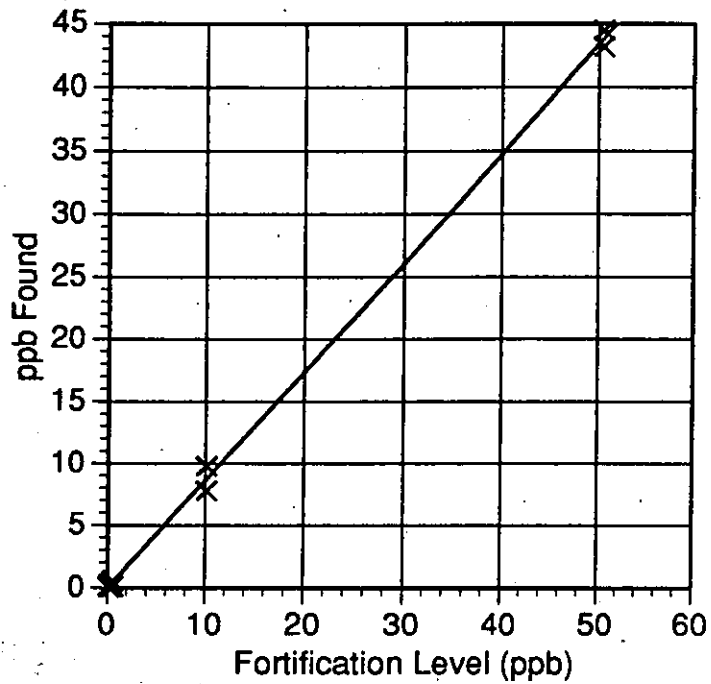
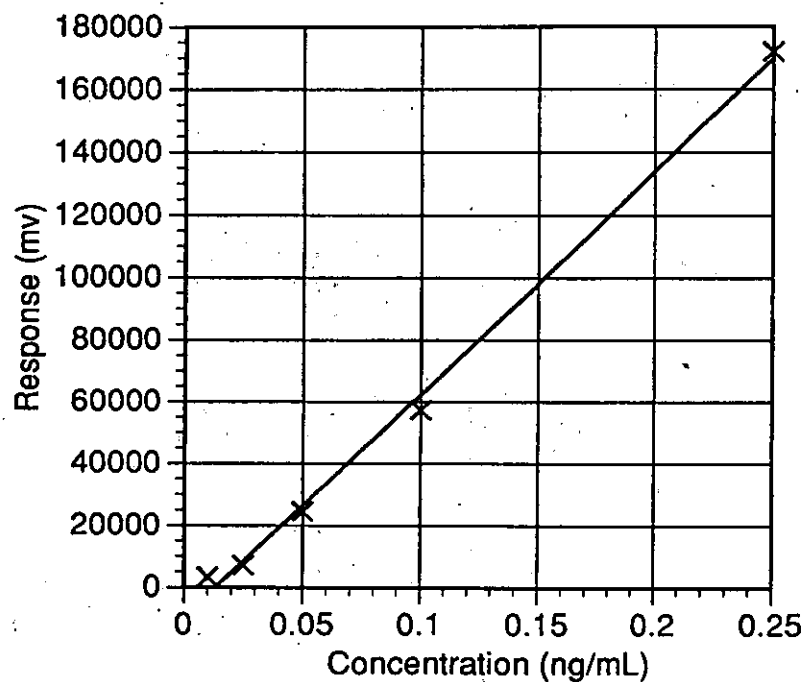


