SNCR Cost Development Methodology

Final

March 2013 Project 12847-002 Systems Research and Applications Corporation

Prepared by

Sargent & Lundy

55 East Monroe Street • Chicago, IL 60603 USA • 312-269-2000

LEGAL NOTICE

This analysis ("Deliverable") was prepared by Sargent & Lundy, L.L.C. ("S&L"), expressly for the sole use of Systems Research and Applications Corporation ("Client") in accordance with the agreement between S&L and Client. This Deliverable was prepared using the degree of skill and care ordinarily exercised by engineers practicing under similar circumstances. Client acknowledges: (1) S&L prepared this Deliverable subject to the particular scope limitations, budgetary and time constraints, and business objectives of the Client; (2) information and data provided by others may not have been independently verified by S&L; and (3) the information and data contained in this Deliverable are time sensitive and changes in the data, applicable codes, standards, and acceptable engineering practices may invalidate the findings of this Deliverable. Any use or reliance upon this Deliverable by third parties shall be at their sole risk.

This work was funded by the U.S. Environmental Protection Agency and reviewed by William A. Stevens, Senior Advisor – Power Technologies.



Project No. 12847-002 March 2013

SNCR Cost Development Methodology

Establishment of Cost Basis

The formulation of the SNCR cost estimating model is based upon a proprietary Sargent & Lundy LLC (S&L) in-house data base of recent (2009 to 2012) quotes for both lump sum contracts and EPC. The S&L data was analyzed in detail regarding project specifics such as coal type, boiler type, and NOx reduction efficiency. The S&L in-house data includes projects that involved cyclone boilers, T-fired and wall fired systems with multiple levels of injection. The cyclone boiler costs include rich reagent injection (RRI). The data was the basis for the cost estimate formulations developed.

The S&L data was fitted with a least squares curve to establish the trend in \$/kW as a function of gross MW. The SNCR cost model parameters were adjusted to account for market changes and escalation, and then the model output was compared to the S&L data. The model output followed a \$/kW correlation very similar to the S&L in-house data, once the adjustments were made to the model.

The rapid rise in project costs at the lower end of the MW range is due primarily to economies of scale. Additionally, older power plants in the 50 MW range tend to have plant sites that are more compact and therefore difficult to accommodate the reagent storage areas and piping, injection mixing/dilution equipment and construction activities. The smaller power plants also tend to have older control systems that may require upgrades to accommodate the new SNCR control system.

The S&L data includes SNCR projects with various types of boilers, coals, sulfur levels and retrofit complexities. The typical SNCR retrofit was based on:

- Retrofit Difficulty = 1 (Average retrofit difficulty);
- Gross Heat Rate = 9800 Btu/kWh;
- SO₂ Rate = < 3 lb/MMBtu;
- Type of Coal = PRB; and
- Project Execution = Multiple lump sum contracts.

Methodology

Inputs

To predict future retrofit costs several input variables are required. The unit size in MW and NOx levels are the major variables for the capital cost estimation followed by the type of fuel. The fuel type affects the air pre-heater costs if sulfuric acid or ammonium bisulfate deposition poses a problem. In general, if the level of SO_2 is above 3 lb/MMBtu, it is assumed that air heater modifications will be required. The unit heat rate factors into the amount of NOx generated and ultimately the size of the SNCR reagent



Project No. 12847-002 March 2013

SNCR Cost Development Methodology

preparation system. A retrofit factor that equates to difficulty in construction of the system must be defined. The NO_x rate and removal efficiency will impact the amount of urea required and size of the reagent handling equipment. Finally, the boiler type will influence the capital costs of the SNCR system and balance of plant considerations. It should be noted that water treatment facility for dilution water may not be required for small units which may lower the overall cost.

