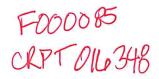
Enclosure 1





November 2, 2016

Received

NOV 0 4 2016

Air Quality Division

Nancy Vehr Air Quality Administrator Wyoming Department of Environmental Quality 200 West 17th Street 3rd Floor Cheyenne, WY 82002

Re: Laramie River Station1-Hour SO₂ Characterization Report

Dear Ms. Vehr:

Basin Electric Power Cooperative recently completed the SO₂ Characterization for the Laramie River Station and the final report is enclosed for your consideration.

Enclosed is one printed copy and electronic CD's containing the report and supporting modeling files. If you have any questions or need any further information, please contact me at (701) 557-5635 or email at <u>cmiller@bepc.com</u>.

Sincerely,

Cris Miller Senior Environmental Project Specialist

/ser Enclosure

cc: Erin Dukart Mike Paul Josh Nall

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Modeling Report for Basin Electric Power Cooperative: SO₂ Characterization for the Laramie River Station

Basin Electric Power Cooperative Bismarck, ND

Project Number: 60438665

October 31, 2016

Received

NUV 0 4 2016

Air Quality Division

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Basin Electric Power Cooperative Bismarck, ND

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Executive Summary

The Basin Electric Power Cooperative operates Laramie River Station (LRS), a coal power plant located 3.5 miles due east of Wyoming Highway 320, 5.5 miles northeast of Wheatland, WY. The facility currently consists of three boiler electric generating units (Units 1 through 3), with a total capacity of approximately 1,710 megawatts (MW). Units 1, 2, and 3 are pulverized coal-fired (Subbituminous) radiant heat boilers. Units 1 and 2 are equipped with wet scrubbers and Unit 3 uses dry scrubber absorbers for SO₂ flue gas desulfurization control. The facility emitted 8,151 tons per year of SO₂ in 2015.

In August 2015, the U.S. Environmental Protection Agency issued the SO_2 Data Requirements Rule¹ (DRR), which directs state and tribal air agencies in "an orderly process" to identify maximum ambient air 1-hour SO_2 concentrations in areas with large sources of SO_2 emissions. The purpose of the DRR is to identify large SO_2 -emitting sources, generally those with annual emissions greater than 2,000 tons for the most recent year for which emissions data are available, and to characterize SO_2 concentrations in the vicinity of these sources. LRS was listed as a DRR source by the state of Wyoming based upon its annual SO_2 emissions.

The Wyoming Department of Environmental Quality (WDEQ) consulted with the owners or operators of the DRR-identified sources in Wyoming to identify the means (either monitoring or modeling) for determining whether the area surrounding each identified source is in attainment with the SO₂ NAAQS for area designation purposes. Basin Electric selected modeling as the means for this characterization.

This modeling report provides the results of the modeling characterization of SO2 concentrations in the vicinity of LRS. The modeling was based upon three recent years of actual emissions (2013-2015). The modeling procedures that were approved by EPA Region 8 used default regulatory options and are consistent with applicable guidance, including the August 2016 "SO₂ NAAQS Designations Modeling Technical Assistance Document" (TAD)² issued by the United States Environmental Protection Agency (EPA).

The modeled concentrations from the AERMOD modeling were calculated based on the form of the 1hour SO₂ NAAQS, with inclusion of regional background concentrations as agreed to in the final protocol. **Table ES-1** shows the NAAQS compliance modeling results of LRS and monitoring background combined. The total concentration is less than 50% of the NAAQS, and indicates that future modeling characterization of the plant's SO₂ concentrations is not needed as long as the emissions are comparable to (or less than) those used in this modeling analysis. The results support the designation of the area in the vicinity of LRS as being in attainment of the 1-hour SO₂ NAAQS.

Table ES-1 AERMOD Modeled Design SO₂ Concentration from LRS including Background Concentration

Modeling Option	LRS Modeled Design Concentration (µg/m³)	Background Design Concentration from Cheyenne (μg/m ³)	Total Design Concentration (μg/m³)	NAAQS (μg/m³)
Default	78.48	6.37	84.85	196.5

1

¹ Docket ID No. EPA-HQ-OAR-2013-0711, August 10, 2015. http://www.epa.gov/oagps001/sulfurdioxide/pdfs/so2_drr__final_081215.pdf.

² https://www.epa.gov/sites/production/files/2016-06/documents/so2modelingtad.pdf

1. Introduction

1.1 Overview of the SO₂ Data Requirements Rule

In August 2015, the U.S. Environmental Protection Agency (EPA) issued the SO₂ Data Requirements Rule³ (DRR), which directs state and tribal air agencies in "an orderly process" to identify maximum ambient air 1-hour SO₂ concentrations in areas with large sources of SO₂ emissions.

The purpose of the DRR is to identify large SO_2 -emitting sources, generally those with annual emissions greater than 2,000 tons for the most recent year for which emissions data are available, and to characterize SO_2 concentrations in the vicinity of these sources. The affected sources are those that have not been previously captured as part of the initial non-attainment area designations for the 1-hour SO_2 National Ambient Air Quality Standard (NAAQS) in August 2013, or with the sources identified by the March 2015 Consent Decree between the EPA and the Sierra Club and National Resources Defense Council.