FIGURE 9
PLOT OF MEASURED VS. KNOWN PPB DPX-PE350



$$f(x) = 8.695485E-1 \cdot x + -8.107959E-2$$
$$R^2 = 9.990410E-1$$

FIGURE 10
STANDARD CURVE FOR [¹⁴C]DPX-PE350 STANDARDS

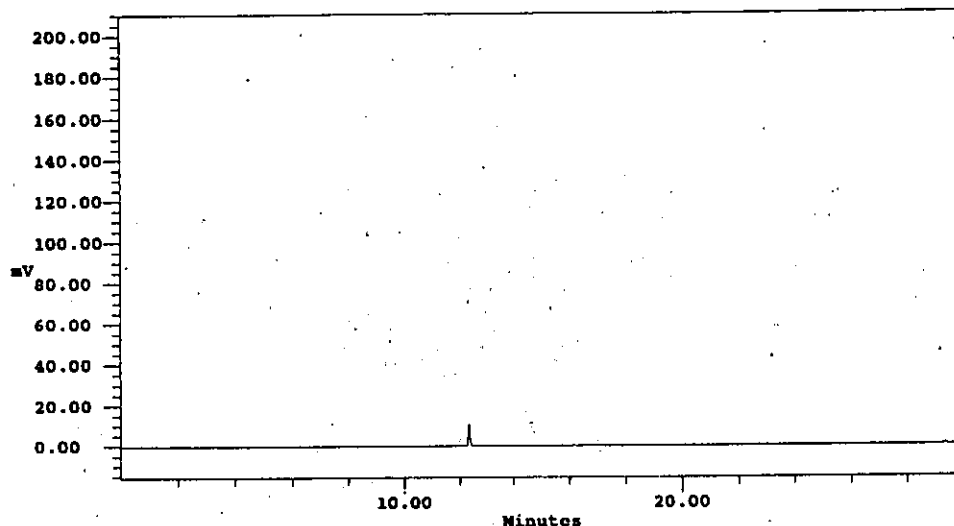


$$f(x) = 7.171401E+5 \cdot x + -9.540731E+3$$

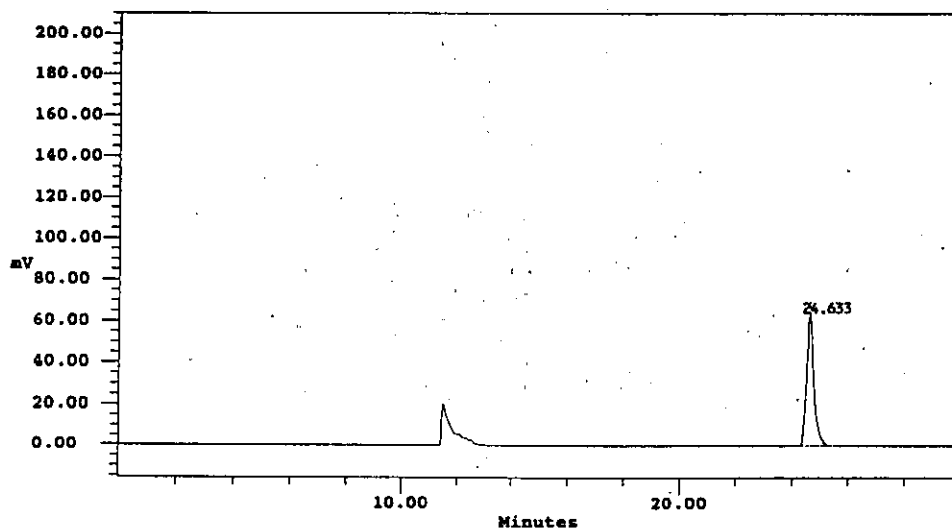
$$R^2 = 9.966389E-1$$

FIGURE 11
CHROMATOGRAMS OF NORTH CAROLINA (NC) GROUNDWATER SAMPLES

- A. Unfortified water sample, NC-1 FC/6-3, see Data Sheet 8 in Appendix. Chromatographic conditions are described in the text. A radioisotope detector was used. DPX-PE350 elutes at 24.63 minutes.



- B. Aged water sample with sediment fortified at 0.513 ppb, NC-1 S2/6-3, see Data Sheet 8 in Appendix. Chromatographic conditions are described in the text. A radioisotope detector was used. DPX-PE350 elutes at 24.633 minutes.



REFERENCES

1. Bates, M., "Determination of the Physico-Chemical Properties of KIH-2031 (DPX-PE350) According to EPA Requirements", DuPont Report No. AMR 2506-92, DuPont Agricultural Products, E. I. du Pont de Nemours and Company, Wilmington, Del.
2. Ramsteiner, K. A., *J. Chromatogr.* 1988, 456, 3-20.
3. Snyder, L. R.; Kirkland, J. J., "Introduction to Modern Liquid Chromatography", 2nd ed.: John Wiley & Sons, Inc.: New York, 1979: Chapter 16.
4. J. C. Miller and J. N. Miller, "Statistics for Analytical Chemistry", 2nd ed.: Ellis, Horwood Limited: Chichester, 1988: p. 216.
5. G. E. P. Box, W. G. Hunter, and J. S. Hunter, "Statistics for Experimenters": John Wiley and Sons: New York, 1978: p. 634.