The cost methodology is based on a unit located within 500 feet of sea level. The actual elevation of the site should be considered separately and factored into the cost due to the effects on the flue gas volume. The base SNCR costs are directly impacted by the site elevation. This base cost module should be increased based on the ratio of the atmospheric pressure between sea level and the unit location. As an example, a unit located 1 mile above sea level would have an approximate atmospheric pressure of 12.2 psia. Therefore, the base SNCR cost should be increased by:

14.7 psia/12.2 psia = 1.2 multiplier to the base SNCR cost

Outputs

Total Project Costs (TPC)

First the installed costs are calculated for each required base module. The base module installed costs include:

- All equipment;
- Installation;
- Buildings;
- Foundations;
- Electrical;
- Water treatment for the dilution water; and
- Retrofit difficulty.

The base modules are:

BMS =	Base SNCR system
BMA =	Base air heater modifications, as required
BMB =	Base balance of plant costs including: piping, site upgrades, water treatment for the dilution water, etc
BM =	BMS + BMA + BMB



Project No. 12847-002 March 2013

SNCR Cost Development Methodology

The total base module installed cost (BM) is then increased by:

- Engineering and construction management costs at 10% of the BM cost;
- Labor adjustment for 6 x 10 hour shift premium, per diem, etc., at 10% of the BM cost; and
- Contractor profit and fees at 10% of the BM cost.

A capital, engineering, and construction cost subtotal (CECC) is established as the sum of the BM and the additional engineering and construction fees.

Additional costs and financing expenditures for the project are computed based on the CECC. Financing and additional project costs include:

- Owner's home office costs (owner's engineering, management, and procurement) at 5% of the CECC; and
- Allowance for Funds Used During Construction (AFUDC) at 0% of the CECC and owner's costs as these projects are expected to be completed in less than a year after the equipment is released for the fabrication.

The total project cost is based on a multiple lump sum contract approach. Should a turnkey engineering procurement construction (EPC) contract be executed, the total project cost could be 10 to 15% higher than what is currently estimated.

Escalation is not included in the estimate. The total project cost (TPC) is the sum of the CECC and the additional costs and financing expenditures.

Fixed O&M (FOM)

The fixed operating and maintenance (O&M) cost is a function of the additional operations staff (FOMO), maintenance labor and materials (FOMM), and administrative labor (FOMA) associated with the SNCR installation. The FOM is the sum of the FOMO, FOMM, and FOMA.



Project No. 12847-002 March 2013

SNCR Cost Development Methodology

The following factors and assumptions underlie calculations of the FOM:

- All of the FOM costs were tabulated on a per kilowatt-year (kW yr) basis.
- In general, 0 additional operators are required a new SNCR system.
- The fixed maintenance materials and labor is a direct function of the process capital cost at 1.2% of the BM.
- The administrative labor is a function of the FOMO and FOMM at 3% of (FOMO + 0.4FOMM).

Variable O&M (VOM)

Variable O&M is a function of:

- Reagent use and unit costs;
- Dilution water required and unit water cost;
- Additional power required and unit power cost; and
- Boiler efficiency reduction due to the added water in the boiler and unit replacement coal cost.

The following factors and assumptions underlie calculations of the VOM:

- All of the VOM costs were tabulated on a per megawatt-hour (MWh) basis.
- The reagent usage is a function of the amount of NOx removed, NOx inlet rate, and boiler type. A utilization factor (UF) of 15% is used for units with an inlet NOx of 0.3 lb/MMBtu or lower and 25% for units with an inlet NOx greater than 0.3 lb/MMBtu. For CFB boilers a utilization factor of 25% is used.
- The dilution water usage is based on creating a 5% dilute reagent stream for injection into the boiler.
- The additional power required includes compressed air or blower requirements for the urea injection system and the reagent supply system.
- The additional power is reported as a percent of the total unit gross production. In addition, a cost associated with the additional power requirements can be included in the total variable costs.

Sargent & Lundy

Project No. 12847-002 March 2013

SNCR Cost Development Methodology

• Impacts on the unit heat rate due to injection of liquid water into the boiler are accounted for by additional coal costs to provide added boiler heat input and can be included in the total variable costs.