The Wyoming Department of Environmental Quality (WDEQ) has consulted with the owners or operators of the DRR-identified sources in Wyoming to identify the means for determining whether the area surrounding each identified source is in attainment with the SO₂ NAAQS for area designation purposes. According to the DRR, the method of characterizing the SO₂ concentrations around each source can be done by either:

- installing and operating an ambient air monitoring network; or
- performing an air dispersion modeling study to characterize the SO₂ concentration pattern in areas beyond the secured industrial boundary where monitors could be placed.

Alternatively, instead of a source characterization, each identified source can modify its air operating permit prior to January 13, 2017 such that the DRR-identified source either:

- limits annual SO₂ emissions to less than 2,000 tons, or
- limits short-term (1-hour) and/or longer-term (up to 30-day average) SO₂ emissions that, based on the results of an air dispersion modeling study, demonstrate that the area surrounding the source is in attainment with the SO₂ NAAQS, allowing the state air agency to provide a recommendation for a designation of attainment with the NAAQS.

This modeling report, based on the revised and EPA-approved protocol dated September 2016, is provided for Basin Electric Power Cooperative's (Basin Electric) Laramie River Station ("LRS") for the option of characterizing SO₂ concentrations from three recent years of actual emissions using modeling. The modeling procedures use default regulatory options and are consistent with applicable guidance, including the August 2016 "SO₂ NAAQS Designations Modeling Technical Assistance Document" (TAD)⁴ issued by the United States Environmental Protection Agency (EPA).

1.2 Report Organization

This report addresses LRS, located northeast of Wheatland, Wyoming, that the Wyoming DEQ has identified for consideration under the DRR. SO₂ emission sources for this facility are discussed in this report, and modeling procedures are specified.

Section 2 provides a description of LRS. This section includes a map showing the location of the source relative to surrounding topographic features, as well as a table of major emission points and stack

http://www.epa.gov/oaqps001/sulfurdioxide/pdfs/so2 drr final 081215.pdf.

³ Docket ID No. EPA-HQ-OAR-2013-0711, August 10, 2015.

⁴ https://www.epa.gov/sites/production/files/2016-06/documents/so2modelingtad.pdf

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parameters. Section 3 provides the general modeling approach and technical options used for the SO_2 concentration characterization. Specific information about the modeling approach used for LRS, and modeling of background contributions, which covers a review of any nearby large sources to include in the modeling, as well as choice of a regional background monitor, are discussed in Section 4. Section 5 discusses the SO_2 characterization modeling results.

2. Description of Basin Electric's Laramie River Station

The Basin Electric operates LRS, a coal power plant located 3.5 miles due east of Wyoming Highway 320, 5.5 miles northeast of Wheatland, WY. The facility currently consists of three boiler electric generating units (Units 1 through 3), with a total capacity of approximately 1,710 megawatts (MW). Units 1, 2, and 3 are pulverized coal-fired (Subbituminous) radiant heat boilers. Units 1 and 2 are equipped with wet scrubbers and Unit 3 uses dry scrubber absorbers for SO₂ flue gas desulfurization control.

The location of the plant showing the topography in the vicinity is provided in **Figure 2-1**. As shown in the figure, the area in the vicinity of the plant features relative flat terrain in the immediate vicinity, with somewhat elevated terrain to the north and east of the plant. In addition, it is evident from inspection of the topography and the land use in **Figure 2-2** that the area in the immediate vicinity (i.e., within 3 km) of LRS can be characterized as having a rural land use type. **Figure 2-3** provides the National Land Cover Database color palette, indicating that the land use around LRS is predominately desert shrubland and grassland outside the immediate plant.

The modeling was performed with the actual stack heights in accordance with recommendations in the DRR and TAD. **Table 2-1** shows the physical stack parameters that were used in the modeling. The hourly exhaust flow rates, temperatures, and emission rates were based on the actual data available from the continuous emission monitor (CEM) systems. The emissions for modeling consisted of actual hourly data for the most recent three calendar years (2013-2015).

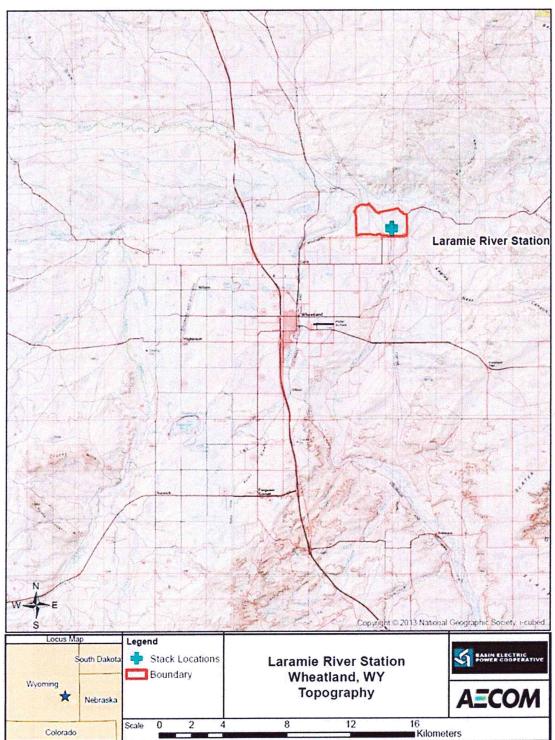
The three coal-fired boilers are the major sources of SO_2 emissions at LRS. There are other small insignificant sources of SO_2 at LRS; however, these sources are either emergency in nature and thus will not operate routinely or have very low actual SO_2 emissions. In 2015, the auxiliary boiler and emergency equipment had very few hours of operation, as is typical. For example, the auxiliary boiler was only operated for 5 hours in 2015. The remainder of the ancillary equipment is operated on an emergency basis and other than the periodic testing, they do not typically operate at all. Therefore, these small sources of SO_2 are not expected to have an impact on the results of the 1-hour SO_2 modeling and were not included in the modeling consistent with guidance provided by EPA's March 1, 2011 Clarification Memo⁵. As such, the three coal-fired boilers are the only emission sources from LRS that were included in the 1-hour SO_2 modeling.