APPENDIX I
DATA SHEETS NUMBERS 1-9

APPENDIX I

DATA SHEET NUMBER 1

DuPont Study Number: AMR 2746-93

Data Sheet Number: 1

Matrix: Wilson Run (WR) Water

Extracted by: Brock Peterson Date: 5/10/94

Analyzed by: Brock Peterson Date: 5/10/94

Chrom. Std. Used: 04/07/94

Fort. Std. Used: 3/31/94

Injection Volume: 0.200 mL

Final Volume: 1.00 mL

MDL = 0.051 ppb

STANDARDS

Concentration ($\mu\text{g/mL}$)	Peak Height* (μV)	Retention Time (min)	RF** ($\mu\text{V}/\mu\text{g}$)
0.010	327.499	23.808	163750
0.025	675.500	23.763	135100
0.050	1381.767	23.752	138177
0.100	2577.750	23.788	128888
*Column cut window: 0.8 min.		Average:	23.778
**RF = Response Factor		Std. Dev.:	0.025
RF = (Peak Height/Conc.)/Inj. Vol.		% RSD:	0.11
			10.8

SAMPLES ANALYZED

Sample	Sample Volume (mL)	Vol. of Fort. Standard (mL)	Conc. of Fort. Stand. ($\mu\text{g/mL}$)	Fortification Level (ppb)
WR C1/5-10	200.0	None		
WR C2/5-10	200.0	None		
WR S1/5-10	200.0	0.0400	1.01	0.202
WR S2/5-10	200.0	0.0400	1.01	0.202

Sample	Peak Height (μV)	Conc. Found ($\mu\text{g/mL}$)	ppb Found	% Recovery
WR C1/5-10	37	<MDL	<MDL	
WR C2/5-10	32	<MDL	<MDL	
WR S1/5-10	929	0.0339	0.170	84
WR S2/5-10	938	0.0342	0.171	85

Fortification Level, ppb = $1000(\text{Vol. Fort. Std., mL})(\text{Conc. Fort. Std., } \mu\text{g/mL}) / (\text{Sample Vol., mL})$ ppb Found = $1000[(\text{Conc. Found, } \mu\text{g/mL})(\text{Final Vol., mL}) / (\text{Sample Vol., mL})]$ Concentration found, $\mu\text{g/mL}$, = $x = (y-b)/m$ From $y = mx + b$ Peak height, μV , = y Slope, m , $\mu\text{V}/\mu\text{g/mL}$ = y intercept, b , μV =

25169

76.546

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Data calculated and entered by:

Sheldon R. Sumpter

Date: 7/11/94

APPENDIX I (CONTINUED)
DATA SHEET NUMBER 2

DuPont Study Number: AMR 2746-93

Data Sheet Number: 2

Matrix: North Carolina (NC) P-4 Water

Extracted by: Brock Peterson Date: 5/20/94

Analyzed by: Brock Peterson Date: 5/23/94

Chrom.Std.Used: 3/30/94, C14

Fort.Std. Used: 3/24/94, C14

Injection Volume: 0.200 mL

Final Volume: 1.00 mL

MDL = 0.051 ppb

STANDARDS

Concentration ($\mu\text{g/mL}$)	Peak Height* (μV)	Retention Time (min)	RF** ($\mu\text{V}/\mu\text{g}$)
0.025	283.018	23.935	56604
0.050	588.212	23.953	58821
0.100	1201.300	23.987	60065
0.250	3620.934	24.040	72419

*Column cut window: 0.4 min.

**RF = Response Factor

RF = (Peak Height/Conc.)/Inj. Vol.

Average: 23.979 61977.12

Std. Dev.: 0.046 7106.73

%RSD 0.19 11.5

SAMPLES ANALYZED

Sample	Sample Volume (mL)	Vol. of Fort. Standard (mL)	Conc. of Fort. Stand. ($\mu\text{g/mL}$)	Fortification Level (ppb)
NC C1/5-20	200.0	None		
NC S1/5-20	200.0	0.100	1.18	0.590
NC C2/5-20	200.0	None		
NC S2/5-20	200.0	0.100	1.18	0.590

Sample	Peak Height (μV)	Conc. Found ($\mu\text{g/mL}$)	ppb Found	% Recovery
NC C1/5-20	17	<MDL	<MDL	
NC S1/5-20	1489	0.111	0.555	94
NC C2/5-20	19	<MDL	<MDL	
NC S2/5-20	1513	0.112	0.560	95