Input options are provided for the user to adjust the variable O&M costs per unit. Average default values are included in the base estimate. The variable O&M costs per unit options are:

- Urea cost for a 50% by weight solution in \$/ton;
- Auxiliary power cost in \$/kWh;
- Dilution water cost in \$/1000 gallon;
- Operating labor rate (including all benefits) in \$/hr; and
- Replacement coal cost in \$/MMBtu.

The variables that contribute to the overall VOM are:

VOMR =	Variable O&M costs for urea reagent
VOMM =	Variable O&M costs for dilution water
VOMP =	Variable O&M costs for additional auxiliary power
VOMB =	Variable O&M costs for additional coal

The total VOM is the sum of VOMR, VOMM, VOMP, and VOMB. Table 1 shows a complete capital and O&M cost estimate worksheet for an SNCR on a T-fired boiler. Table 2 shows a complete capital and O&M cost estimate worksheet for an SNCR on a CFB boiler.



Project No. 12847-002 March 2013

IPM Model – Updates to Cost and Performance for APC Technologies

SNCR Cost Development Methodology

Table 1. Example Complete Cost Estimate for an SNCR System Installed on a T-fired boiler

Variable	Designation	Units	Value	Calculation
Boiler Type	BT		Tangential	_< User Input
Unit Size	A	(MW)	500	< User Input
Retrofit Factor	В		1	< User Input (An "average" retrofit has a factor = 1.0)
Heat Rate	С	(Btu/kWh)	9800	< User Input
NOx Rate	D	(lb/MMBtu)	0.22	< User Input
SO2 Rate	E	(lb/MMBtu)	2	< User Input
Type of Coal	F		Bituminous 🛛 🔻	< User Input
Coal Factor	G		1	Bit=1.0, PRB=1.05, Lig=1.07
Heat Rate Factor	Н		0.98	C/10,000
Heat Input	- I	(Btu/hr)	4.90E+09	A*C*1000
NOx Removal Efficiency	K	(%)	25	
NOx Removed	L	(lb/hr)	270	D*I/10^6*K/100
Urea Rate (100%)	M	(lb/hr)	1172	L/UF/46*30; IF Boiler Type = CFB OR D > 0.3 THEN UF = 0.25; ELSE UF = 0.15
Water Required	N	(lb/hr)	22263	M*19
Heat Rate Penalty Include in VOM? ☑	V	(%)	0.53	1175*N//*100
Aux Power	0	(%)	0.05	0.05 default value
Include in VOM? 🗹				
Dilution Water Rate	Р	(1000 gph)	2.67	N*0.12/1000
Urea Cost (50% wt solution)	Q	(\$/ton)	310	< User Input
Aux Power Cost	R	(\$/kWh)	0.06	< User Input
Dilution Water Cost	S	(\$/kgal)	1	< User Input
Operating Labor Rate	Т	(\$/hr)	60	< User Input (Labor cost including all benefits)
Replacement Coal Cost	U	(\$/MMBtu)	2	< User Input