Unit	Description	Stack Base Elevation (meters)	Stack Height (meters)	Flue Diameter (meters)
Unit 1	Pulverized Coal Fired Boiler	1391.1	182.1	8.69
Unit 2	Pulverized Coal Fired Boiler	1391.1	182.1	8.69
Unit 3	Pulverized Coal Fired Boiler	1391.1	182.1	8.69

Table 2-1: Laramie River Station – Physical Stack Parameters⁽¹⁾

(1) Emission rates, exhaust temperature, and exhaust flow rate will be based on hourly CEMs data.

⁵ Available at <u>http://www3.epa.gov/scram001/guidance/clarification/Additional Clarifications AppendixW Hourly-NO2-</u>NAAQS FINAL 03-01-2011.pdf.



Topography in the Vicinity of the Laramie River Station Figure 2-1:

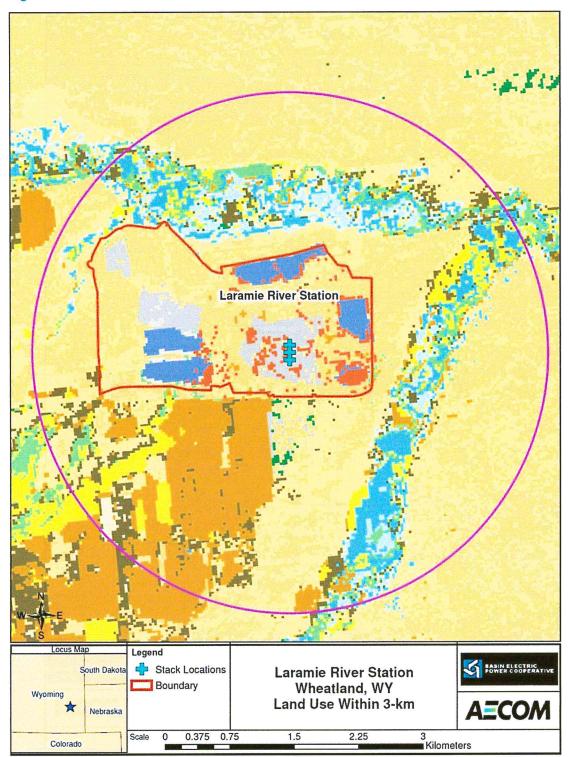


Figure 2-2: Land Use within 3 Kilometers of Laramie River Station

Figure 2-3: NCLD Color Palette for Land Use Types

NLCD 1992 Land Cover Classification Legend

- 11 Open Water
- 12 Perennial Ice/Snow
- 21 Low Intensity Residential
- 22 High Intensity Residential
- 23 Commercial/Industrial/Transportation
- 31 Bare Rock/Sand/Clay
- 32 Quarries/Strip Mines/Gravel Pits
 - 33 Transitional Barren
 - 41 Deciduous Forest
 - 42 Evergreen Forest
 - 43 Mixed Forest
 - 51 Shrubland
 - 61 Orchards/Vineyards/Other
 - 71 Grassland/Herbaceous
 - 81 Pasture/Hay
 - 82 Row Crops
- 83 Small Grains
 - 84 Fallow
 - 85 Urban/Recreational Grasses
- 91 Woody Wetlands
 - 92 Emergent Herbaceous Wetlands

3. Dispersion Modeling Selection and Options

The EPA Guideline on Air Quality Models (Appendix W⁶) prescribes a set of approved models for regulatory applications for a wide range of source types and dispersion environments. Based on a review of the factors discussed below, the latest version of AERMOD (15181) was used in the DRR modeling for the LRS utilizing default options only.

Based on EPA guidance provided in the modeling Technical Assistance Document (TAD), all stacks were modeled with their actual physical stack height. In addition, EPA's Building Profile Input Program (BPIP-Version 04274) version that is appropriate for use with PRIME algorithms in AERMOD was used to incorporate downwash effects in the model for all modeled point sources. The building dimensions of nearby building structures were input to the BPIPPRM program to determine direction-specific building data for input to AERMOD.

Consistent with the modeling TAD guidance for characterizing SO₂ concentrations due to existing emissions, actual hourly emission rates (as well as hourly stack temperature and exit velocity) from the most recent three years that are available (2013-2015) were used. Consistent with the TAD guidance, receptors used in the modeling may be excluded from the following areas that are not considered ambient air, or where a monitor could not be placed:

- over water (rivers, lakes, ponds, and swamps), and
- on the secured property of LRS.

Receptor spacing is consistent with WDEQ guidelines⁷ and features the most closely spaced receptors close to the LRS.

⁷ http://deg.wyoming.gov/aqd/new-source-review/resources/quidance-documents/.

⁶ Available at <u>http://www3.epa.gov/ttn/scram/guidance/guide/appw_05.pdf</u>.