Fortification Level, ppb = $1000(\text{Vol.Fort.Std., mL})(\text{Conc.Fort.Std., } \mu\text{g/mL}) / (\text{Sample Vol., mL})$ ppb Found = $1000[(\text{Conc.Found, } \mu\text{g/mL})(\text{Final Vol., mL}) / (\text{Sample Vol., mL})]$ Concentration found, $\mu\text{g/mL}$, = $x = (y-b)/m$ From $y = mx + b$ Peak height, μV , = y Slope, m , $\mu\text{V}/\mu\text{g/mL}$ = y intercept, b , μV =

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 Fort. Samples: Control Samples Du Pont Agricultural Products
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Data calculated and entered by: *Sheldon R. Sumpter*

Date: 7/11/94

APPENDIX I (CONTINUED) DATA SHEET NUMBER 3

DuPont Study Number: AMR 2746-93

Data Sheet Number: 3

Matrix: North Carolina (NC) P-4 Water With Sediment, Aged 24 Hours

Extracted by: Brock Peterson Date: 6/3/94

Chrom. Std. Used: 3/30/94, C14

Fort. Std. Used: 3/24/94, C14

Injection Volume: 0.200 mL

Analyzed by: Brock Peterson Date: 6/3/94

Final Volume: 1.00 mL

STANDARDS

MDL = 0.051 ppb

Concentration ($\mu\text{g/mL}$)	Peak Height* (μV)	Retention Time (min)	RF** ($\mu\text{V}/\mu\text{g}$)
0.010	153.841	24.122	76921
0.025	309.172	24.075	61834
0.050	830.042	24.113	83004
0.100	1681.541	24.110	84077
0.250	4431.908	24.157	88638
*Column cut window: 0.4 min.		Average:	24.105
**RF = Response Factor		Std. Dev.:	0.021
RF = (Peak Height/Conc.)/Inj. Vol		% RSD	0.086
			78895
			10412
			13.20

SAMPLES ANALYZED

Sample	Sample Volume (mL)	Vol. of Fort. Standard (mL)	Conc. of Fort. Stand. ($\mu\text{g/mL}$)	Fortification Level (ppb)
NC-1 FC/6-3 (fresh control)	200.0	None		
NC-1 C1/6-3*	230.0	None		
NC-1 C2/6-3*	230.0	None		
NC-1 S1/6-3*	230.0	0.1000	1.18	0.513
NC-1 S2/6-3*	230.0	0.1000	1.18	0.513
NC-1 FS/6-3 (fresh spike)	200.0	0.0870	1.18	0.513

*For these samples, 230 mL of water was fortified, but only 200 mL was used in the method.

These samples were aged 24 h at room temperature.

Sample	Peak Height (μV)	Conc. Found ($\mu\text{g/mL}$)	ppb Found	% Recovery
NC-1 FC/6-3	15	<MDL	<MDL	
NC-1 C1/6-3	30	<MDL	<MDL	
NC-1 C2/6-3	31	<MDL	<MDL	
NC-1 S1/6-3	1770	0.103	0.515	100
NC-1 S2/6-3	1705	0.0994	0.497	97
NC-1 FS/6-3	1731	0.101	0.505	98

Fortification Level, ppb = $1000(\text{Vol. Fort. Std., mL})(\text{Conc. Fort. Std., } \mu\text{g/mL}) / (\text{Sample Vol., mL})$ ppb Found = $1000[(\text{Conc. Found, } \mu\text{g/mL})(\text{Final Vol., mL}) / (\text{Sample Vol., mL})]$ Concentration found, $\mu\text{g/mL}$, = $x = (y-b)/m$ From $y = mx + b$ Peak height, μV , = y Slope, m , $\mu\text{V}/\mu\text{g/mL}$ =

18,018

y intercept, b , μV =

-86.3

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Data calculated and entered by: *Shelton R. Sumpter*

Date: 7/15/94

APPENDIX I (CONTINUED)
DATA SHEET NUMBER 4

DuPont Study Number: AMR 2746-93

Data Sheet Number: 4

Matrix: Wilson Run (WR) Water

Chrom. Std. Used: 4/7/94

Extracted by: Brock Peterson Date: 6/7/94

Fort. Std. Used: 3/31/94

Analyzed by: Brock Peterson Date: 6/7/94

Injection Volume: 0.200 mL

Final Volume: 1.00 mL

MDL = 0.051 ppb

STANDARDS

Concentration ($\mu\text{g/mL}$)	Peak Height* (μV)	Retention Time (min)	RF** ($\mu\text{V}/\mu\text{g}$)
0.010	199.133	23.770	99567
0.025	380.142	23.823	76028
0.050	843.336	23.890	84334
0.100	1665.449	23.857	83272
0.250	4056.051	23.857	81121

*Column cut window: 0.5 min.