Costs are all based on 2012 dollars

Capital Cost Calculation Includes - Equipment, installation, buildings, foundations, electrical, and retrofit difficulty	Example	Comments
BMS (\$) = BT*B*G*220000*(A*H)^0.42; (IF CFB then BT=0.75, ELSE BT=1)	\$ 2,967,000	SNCR (Injectors, Blowers, DCS, Reagent System) Cost
BMA (\$) = IF E ≥ 3 AND F=Bituminous, THEN 69000*(B)*(A*G*H)^0.78, ELSE 0 BT*(L^0.12)*320000*(A)^0.33; (IF CFB then BT=0.75, ELSE BT=1)	\$ - \$ 4,869,000	Air Heater Modification / SO3 Control (Bituminous only & > 3lb/mmBtu) Balance of Plant Cost (Piping, Site Upgrades, water treatment for the dilution water, etc)
BM (\$) = BMS + BMA + BMB BM (\$/KW) =	\$ 7,836,000 16	Total bare module cost including retrofit factor Base cost per kW
Total Project Cost A1 = 10% of BM A2 = 10% of BM A3 = 10% of BM	\$ 784,000 \$ 784,000 \$ 784,000	Engineering and Construction Management costs Labor adjustment for 6 x 10 hour shift premium, per diem, etc Contractor profit and fees
CECC (\$) = BM+A1+A2+A3 CECC (\$/kW) =	\$ 10,188,000 20	Capital, engineering and construction cost subtotal Capital, engineering and construction cost subtotal per kW
B1 = 5% of CECC	\$ 509,000	Owners costs including all "home office" costs (owners engineering, management, and procurement activities)
TPC' (\$) - Includes Owner's Costs = CECC + B1 TPC' (\$/kW) - Includes Owner's Costs =	\$ 10,697,000 21	Total project cost without AFUDC Total project cost per kW without AFUDC
B2 = 0% of (CECC + B1)	\$-	AFUDC (Zero for less than 1 year engineering and construction cycle)
TPC (\$) = CECC + B1 TPC (\$/kW) =	\$ 10,697,000 21	Total project cost Total project cost per kW



Project No. 12847-002 March 2013

Variable	Designation	Units	Value	Calculation
Boiler Type	BT		Tangential 🔹 🔻	< User Input
Unit Size	A	(MW)	500	< User Input
Retrofit Factor	В		1	< User Input (An "average" retrofit has a factor = 1.0)
Heat Rate	С	(Btu/kWh)	9800	< User Input
NOx Rate	D	(lb/MMBtu)	0.22	< User Input
SO2 Rate	E	(lb/MMBtu)	2	< User Input
Type of Coal	F		Bituminous 🛛 🔻	< User Input
Coal Factor	G		1	Bit=1.0, PRB=1.05, Lig=1.07
Heat Rate Factor	Н		0.98	C/10,000
Heat Input	- I	(Btu/hr)	4.90E+09	A*C*1000
NOx Removal Efficiency	K	(%)	25	
NOx Removed	L	(lb/hr)	270	D*I/10^6*K/100
Urea Rate (100%)	М	(lb/hr)	1172	L/UF/46*30; IF Boiler Type = CFB OR D > 0.3 THEN UF = 0.25; ELSE UF = 0.15
Water Required	N	(lb/hr)	22263	M*19
Heat Rate Penalty Include in VOM? ☑	V	(%)	0.53	1175*N/I*100
Aux Power	0	(%)	0.05	0.05 default value
Include in VOM?				
Dilution Water Rate	Р	(1000 gph)	2.67	N*0.12/1000
Urea Cost (50% wt solution)	Q	(\$/ton)	310	< User Input
Aux Power Cost	R	(\$/kWh)	0.06	< User Input
Dilution Water Cost	S	(\$/kgal)	1	< User Input
Operating Labor Rate	Т	(\$/hr)	60	< User Input (Labor cost including all benefits)
Replacement Coal Cost	U	(\$/MMBtu)	2	< User Input

SNCR Cost Development Methodology

Costs are all based on 2012 dollars

Fixed O&M Cost

FOMO (\$/kW yr) = (No operator time assumed)*2080*T/(A*1000) FOMM (\$/kW yr) = BM*0.012/(B*A*1000) FOMA (\$/kW yr) = 0.03*(FOMO+0.4*FOMM)	\$ \$ \$	- 0.19 0.00	Fixed O&M additional operating labor costs Fixed O&M additional maintenance material and labor costs Fixed O&M additional administrative labor costs
FOM (\$/kW yr) = FOMO + FOMM	\$	0.19	Total Fixed O&M costs
Variable O&M Cost			
VOMR (\$/MWh) = M*Q/A/1000	\$	0.73	Variable O&M costs for Urea
VOMM (\$/MWh) = P*S/A	\$	0.01	Variable O&M costs for dilution water
VOMP $(MWh) = O^{R*10}$	\$	0.03	Variable O&M costs for additional auxiliary power required.
VOMB (\$/MWh) = 0.001175*N*U/A	\$	0.10	Variable O&M costs for heat rate increase due to water injected into the boiler
VOM (\$/MWh) = VOMR + VOMM + VOMP + VOMB	\$	0.87	