4. Modeling Configuration

4.1 Modeling Domain

LRS is a relatively isolated facility with little to no industrial development nearby. The modeling domain was established based on the area necessary to include all modeled sources (primary plus background) and all modeled receptor points. The modeling domain was set to 25 km, as this is the furthest distance we anticipated the need for receptor points.

4.2 Receptor Grid

The proposed modeling analysis was conducted using the following Cartesian receptor grid design.

- 25-m receptor spacing along the facility boundaries for the SO₂ characterization.
- 100-m receptor spacing extending out 5 kilometers from the grid center.
- 500-m receptor spacing between 5 and 10 kilometers from the grid center.
- 1000-m receptor spacing was used beyond 10 kilometers (out to 25 km).

The receptor grid used in the modeling analysis was based on Universal Transverse Mercator (UTM) coordinates referenced to NAD 83 datum and in zone 13. The receptor grid is centered at the approximate mid-point of the modeled facility based on WDEQ Guidance Document⁸.

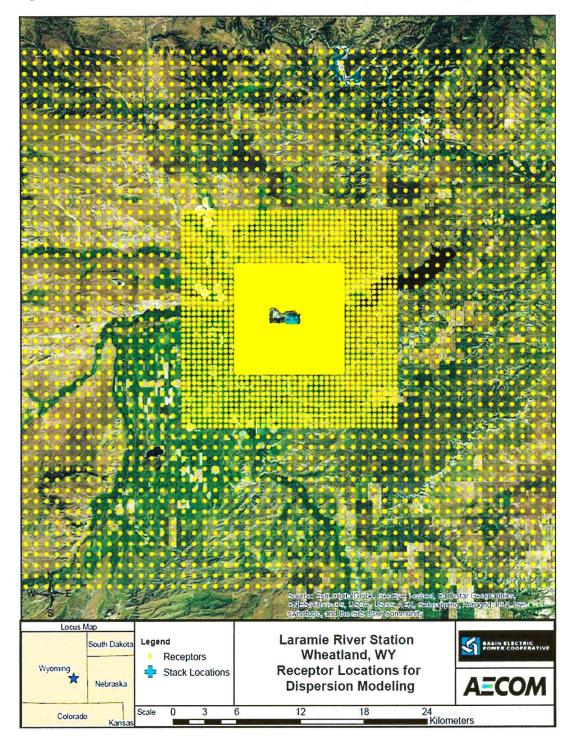
As shown in the results reported below, the extent of this grid was found to be sufficient to capture the maximum modeled impacts. Furthermore, the peak impact was in an area of receptors spaced at 100-meter intervals, so no additional fine receptor grids were necessary. Near-field and far-field receptor grid locations are shown in Figures 4-1 and Figure 4-2, respectively.

The latest version of AERMAP (version 15181), the AERMOD terrain preprocessor program, was used to calculate terrain elevations and critical hill heights for the modeled receptors at each of the project facilities using National Elevation Data (NED). The dataset was downloaded from the USGS website (<u>http://viewer.nationalmap.gov/viewer/</u>) and will consist of 1/3 arc second (~10 m resolution) NED. As per the AERMAP User's Guide, the domain was sufficient to ensure that all terrain features exceeding a 10% elevation slope from any given receptor were considered.

Section 4.2 of the TAD states that receptors can be excluded from areas where it is not feasible to place a monitor (water bodies, etc.). To be conservative, the modeling did not exclude any receptor areas outside of the fenceline out to a distance of 25 km from the plant.

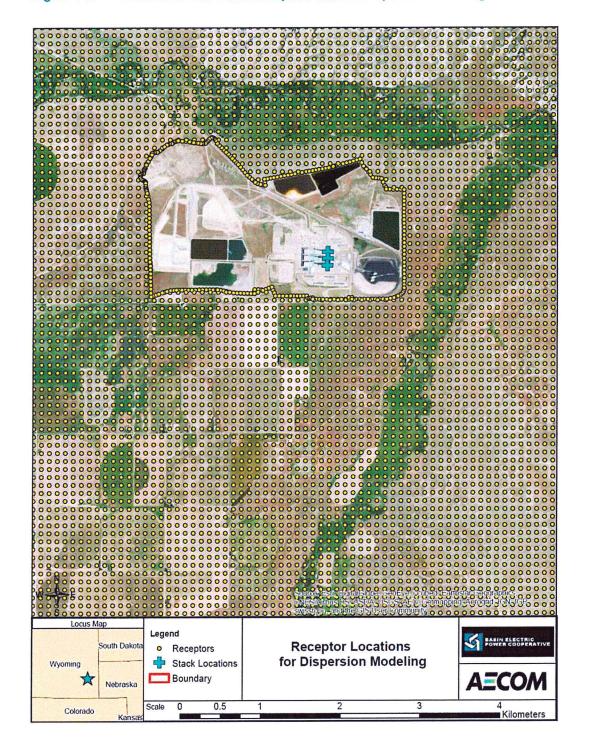
⁸ Wyoming Department of Environmental Quality/Air Quality Division Guidance for Submitting Major Source/PSD Modeling Analyses.





