Colt Atlantic Services, Inc.

Power Services Division

SF-6 Gas Leak Reduction Using Under Pressure Leak Sealing

Industry Start

- Repairing steam leaks to keep ships moving during WWII.
- Also allowed manufacturing facilities to be more productive.
- Power generation was maintained by making repairs without shutting down.



Before & After





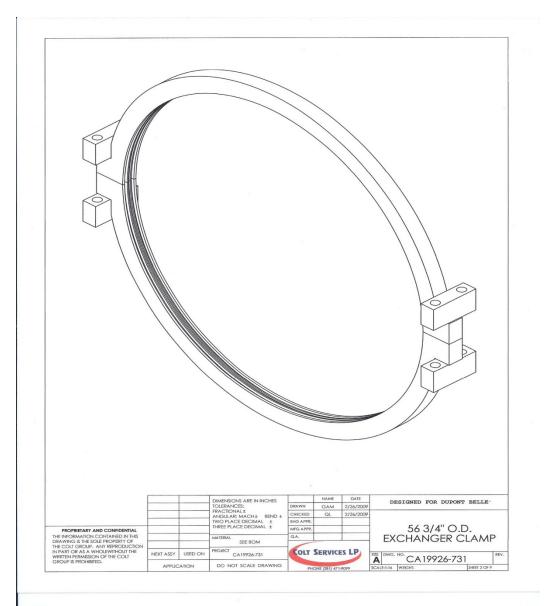
The Repair Process

- Determine point of leak.
- Technician takes precise measurements for a containment device.
- Engineer designs a clamp or enclosure.
- Clamp/enclosure is bolted around the leak and hydraullicy injected with sealant.



Clamp/Enclosure Engineering

DEVICE FABRICATION & CALCULATION PACKAGE CHECKLIST	22
(CHECK MARKS AND N/A ARE THE ONLY OPTIONS)	
DRAWING	CHECK
Each component fully dimensioned where shown	~
Studs defined and described	
Shell thickness	
Corrosion allowance.	
Ear width, height, holes	
Number (& location) of injection fittings	
Mating (to host) surface features	./
Detail allows fabrication (& Cal's) without other ref	11.00
Weld details defined and supported	
weid details defined and supported	N/A
CALCULATIONS	
Conceptual (Isometric) exists, and is accurate	/
Index describes location of key calculations	
Client parameter are defined, (and adequate)	
Stresses at all key points	
Maximum allowable pressure (and limiting component)	
Strongbacking	
Welds (& strengths) fully defined	N/A
Complete bill of materials	
TESTING	
Dye check	N/A
Hydrostatic pressure.	
Other	
OCHEL	
Just to	
CALCULATIONS BY	
DATE 2/26/09	
CHECKED BY PG	
DATE 2/26/09	



CLIENT: DUPONT BELLE

JOB #: CA19926-731 DESIGN #: Q020923

COLT SERVICES LP		
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lculations by	on	2/26/09
PG		2/26/09

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CLIENT: DUPONT BELLE

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SUMMARY OF THE CALCULATIONS
DESIGN PRESSURE = 200 psig DESIGN TEMPERATURE = 338 deg f SERVICE = Amine
THIS DEVICE WILL SUSTAIN MAXIMUM DESIGN PRESSURE OF 453.50 PSI
This clamp is made from SA-516/675 Gr 70 plate and held together by studs of SA-193 Gr B7 & SA-194 Gr 2H nuts.
The injection pressure of 260 psi is derived from the design pressure, it is the pressure differential (required at the gage) to overcome the design pressure, which is assumed to be in the device after attachment, and this higher pressure is used throughout calculations.
All formulae are from ASME Sect. VIII Div. I or ROARK'S 'Formulas for Stress and Strain."
The stress in the clamp shell is 2673.02 psi vs the allowed 22196 psi.
The studs (worst case) are stressed at $14332.88~\mathrm{psi}$ vs their $25000~\mathrm{psi}$ allowed.
The stress in the plate ears are $1839.67~\mathrm{psi}$ vs their allowed $22196~\mathrm{psi}$.
The installed unit will weigh about 560.0 $\#$.
guary 2/26/09 Calculations by on
PG 2/26/09 Checked by on