Average: 23.835 85800

**RF = Response Factor

Std. Dev.: 0.051 9892

RF = (Peak Height/Conc.)/Inj. Vol.

% RSD: 0.21 11.5

SAMPLES ANALYZED

Sample	Sample Volume (mL)	Vol. of Fort. Standard (mL)	Conc. of Fort. Stand. ($\mu\text{g/mL}$)	Fortification Level (ppb)
WR C1/6-7	200.0	None		
WR C2/6-7	200.0	None		
WR S1/6-7	200.0	0.0200	101	10.10
WR S2/6-7	200.0	0.0200	101	10.10
WR S3/6-7	200.0	0.1000	101	50.50
WR S4/6-7	200.0	0.1000	101	50.50

Sample	Peak Height (μV)	Conc. Found ($\mu\text{g/mL}$)	ppb Found	% Recovery
WR C1/6-7	33	<MDL	<MDL	
WR C2/6-7	27	<MDL	<MDL	
WR S1/6-7*	31598	1.952	9.760	97
WR S2/6-7*	25216	1.558	7.790	77
WR S3/6-7*	139618	8.631	43.16	85
WR S4/6-7*	143895	8.895	44.48	88

*Note: The spikes are out of the range of the standard curve; however, the curve is probably linear, as indicated by the recoveries.

Fortification Level, ppb = $1000(\text{Vol. Fort. Std., mL})(\text{Conc. Fort. Std., } \mu\text{g/mL}) / (\text{Sample Vol., mL})$

ppb Found = $1000[(\text{Conc. Found, } \mu\text{g/mL})(\text{Final Vol., mL}) / (\text{Sample Vol., mL})]$

Concentration found, $\mu\text{g/mL}$, = $x = (y-b)/m$

From $y = mx + b$

Peak height, μV , = y

Slope, m , $\mu\text{V}/\mu\text{g/mL}$ =

16.174

y intercept, b , μV =

21.66

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Data calculated and entered by:

Sheldon R. Hampton

Date: 7/15/94

APPENDIX I (CONTINUED) DATA SHEET NUMBER 5

DuPont Study Number: AMR 2746-93

Data Sheet Number: 5

Matrix: North Carolina (NC) P-4 Water With Sediment, Aged 48 Hours

Extracted by: Brock Peterson Date: 6/8/94

Chrom. Std. Used: 3/30/94, C14

Fort. Std. Used: 3/24/94, C14

Injection Volume: 0.200 mL

Analyzed by: Brock Peterson Date: 6/8/94

Final Volume: 1.00 mL

MDL = 0.051 ppb

STANDARDS

Concentration ($\mu\text{g/mL}$)	Peak Height* (μV)	Retention Time (min)	RF** ($\mu\text{V}/\mu\text{g}$)
0.025	338.760	23.782	67752
0.050	753.110	23.742	75311
0.100	1330.445	23.768	66522
0.250	3645.562	23.787	72911

*Column cut window: 0.5 min.

Average: 23.770 70624

**RF = Response Factor

Std. Dev.: 0.020 4174

RF = (Peak Height/Conc.)/Inj. Vol.

%RSD 0.085 5.91

SAMPLES ANALYZED

Sample	Sample Volume (mL)	Vol. of Fort. Standard (mL)	Conc. of Fort. Stand. ($\mu\text{g/mL}$)	Fortification Level (ppb)
NC FC/6-8	200.0	None		
NC-1 S1/6-8*	230.0	0.1000	1.18	0.513
NC-1 S2/6-8*	230.0	0.1000	1.18	0.513
NC-1 S2/6-8*	230.0	0.1000	1.18	0.513
NC FS/6-8	200.0	0.0870	1.18	0.513

*For these samples, 230 mL of water was fortified, but only 200 mL was used in the method.

These samples were aged 48 h at room temperature.