Prepared for: Basin Electric Project 60438665





Prepared for: Basin Electric Project 60438665

October 2016 AECOM

4.3 Meteorological Data for Modeling

Meteorological data required for AERMOD include hourly values of wind speed, wind direction, and ambient temperature. Since the AERMOD dispersion algorithms are based on atmospheric boundary layer dispersion theory, additional boundary layer variables are derived by parameterization formulas, which are computed by the AERMOD meteorological preprocessor, AERMET. These parameters include sensible heat flux, surface friction velocity, convective velocity scale, vertical potential temperature gradient, convective and mechanical mixing heights, Monin-Obukhov length, surface roughness length, Bowen ratio, and albedo.

Hourly surface observations (including 1-minute and 5-minute ASOS) were processed from Torrington Municipal Airport (Torrington, WY) per guidance from WDEQ. Concurrent upper-air data was obtained from the closest or most representative National Weather Service site, which is determined to be Riverton, WY. Additional details are provided in the following sections.

4.3.1 Available Offsite Meteorological Data and NWS Upper-Air Data

The hourly meteorological data for LRS was processed with the latest version of AERMET (Version 15181). AERMET was run utilizing three concurrent years (2013-2015) of hourly surface observations from Torrington Municipal Airport in Torrington, WY along with concurrent upper air data from Riverton, WY.

Figure 4-3 shows the location of these meteorological stations in relationship to the LRS. A wind rose for Torrington for the years 2013-2015 is shown in **Figure 4-4**.

The AERMET inputs were based on surface meteorological data from the National Climatic Data Center's (NCDC) Integrated Surface Hourly (ISH) database along with both 1-minute and concurrent 5-minute Automated Surface Observing System (ASOS) data. The latest version of AERMINUTE (version 15272) was used to process this data. The upper air data input to AERMET was downloaded from the NOAA/ESRL/GSD - RAOB database (<u>http://esrl.noaa.gov/raobs/</u>).

Table 4-1 gives the site location and information on the meteorological datasets. The surface wind data are measured 10 meters above ground level. The temperature and relative humidity are measured 2 meters above ground level.

Met Site	Latitude	Longitude	Base Elevation (m)	Data Source	Data Format
Torrington Municipal Airport, WY	42.065N	104.150W	1282.0	NCDC	ISHD, 1-min, 5-min ASOS
Riverton, WY	43.060	-108.470	1684	FSL	FSL

Table 4-1: Meteorological Data Used in AERMET for Laramie River Station

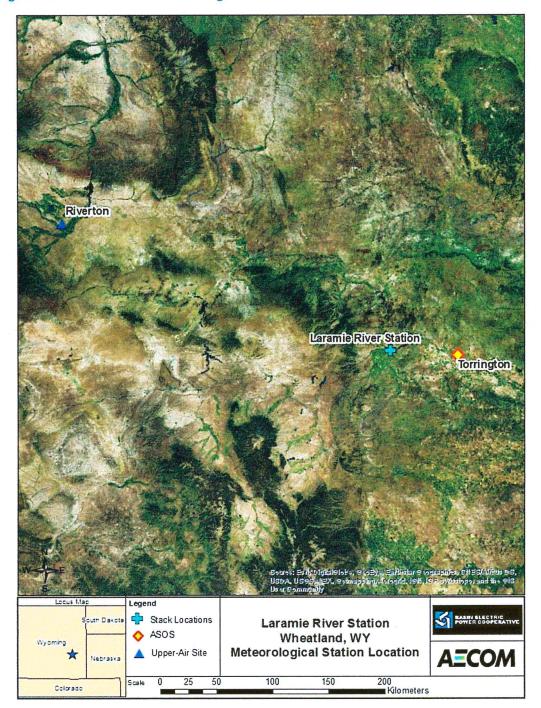


Figure 4-3: Location of Meteorological Stations Relative to Laramie River Station

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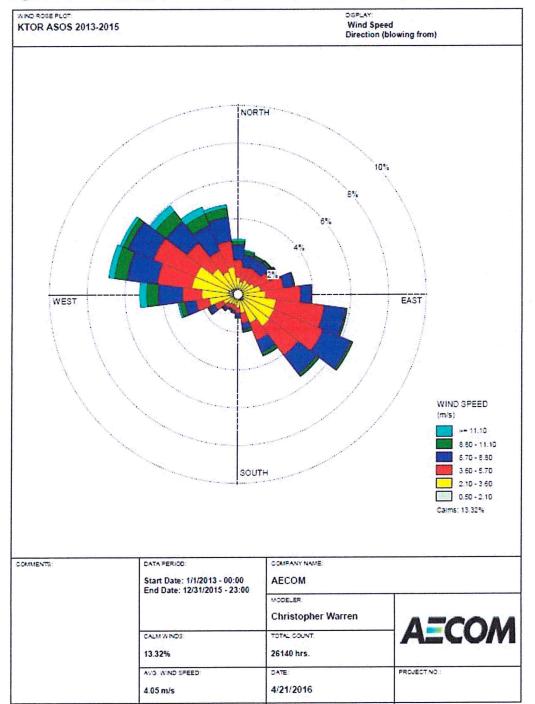


Figure 4-4: Wind Rose for Torrington Municipal Airport, Torrington, WY (KTOR)

4.3.2 AERSURFACE Analysis – Meteorological Site Land Use Characteristics

AERMET requires specification of site characteristics including surface roughness (z_o), albedo (r), and Bowen ratio (B_o). These parameters were developed according to the guidance provided by USEPA in the recently revised AERMOD Implementation Guide (AIG)⁹.