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                     CALCULATION OF STRESSES
For stress in the clamp shell;
                               where Pi = injection pressure = 260
                                     R = inner radius = 28.44
t = shell thickness = 2.94
              Pi(R+.6t)
          ----- = 2673.02 psi
                  t
                                     vs the allowed 22196 psi
The stress in the retaining studs due to pressure is;
                           where F = Pi * Ap
                                                      = 18486.0
                                 F = Pi * Ap = 18486
Ap = pressure area = 71.1
                                  Nb = number of studs = 4
                                 Ab = area of each = 0.929
                  F
              ----- = 4974.70 psi
                                    vs the allowed 25000 psi
               Nb * Ab
For the plate ears stresses;
                             where F = (Pi * Ap)/2 = 9321.0
                                   Ap = pressure area = 71.7
                                   1 = effective beam = 5.00
                                  b = 2.38 d = 4.00
                                   Z = section modulus = 6.33
                                       (b * d^2) / 6
                  F * 1
                                = 1839.67 psi
                -----
                  4 * Z
                                    vs the allowed 22196 psi
The stress in the existing exchanger stude due to pressure is;
                          where F = Pi * Ap = 639132.0
Ap = pressure area = 2458.2
Nb = number of stude = 48
                                 Ab = area of each = 0.929
                  F
             ----- = 14332.88 psi
               Nb * Ab
                                 vs the allowed 25000 psi
```

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COLT SERVICES LP

	В	I	L	L	0	F	М	A	T	E	R	I	A	L	
ITEM	1	QTY	1		I	DESCRI	PTION				1	MAT	ERIA	LS	
1		1		CLAMP	2 1/2	" THK	. * 62	3/4	l" O.	D.		SA-	516/	675 6	r 70
2		4		BARS 2	3/8	THK.	* 4"	* 8"	LON	1G		SA-	516/	675 G	r 70
3		40		STANDA	RD IN	JECTO	RS					SA-	240	Gr 31	6
4		4		STUDS	1 1/4	1-8 *	20" LO	NG				SA-	193	Gr B7	
5		8		NUTS 1	1/4-	-8 HEX						SA-	194	Gr 2E	ī
6		50.0	#	SEALAN	т										

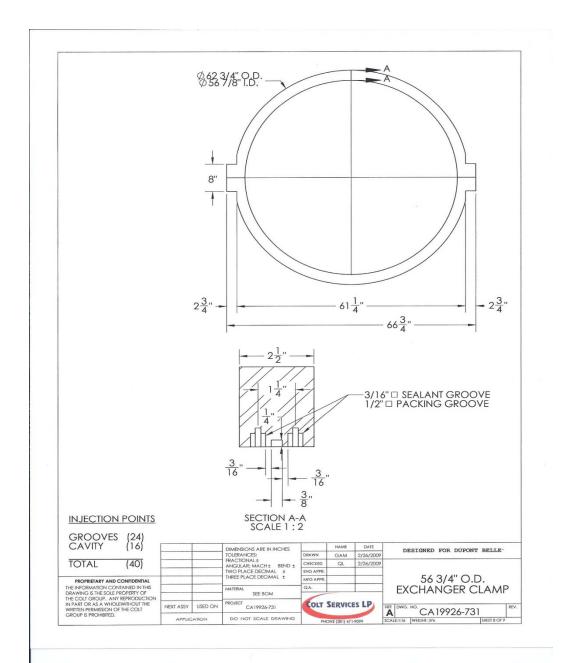
	W	E	I	G	H	T	s	
	CLAMP						480.0	#
	STUDS	&	NUTS				30.0	#
	SEALA	NT					50.0	
-	TOTAL						560.0	

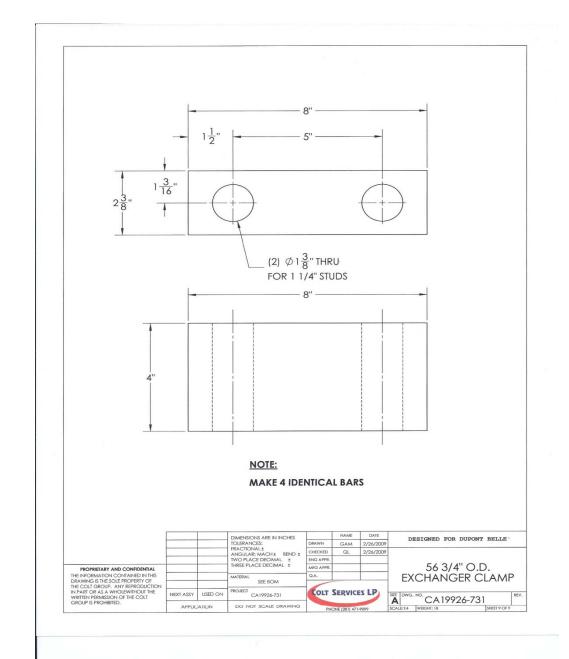