Sample	Peak Height (μV)	Conc. Found ($\mu\text{g/mL}$)	ppb Found	% Recovery
NC FC/6-8	36	<MDL	<MDL	
NC-1 S1/6-8	1583	0.111	0.555	108
NC-1 S2/6-8	1597	0.112	0.560	109
NC-1 S3/6-8	1401	0.0983	0.492	96
NC FS/6-8	1373	0.0964	0.482	94

Fortification Level, ppb = $1000(\text{Vol. Fort. Std., mL})(\text{Conc. Fort. Std., } \mu\text{g/mL}) / (\text{Sample Vol., mL})$ ppb Found = $1000[(\text{Conc. Found, } \mu\text{g/mL})(\text{Final Vol., mL}) / (\text{Sample Vol., mL})]$ Concentration found, $\mu\text{g/mL}$, = $x = (y-b)/m$ From $y = mx + b$ Peak height, μV , = y Slope, m , $\mu\text{V}/\mu\text{g/mL}$ =

14.633

 y intercept, b , μV =

-37.78

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Data calculated and entered by: *Sheldon K. Shimpster*

Date: 7/15/94

APPENDIX I (CONTINUED) DATA SHEET NUMBER 6

DuPont Study Number: AMR 2746-93

Data Sheet Number: 6

Matrix: North Carolina (NC) and Wilson Run (WR) Water

Extracted by: Brock Peterson Date: 6/23/94

MDL = 0.051 ppb

Analyzed by: Brock Peterson Date: 6/24/94

Standard Used: 6/9/94

Injection Volume: 0.200 mL

Final Volume: 1.00 mL

STANDARDS

Concentration ($\mu\text{g/mL}$)	Peak Height* (μV)	Retention Time (min)	RF** ($\mu\text{V}/\mu\text{g}$)
0.010	159.561	23.922	79781
0.010	200.247	23.845	100124
0.025	466.690	23.745	93338
0.050	891.398	23.832	89140
0.050	922.102	23.887	92210
0.100	1921.852	23.847	96093
0.250	4816.085	23.838	96322

*Column cut window: 0.5 min.

Average: 23.845 92429

**RF = Response Factor

Std. Dev.: 0.055 6576

RF = (Peak Height/Conc.)/Inj. Vol.

%RSD 0.23 7.11

SAMPLES ANALYZED

Sample	Sample Volume (mL)	Vol. of Fort. Standard (mL)	Conc. of Fort. Stand. ($\mu\text{g/mL}$)	Fortification Level (ppb)
NC Control/6-23	200.0	None		
NC 100ppt1/6-23	200.0	0.0200	1.00	0.100
NC 100ppt2/6-23	200.0	0.0200	1.00	0.100
WR Control/6-23	200.0	None		
WR 100ppt1/6-23	200.0	0.0200	1.00	0.100
WR 100ppt2/6-23	200.0	0.0200	1.00	0.100

Sample	Peak Height (μV)	Conc. Found ($\mu\text{g/mL}$)	ppb Found	% Recovery
NC Control/6-23	25	<MDL	<MDL	
NC 100ppt1/6-23	358	0.0200	0.1000	100
NC 100ppt2/6-23	406	0.0225	0.1125	112
WR Control/6-23	18	<MDL	<MDL	
WR 100ppt1/6-23	356	0.0199	0.0995	100
WR 100ppt2/6-23	260	0.0150	0.0750	75

Fortification Level, ppb = $1000(\text{Vol.Fort.Std., mL})(\text{Conc.Fort.Std., } \mu\text{g/mL}) / (\text{Sample Vol., mL})$ ppb Found = $1000[(\text{Conc.Found, } \mu\text{g/mL})(\text{Final Vol., mL}) / (\text{Sample Vol., mL})]$ Concentration found, $\mu\text{g/mL}$, = $x = (y-b)/m$ From $y = mx + b$ Peak height, μV , = y Slope, m , $\mu\text{V}/\mu\text{g/mL}$ =

19.367

 y intercept, b , μV =

-29.79

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Data calculated and entered by:

William R. Sumpter

Date:

7/11/94

APPENDIX I (CONTINUED)
DATA SHEET NUMBER 7

DuPont Study Number: AMR 2746-93

Data Sheet Number: 7

Matrix: North Carolina (NC) and Brandywine River (BW) Water

Extracted by: Brock Peterson Date: 6/24/94

Analyzed by: Brock Peterson Date: 6/24/94

Chrom. Std. Used: 6/9/94

Fort. Std. Used: 6/9/94

Injection Volume: 0.200 mL

Final Volume: 1.00 mL

MDL = 0.051 ppb

STANDARDS

Concentration ($\mu\text{g/mL}$)	Peak Height* (μV)	Retention Time (min)	RF** ($\mu\text{V}/\mu\text{g}$)
0.010	159.561	23.922	79781
0.010	200.247	23.845	100124
0.025	466.690	23.745	93338
0.050	891.398	23.832	89140
0.050	922.102	23.887	92210
0.100	1921.852	23.847	96093
0.250	4816.085	23.838	96322

*Column cut window: 0.5 min.

**RF = Response Factor

RF = (Peak Height/Conc.)/Inj. Vol.

Average:	23.845	92429
Std. Dev.:	0.055	6576
% RSD	0.23	7.11

SAMPLES ANALYZED

Sample	Sample Volume (mL)	Vol. of Fort. Standard (mL)	Conc. of Fort. Stand. ($\mu\text{g/mL}$)	Fortification Level (ppb)
NC Control/6-24	200.0	None		
NC 100ppt1/6-24	200.0	0.0200	1.00	0.100
NC 100ppt2/6-24	200.0	0.0200	1.00	0.100
BW Control/6-24	200.0	None		
BW 100ppt1/6-24	200.0	0.0200	1.00	0.100
BW 100ppt2/6-24	200.0	0.0200	1.00	0.100

Sample	Peak Height (μV)	Conc. Found ($\mu\text{g/mL}$)	ppb Found	% Recovery
NC Control/6-24	13	<MDL	<MDL	
NC 100ppt1/6-24	315	0.0178	0.089	89
NC 100ppt2/6-24	381	0.0212	0.106	106
BW Control/6-24	37	<MDL	<MDL	
BW 100ppt1/6-24	270	0.0155	0.078	78
BW 100ppt2/6-24	223	0.0130	0.065	65

Fortification Level, ppb = $1000(\text{Vol. Fort. Std., mL})(\text{Conc. Fort. Std., } \mu\text{g/mL}) / (\text{Sample Vol., mL})$ ppb Found = $1000[(\text{Conc. Found, } \mu\text{g/mL})(\text{Final Vol., mL}) / (\text{Sample Vol., mL})]$ Concentration found, $\mu\text{g/mL}$, = $x = (y-b)/m$ From $y = mx + b$ Peak height, μV , = y Slope, m , $\mu\text{V}/\mu\text{g/mL}$ =

19,367

y intercept, b , μV =

-29.79

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Data calculated and entered by:

Sheldon R. Sumpter

Date: 7/11/94

APPENDIX I (CONTINUED) DATA SHEET NUMBER 8

DuPont Study Number: AMR 2746-93

Data Sheet Number: 8

Matrix: North Carolina (NC) P-4 Water With Sediment, Aged 24 Hours

Extracted by: Brock Peterson Date: 6/3/94

Chrom.Std.Used: 3/30/94, C14

Fort.Std. Used: 3/24/94, C14

Injection Volume: 0.200 mL

Final Volume: 1.00 mL

Analyzed by: Brock Peterson Date: 6/3/94

MDL = 0.051 ppb

STANDARDS

Concentration ($\mu\text{g/mL}$)	Peak Height* (mV)	Retention Time (min)	RF** (mV/ μg)
0.010	3300.625	24.783	1650313
0.025	7133.352	24.700	1426670
0.050	24613.578	24.617	2461358
0.100	57253.250	24.533	2862663
0.250	171951.500	24.583	3439030
*Column cut window: 0.4 min.		Average:	24.658
**RF = Response Factor		Std. Dev.:	0.108
RF = (Peak Height/Conc.)/Inj. Vol.		%RSD	0.436
			2368007
			836912
			35.34

SAMPLES ANALYZED

Sample	Sample Volume (mL)	Vol. of Fort. Standard (mL)	Conc. of Fort. Stand. ($\mu\text{g/mL}$)	Fortification Level (ppb)
NC-1 FC/6-3 (fresh control)	200.0	None		
NC-1 C1/6-3*	230.0	None		
NC-1 C2/6-3*	230.0	None		
NC-1 S1/6-3*	230.0	0.1000	1.18	0.513
NC-1 S2/6-3*	230.0	0.1000	1.18	0.513
NC-1 FS/6-3 (fresh spike)	200.0	0.0870	1.18	0.513

*For these samples, 230 mL of water was fortified, but only 200 mL was used in the method.
 These samples were aged 24 h at room temperature.