The revised AIG provides the following recommendations for determining the site characteristics:

- The determination of the surface roughness length should be based on an inverse distance weighted geometric mean for a default upwind distance of 1 kilometer relative to the measurement site. Surface roughness length may be varied by sector to account for variations in land cover near the measurement site; however, the sector widths should be no smaller than 30 degrees.
- The determination of the Bowen ratio should be based on a simple un-weighted geometric mean (i.e., no direction or distance dependency) for a representative domain, with a default domain defined by a 10-km by 10-km region centered on the measurement site.
- 3. The determination of the albedo should be based on a simple un-weighted arithmetic mean (i.e., no direction or distance dependency) for the same representative domain as defined for Bowen ratio, with a default domain defined by a 10-km by 10-km region centered on the measurement site.

The AIG recommends that the surface characteristics be determined based on digitized land cover data. US EPA has developed a tool called AERSURFACE¹⁰ that can be used to determine the site characteristics based on digitized land cover data in accordance with the recommendations from the AIG discussed above. AERSURFACE incorporates look-up tables of representative surface characteristic values by land cover category and seasonal category. The latest version of AERSURFACE (13016) version was applied with the instructions provided in the AERSURFACE User's Guide.

The current version of AERSURFACE supports the use of land cover data from the USGS National Land Cover Data 1992 archives¹¹ (NLCD92). The NLCD92 archive provides data at a spatial resolution of 30 meters based upon a 21-category classification scheme applied over the continental U.S. The AIG recommends that the surface characteristics be determined based on the land use surrounding the site where the surface meteorological data were collected. As recommended in the AIG for surface roughness, the 1-km radius circular area centered at the meteorological station site can be divided into sectors for the analysis; each chosen sector has a mix of land uses that is different from that of other selected sectors. Sectors used to define the meteorological surface characteristics for the airport anemometer site are shown in **Figure 4-5**. The land use around the airport is dominated by the same land use features present at LRS: desert shrubland and grasslands. The similarity of these dominant land use features make this meteorological site representative for use in the AERMET modeling.

4.3.2.1 Seasonal Classification

In AERSURFACE, the various land cover categories are linked to a set of seasonal surface characteristics. As such, AERSURFACE requires specification of the seasonal category for each month of the year. Each month was assigned to its default season unless evidence of snow cover

4-8

⁹ Available at http://www3.epa.gov/ttn/scram/7thconf/aermod/aermod implmtn guide 3August2015.pdf.

¹⁰ Available at http://www3.epa.gov/ttn/scram/dispersion_related.htm#aersurface.

¹¹ Available at http://edcftp.cr.usgs.gov/pub/data/landcover/states/.

changes the default season to winter with snow. The following five seasonal categories, as offered by AERSURFACE, include:

- Midsummer with lush vegetation;
- Autumn with un-harvested cropland;
- Late autumn after frost and harvest, or winter with no snow;
- · Winter with continuous snow on ground; and
- Transitional spring with partial green coverage or short annuals.

The following seasonal classifications were used:

June, July, August = Midsummer with lush vegetation;

September, October = Autumn with un-harvested cropland;

April, May = Transitional spring with partial green coverage or short annuals;

November, December, January, February, March = Late autumn after frost and harvest, or winter with no snow; and

November, December, January, February, March = Winter with continuous snow on ground.

For the months of November, December, January, February, and March, locally-representative snow cover data records were reviewed for sites near the plant. For each month, if the month had more than 50% of the days with a measurable snow depth, then the month was considered "Winter with continuous snow on ground". Otherwise, the month was considered "Late autumn after frost and harvest, or winter with no snow". Based on daily snow depth data from Old Fort Laramie, WY, there were no months with 50% or more days with a measureable snow depth. Therefore, all months were processed as winter with no snow.

4.3.2.2 Surface Moisture Determination

For Bowen ratio, the land use values are linked to three categories of surface moisture corresponding to average, wet and dry conditions. The surface moisture condition for the site may vary depending on the meteorological data period for which the surface characteristics will be applied. AERSURFACE applies the surface moisture condition for the entire data period. Therefore, if the surface moisture condition varies significantly across the data period, then AERSURFACE can be applied multiple times to account for those variations. As recommended in AERSURFACE User's Guide, the surface moisture condition for each month was determined by comparing precipitation for the period of data to be processed to the 30-year climatological record, selecting "wet" conditions if precipitation is in the upper 30th-percentile, "dry" conditions if precipitation is in the lower 30th-percentile, middle 40th-percentile. The 30-year precipitation data set used in this modeling was taken from Torrington Experimental Farm (1986-1997) and Torrington Municipal Airport (1998-2015).

As part of the AERSURFACE processing, the user is required to provide whether the site is in an arid region. WDEQ has historically used a long-term average of approximately nine inches or less of annual precipitation to be an arid region. Therefore, if the annual precipitation meets this threshold, the input to AERSURFACE would be labeled as being arid. For the years 2013 through 2015, the annual precipitation was 13 inches or greater. Therefore, none of these years were processed as arid.

4.3.3 AERMET Data Processing

AERMET (Version 15181) and AERMINUTE (Version 15272) were used to process data required for input to AERMOD. Boundary layer parameters used by AERMOD, which also are required as input to the AERMET processor, include albedo, Bowen ratio, and surface roughness. The land classifications and associated boundary layer parameters were determined following procedures outlined below. In running AERMET, the observed airport hourly wind direction was randomized based on guidance from EPA's March 8, 2013 "Use of ASOS Meteorological Data in AERMOD Dispersion Modeling" memo. The randomization method addresses the lack of precision in wind direction observations, which are reported to the nearest 10 degrees, resulting in overly conservative model impacts along wind directions that are multiples of 10 degrees.