Project No. 12847-002 March 2013

IPM Model – Updates to Cost and Performance for APC Technologies

SNCR Cost Development Methodology

Table 2. Example Complete Cost Estimate for an SNCR System Installed on a CFB boiler

Variable	Designation	Units	Value	Calculation
Boiler Type	BT		CFB	_< User Input
Unit Size	Α	(MW)	500	< User Input
Retrofit Factor	В		1	< User Input (An "average" retrofit has a factor = 1.0)
Heat Rate	С	(Btu/kWh)	9800	< User Input
NOx Rate	D	(lb/MMBtu)	0.22	< User Input
SO2 Rate	E	(lb/MMBtu)	2	< User Input
Type of Coal	F		Bituminous 🛛 🔻	< User Input
Coal Factor	G		1	Bit=1.0, PRB=1.05, Lig=1.07
Heat Rate Factor	Н		0.98	C/10,000
Heat Input	1	(Btu/hr)	4.90E+09	A*C*1000
NOx Removal Efficiency	К	(%)	25	
NOx Removed	L	(lb/hr)	270	D*I/10^6*K/100
Urea Rate (100%)	М	(lb/hr)	703	L/UF/46*30; IF Boiler Type = CFB OR D > 0.3 THEN UF = 0.25; ELSE UF = 0.15
Water Required	N	(lb/hr)	13358	M*19
Heat Rate Penalty Include in VOM?	V	(%)	0.32	1175*N//*100
Aux Power	0	(%)	0.05	0.05 default value
Include in VOM?				
Dilution Water Rate	Р	(1000 gph)	1.60	N*0.12/1000
Urea Cost (50% wt solution)	Q	(\$/ton)	310	< User Input
Aux Power Cost	R	(\$/kWh)	0.06	< User Input
Dilution Water Cost	S	(\$/kgal)	1	< User Input
Operating Labor Rate	Т	(\$/hr)	60	< User Input (Labor cost including all benefits)
Replacement Coal Cost	U	(\$/MMBtu)	2	< User Input

Costs are all based on 2012 dollars

Capital Cost Calculation Includes - Equipment, installation, buildings, foundations, electrical, and retrofit difficulty	Example	Comments
BMS (\$) = BT*6*G*220000*(A*H)^0.42; (IF CFB then BT=0.75, ELSE BT=1)	\$ 2,225,000	SNCR (Injectors, Blowers, DCS, Reagent System) Cost
BMA (\$) = IF E ≥ 3 AND F=Bituminous, THEN 69000*(B)*(A*G*H)^0.78, ELSE 0 BMB (\$) = BT*(L^0.12)*320000*(A)^0.33; (IF CFB then BT=0.75, ELSE BT=1)	\$- \$3,652,000	Air Heater Modification / SO3 Control (Bituminous only & > 3lb/mmBtu) Balance of Plant Cost (Piping, Site Upgrades, water treatment for the dilution water, etc)
BM (\$) = BMS + BMA + BMB BM (\$/KW) =	\$ 5,877,000 12	water, etc) Total bare module cost including retrofit factor Base cost per kW
Total Project Cost A1 = 10% of BM A2 = 10% of BM A3 = 10% of BM	\$ 588,000 \$ 588,000 \$ 588,000	Engineering and Construction Management costs Labor adjustment for 6 x 10 hour shift premium, per diem, etc Contractor profit and fees
CECC (\$) = BM+A1+A2+A3 CECC (\$/kW) =	\$ 7,641,000 15	Capital, engineering and construction cost subtotal Capital, engineering and construction cost subtotal per kW
B1 = 5% of CECC	\$ 382,000	Owners costs including all "home office" costs (owners engineering, management, and procurement activities)
TPC' (\$) - Includes Owner's Costs = CECC + B1 TPC' (\$/kW) - Includes Owner's Costs =	\$ 8,023,000 16	Total project cost without AFUDC Total project cost per kW without AFUDC
B2 = 0% of (CECC + B1)	\$-	AFUDC (Zero for less than 1 year engineering and construction cycle)
TPC (\$) = CECC + B1 TPC (\$/kW) =	\$ 8,023,000 16	Total project cost Total project cost per kW