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	COLT SERVICES LP		
MAXIMUM	ALLOWABLE PR	ESS	URE
The maximum allowable de	sign pressure for this (clamp;	
For the clamp shell;	Sa * t (R + .6 * t)	=	2158.97 psi
For the studs; (worst case)	Sa * Nb * Ab Ap	=	453.50 psi
For the plate ears:		=	3136.95 psi
	1 * Ap		
For this device (EXIS	TING EXCHANGER STUDS LI		

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Typical Custom Flange Clamp

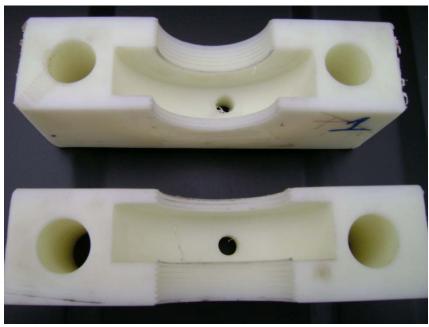
Manufactured from Aluminum, Cast Nylon or Carbon depending upon the application.

Cast Nylon-SF6 Gas Leak Enclosure

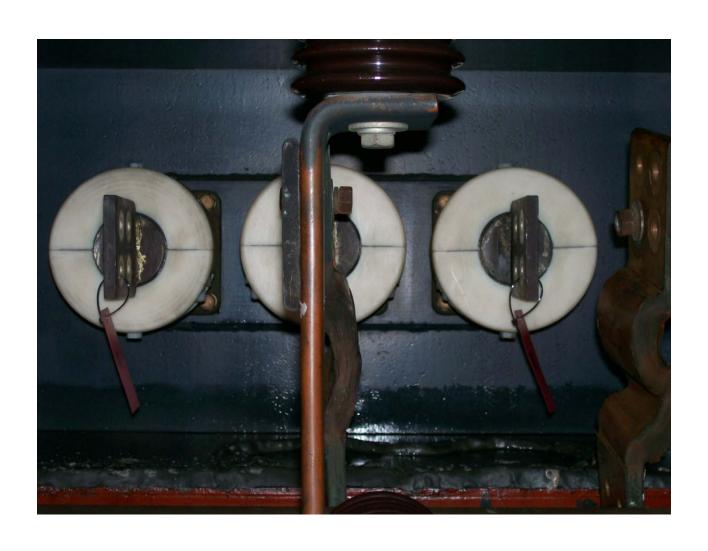


Various Applications





Cast Nylon Clamps



Aluminum Flange Clamps



SF6 Repairs

Insulated Bus



Strong-back ring



Gas Breaker Leaks



Leaking Casting Pores



Before-345 KV SF6 Breaker Leak



SF6 Gas Bushing Flange Repair





Bushing Leak Repair



SF6 Tubing Leak





Breaker Repair

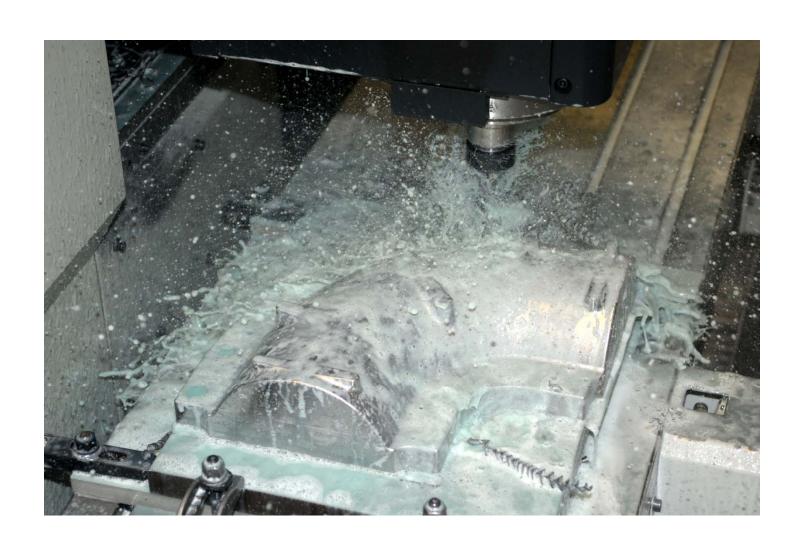




Colt Owned and Operated



Made from a solid block



Colt Injectors



S22 Sealant & Injection Gun



REPORT

Description: Perform analysis of oil samples.

SUMMARY

Two (2) samples of electrical insulating oil were provided for analysis. One sample had been "contaminated" with the customer's two-part sealant (S-22).

The sealant was injected into the oil and allowed to cure. The oil was then analyzed.

Both samples were analyzed for dissolved gas content to determine if the presence of the sealant in transformer oil would generate additional combustible gases.

Results are provided for both sets of tests and there is no noticeable change in the total combustible gas content.

Carbon Dioxide, Nitrogen and Oxygen are non-combustible gasses that are present in air and therefore are not likely due to the presence of the sealant but instead due to exposure to air.

A second series of tests was performed on a solid piece of harden sealant. An AC hipot test was performed on the square sample at increasing voltages.

This report certifies that the above equipment has been tested in compliance with recognized standards or for safe use in a specific manner, or in accordance with Federal, State or Municipal regulations. The report is accurate and true to the best of our knowledge and belief. All equipment used in making physical determinations is accurate and bears recent and direct traceability to the National Bureau of Standards (NBS)

Burlington Electrical Testing Co., Inc.