AERMET was applied in default mode to create two meteorological data files required for input to AERMOD:

- **SURFACE**: A file with boundary layer parameters such as sensible heat flux, surface friction velocity, convective velocity scale, vertical potential temperature gradient in the 500-meter layer above the planetary boundary layer, and convective and mechanical mixing heights. Also provided are values of Monin-Obukhov length, surface roughness, albedo, Bowen ratio, wind speed, wind direction, temperature, and heights at which measurements were taken.
- **PROFILE**: A file containing multi-level meteorological data with wind speed, wind direction, temperature, sigma-theta (σ_{θ}) and sigma-w (σ_{w}) when such data are available. For LRS, the profile file will contain a single level of wind data (10 meters) and the temperature data only, corresponding to the Douglas airport observation.

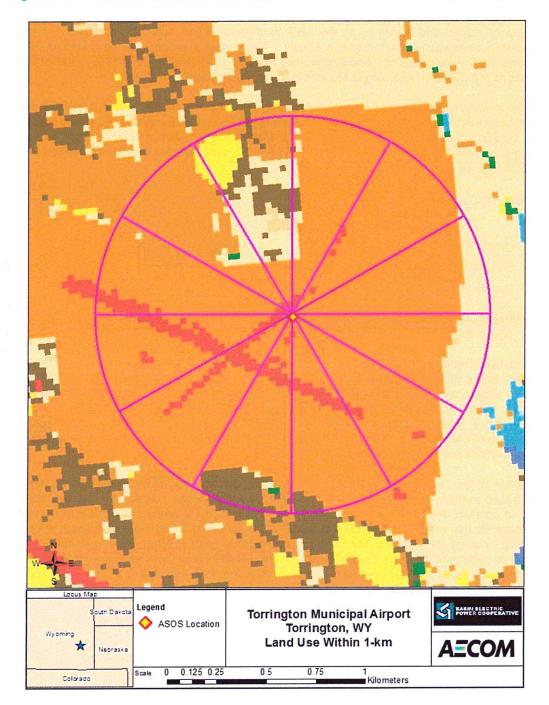


Figure 4-5: Sectors to be used for Surface Characteristics at the Torrington Airport

Prepared for: Basin Electric Project 60438665

4.3.4 Good Engineering Practice Stack Height Analysis

A Good Engineering Practice (GEP) stack height analysis¹² was performed based on the current geometry of stacks and buildings at the LRS to determine the potential for building-induced aerodynamic downwash for all modeled stacks. The analysis procedures described in EPA's Guidelines for Determination of Good Engineering Practice Stack Height (EPA 1985), Stack Height Regulations (40 CRF 51), and current Model Clearinghouse guidance was used.

The GEP formula height is based on the observed phenomena of disturbed atmospheric flow in the immediate vicinity of a structure resulting in higher ground level concentrations at a closer proximity to the building than would otherwise occur. It identifies the minimum stack height at which significant aerodynamic downwash is avoided. The GEP formula stack height, as defined in the 1985 final regulations, is calculated from:

$$H_{GEP} = H_{BLDG} + 1.5L$$

Where:

- H_{GEP} is the maximum GEP stack height;
- H_{BLDG} is the height of the nearby structure; and
- L is the lesser dimension (height or projected width) of the nearby structure.

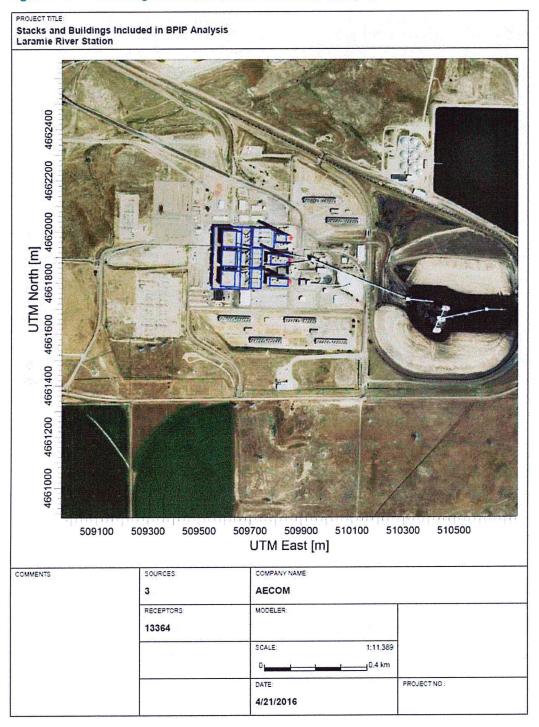
For a squat structure, i.e., height less than projected width, the formula reduces to: $H_{GEP} = 2.5H_{B}$

Both the height and width of the structure are determined from the frontal area of the structure projected onto a plane perpendicular to the direction of the wind. In all instances, the GEP stack height is based on the plane projections of any nearby building which result in the greatest justifiable height. For purposes of the GEP analysis, nearby refers to the "sphere of influence," defined as five times the height or width of the building, whichever is less, downwind from the trailing edge of the structure. In the case where a stack is not influenced by nearby structures, the maximum GEP stack height is defined as 65 meters.