Project No. 12847-002 March 2013

IPM Model – Updates to Cost and Performance for APC Technologies

Variable	Designation	Units	Value	Calculation
Boiler Type	BT		CFB 🗸	_< User Input
Unit Size	Α	(MW)	500	< User Input
Retrofit Factor	В		1	< User Input (An "average" retrofit has a factor = 1.0)
Heat Rate	С	(Btu/kWh)	9800	< User Input
NOx Rate	D	(lb/MMBtu)	0.22	< User Input
SO2 Rate	E	(lb/MMBtu)	2	< User Input
Type of Coal	F		Bituminous 🗨	< User Input
Coal Factor	G		1	Bit=1.0, PRB=1.05, Lig=1.07
Heat Rate Factor	Н		0.98	C/10,000
Heat Input		(Btu/hr)	4.90E+09	A*C*1000
NOx Removal Efficiency	K	(%)	25	
NOx Removed	L	(lb/hr)	270	D*1/10^6*K/100
Urea Rate (100%)	M	(lb/hr)	703	L/UF/46*30; IF Boiler Type = CFB OR D > 0.3 THEN UF = 0.25; ELSE UF = 0.15
Water Required	N	(lb/hr)	13358	M*19
Heat Rate Penalty Include in VOM? ☑	V	(%)	0.32	1175*N/I*100
Aux Power	0	(%)	0.05	0.05 default value
Include in VOM?	-	(10)		
Dilution Water Rate	Р	(1000 gph)	1.60	N*0.12/1000
Urea Cost (50% wt solution)	Q	(\$/ton)	310	< User Input
Aux Power Cost	R	(\$/kWh)	0.06	< User Input
Dilution Water Cost	S	(\$/kgal)	1	< User Input
Operating Labor Rate	Т	(\$/hr)	60	< User Input (Labor cost including all benefits)
Replacement Coal Cost	U	(\$/MMBtu)	2	< User Input

SNCR Cost Development Methodology

Costs are all based on 2012 dollars

FOMO (\$/kW yr) = (No operator time assumed)*2080*T/(A*1000) FOMM (\$/kW yr) = BM*0.012/(B*A*1000) FOMA (\$/kW yr) = 0.03*(FOMO+0.4*FOMM)	\$ \$	- 0.14 0.00	Fixed O&M additional operating labor costs Fixed O&M additional maintenance material and labor costs Fixed O&M additional administrative labor costs
FOM (\$/kW yr) = FOMO + FOMM	\$	0.14	Total Fixed O&M costs
Variable O&M Cost VOMR (\$/MWh) = M*Q/A/1000 VOMM (\$/MWh) = P*S/A VOMP (\$/MWh) = O*R*10	\$ \$ \$	0.44 0.00 0.03	Variable O&M costs for Urea Variable O&M costs for dilution water Variable O&M costs for additional auxiliary power required.
VOMB (\$/MWh) = 0.001175*N*U/A	\$	0.06	Variable O&M costs for heat rate increase due to water injected into the boiler
VOM (\$/MWh) = VOMR + VOMM + VOMP + VOMB	\$	0.54	