825 Sycamore Avenue
Croydon, Pa. 19021 (215) 826-9400

Michael Johnson
Project Manager

Colt Atlantic Services, Inc.

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The sample was approximately 4" square and 1" thick. Tests were performed corner to corner and front to back at test voltages up to 35000 Volts AC.

The material performed a level of dielectric strength much greater than oil or air alone.

There is no indication from the tests performed that the presence of this sealant will negatively effect the oil.

Results of Dielectric Fluid Laboratory Tests Device History Report

Customer Name: Colt Atlantic

Customer No: C2548 Report Date: 3/8/03

Project: Colt Atlantic

Device Designation: Clean Control Sample
Manufacturer: -

Job No: 9051L

Serial Number: -Fluid Type: Mineral Oil

Dissolved Gas in Oil/R-Temp Date:	3/ 8/03	(DGIO)	
Sample No:	Y3133		
Hydrogen (H2):	1		
Methane (CH4):	1		
Ethane (C2H3):	0		
Ethylene (C2H4):	0		
Acetylene (C2H2):	0		
Carbon Monoxide (CO):	0		
Carbon Dioxide (CO2):	647		
Nitrogen (N2):	35403		
Oxygen (O2):	17597		
Total Gas Content:	53649		
Total Combustible Gas:	2		

-----BURLINGTON ELECTRICAL TESTING COMPANY-----

Results of Dielectric Fluid Laboratory Tests Device History Report

Customer Name: Colt Atlantic Project: Colt Atlantic

Device Designation: Contaminated Sample

Manufacturer: Serial Number: Fluid Type: Mineral Oil

Customer No: C2548 Report Date: 3/8/03 Job No: 9051L

eral Oil			

Date:	3/8/03	
Sample No:	Y3132	
Hydrogen (H2):	0	1
Methane (CH4):	1	
Ethane (C2H3):	0	
Ethylene (C2H4):	0	
Acetylene (C2H2):	0	
Carbon Monoxide (CO):	1	
Carbon Dioxide (CO2):	707	
Nitrogen (N2):	41395	
Oxygen (O2):	22653	
Total Gas Content:	64757	
Total Combustible Gas:	2	

Job No: 9051L Issued to: Colt Atlantic Services, Inc. P.O. Box 74396 Richmond, VA 23236 Colt Atlantic Services, Inc. Project: Richmond, VA FIELD ENGINEER'S REPORT A/C Hipot Corner to Corner Test Voltage Leakage - 5,000: .2 AC mA - 10,000: .3 AC mA - 15,000: .5 AC mA - 20,000: .7 AC mA - 25,000: .75 AC mA Hear Tracking - 30,000: 1.0 AC mA Hear Tracking - 35,000: 1.2 AC mA Hear Tracking (5 Minutes) Front to Back - 5,000: .2 AC mA - 10,000: .3 AC mA - 15,000: .5 AC mA - 20,000: .75 AC mA - 25,000: 1.0 AC mA - 30,000: 1.25 AC mA - 35,000: Flash over before.

Leakage current is measured in AC milliamps.

Summary

Reduced or no outage time.

Guaranteed for two-years.

Can be re-injected if needed at a later date.

Should not be used to replace re-gasketing.