Sample	Peak Height (mV)	Conc. Found ($\mu\text{g/mL}$)	ppb Found	% Recovery
NC-1 FC/6-3		<MDL	<MDL	
NC-1 C1/6-3		<MDL	<MDL	
NC-1 C2/6-3		<MDL	<MDL	
NC-1 S1/6-3	61579	0.0992	0.496	97
NC-1 S2/6-3	57253	0.1000	0.500	97
NC-1 FS/6-3	65436	0.1046	0.523	102

Fortification Level, ppb = $1000(\text{Vol.Fort.Std., mL})(\text{Conc.Fort.Std., } \mu\text{g/mL}) / (\text{Sample Vol., mL})$

ppb Found = $1000[(\text{Conc.Found, } \mu\text{g/mL})(\text{Final Vol., mL}) / (\text{Sample Vol., mL})]$

Concentration found, $\mu\text{g/mL}$, = $x = (y-b)/m$

From $y = mx + b$

$R = 0.996639$

Peak height, mV, = y

Slope, m , $\mu\text{V}/\mu\text{g/mL}$ =

717.14

y intercept, b , μV =

-9540.73

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Data calculated and entered by:



Date: 7/19/94

APPENDIX I (CONTINUED) DATA SHEET NUMBER 9

DuPont Study Number: AMR 2746-93

Data Sheet Number: 9

Matrix: North Carolina (NC) P-4 Water With Sediment, Aged 48 Hours

Extracted by: Brock Peterson Date: 6/8/94

Chrom.Std.Used: 3/30/94, C14

Fort. Std. Used: 3/24/94, C14

Injection Volume: 0.200 mL

Analyzed by: Brock Peterson Date: 6/8/94

Final Volume: 1.00 mL

MDL = 0.051 ppb

STANDARDS

Concentration ($\mu\text{g/mL}$)	Peak Height* (mV)	Retention Time (min)	RF** (mV/ μg)
0.025	7826	24.417	1565200
0.050	21570	24.267	2157000
0.100	40884	24.167	2044200
0.250	124007	24.217	2480140
*Column cut window: 0.5 min.		Average:	24.267
**RF = Response Factor		Std. Dev.:	0.108
RF = (Peak Height/Conc.)/Inj. Vol.		% RSD	0.445
			18.38

SAMPLES ANALYZED

Sample	Sample Volume (mL)	Vol. of Fort. Standard (mL)	Conc. of Fort. Stand. ($\mu\text{g/mL}$)	Fortification Level (ppb)
NC FC/6-8	200.0	None		
NC-1 S1/6-8*	230.0	0.1000	1.18	0.513
NC-1 S2/6-8*	230.0	0.1000	1.18	0.513
NC-1 S2/6-8*	230.0	0.1000	1.18	0.513
NC FS/6-8	200.0	0.0870	1.18	0.513

*For these samples, 230 mL of water was fortified, but only 200 mL was used in the method.

These samples were aged 48 h at room temperature.

Sample	Peak Height (mV)	Conc. Found ($\mu\text{g/mL}$)	ppb Found	% Recovery
NC FC/6-8		<MDL	<MDL	
NC-1 S1/6-8	46134	0.102	0.508	99
NC-1 S2/6-8	45659	0.101	0.503	98
NC-1 S3/6-8	38061	0.0859	0.429	84
NC FS/6-8	43619	0.0967	0.483	94

Fortification Level, ppb = $1000(\text{Vol.Fort.Std., mL})(\text{Conc.Fort.Std., } \mu\text{g/mL}) / (\text{Sample Vol., mL})$ ppb Found = $1000[(\text{Conc.Found, } \mu\text{g/mL})(\text{Final Vol., mL}) / (\text{Sample Vol., mL})]$ Concentration found, $\mu\text{g/mL}$, = $x = (y-b)/m$ From $y = mx + b$ Peak height, mV, = y Slope, m , $\mu\text{V}/\mu\text{g/mL}$ = y intercept, b , μV =

515.984

-6,251.527

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Data calculated and entered by:

William A. Lempert

Date: 7/15/94