The stacks at the LRS are all greater than 65 meters, but are all below the GEP formula stack height based on the formula shown above. As such, all stacks were modeled with their actual stack height. In addition, the EPA's Building Profile Input Program (BPIP-Version 04274) version that is appropriate for use with PRIME algorithms in AERMOD is used to incorporate downwash effects in the model for all modeled stacks. The building dimensions of each structure were input in BPIPPRM program to determine direction specific building data. PRIME addresses the entire structure of the wake, from the cavity immediately downwind of the building, to the far wake. **Figures 4-6** and **4-7** show the buildings and stacks input to BPIPPRM and included in AERMOD. The PBIPPRM input, output, and supplemental files are provided in Appendix B.

¹² EPA 1985. Guideline for the Determination of Good Engineering Practice Stack Height (Technical Support Document for the Stack Height Regulations) – Revised. EPA-450/4-80-023R, EPA, Research Triangle Park, NC 27711.

Figure 4-6: Buildings and Stacks Included in GEP Analysis



Prepared for: Basin Electric Project 60438665

October 2016 AECOM

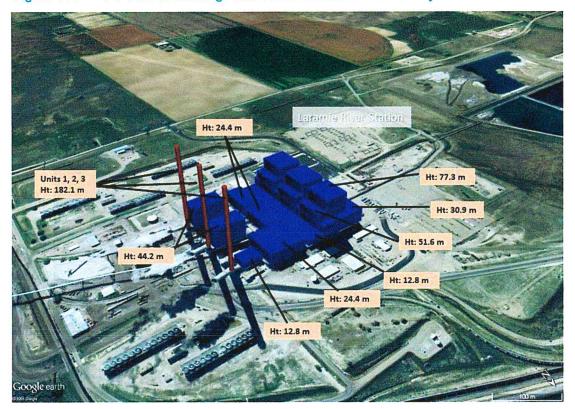


Figure 4-7: 3-D View of Buildings and Stacks Included in GEP Analysis

4.4 Nearby Sources and Ambient Background Concentrations

4.4.1 Nearby Sources to be Modeled

A review of the 2011 National Emissions Inventory (available at <u>http://www.epa.gov/ttnchie1/net/2011inventory.html</u>) indicates that there are no SO₂ sources with emissions exceeding 10 tons per year within 20 km of LRS. Accordingly, we did not model any other point sources in this SO₂ concentration characterization.

4.4.2 Regional Background Concentrations

Ambient air quality data are used to represent the contribution of non-modeled sources to the total ambient air pollutant concentrations. In order to characterize SO₂ concentrations in the vicinity of each plant, the modeled design concentration must be added to a measured ambient background concentration to estimate the total design concentration. This total design concentration is then used to characterize the area as attainment or non-attainment for the 1-hour SO₂ NAAQS. We developed seasonal and hour-of-day varying background concentrations consistent with EPA guidance in their March 1, 2011 clarification memo¹³ for use in this analysis. NCORE (Cheyenne) monitoring station concentrations observed during the recent 2012-2014 three-year period are listed in **Table 4-2** and **Table 4-3**.

¹³ <u>http://www.epa.gov/ttn/scram/guidance/clarification/Additional_Clarifications_AppendixW_Hourly-NO2-NAAQS_FINAL_03-01-2011.pdf</u>

Table 4-2:		NCORE Stati	ion 99th	Percentile H	le Hour o	Hour of the Day	and by S	' and by Season Concentrations (μ g/m ³), Hours 0-11	Icentration	s (µg/m³),	Hours 0-1	-
AVG	0:00	1:00	2:00	3:00	4:00	5:00	6:00	7:00	8:00	9:00	10:00	11:00
Winter	1.48	1.31	1.31	1.31	1.92	1.40	1.48	1.75	2.97	5.76	5.33	6.81
Spring	1.05	1.31	1.31	1.22	1.05	1.40	2.18	3.06	6.72	8.65	5.94	3.58
Summer	4.54	4.02	3.14	1.66	1.66	1.31	6.38	10.39	7.07	6.90	6.38	4.54
Fall	1.83	2.71	3.06	2.18	2.18	2.27	1.92	2.62	8.03	7.77	8.73	7.42

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NCORE Station 99th Percentile Hour of the Day and by Season Concentrations (µg/m³), Hours 12-23 Table 4-3:

							a					
AVG	12:00	13:00	14:00	15:00	16:00	17:00	18:00	19:00	20:00	21:00	22:00	23:00
Winter	5.68	5.15	4.45	3.93	3.67	2.10	2.10	2.10	1.92	1.75	1.48	1.48*
Spring	2.97	1.83	2.79	2.71	2.88	2.18	3.06	3.14	5.07	3.58	3.41	3.41*
Summer	2.71	2.53	2.10	3.32	3.32	2.79	4.98	5.68	2.71	3.49	4.19	3.67
Fall	5.07	4.54	4.10	2.71	3.32	3.23	3.67	3.14	3.14	2.97	2.62	2.01
* NOTE: WE	VDEQ perfe	ormed cali	bration che	ecks every	day on hot	lay on hour 23 (24th	hour) until	May 7, 2012	2, so no data	May 7, 2012, so no data is available for this hour before	for this hou	r before

that date. The higher of the 99th percentile of the hour before and the hour after (22:00, 0:00) was used as the 99th percentile for this missing hour.

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5. SO₂ Characterization Modeling Results

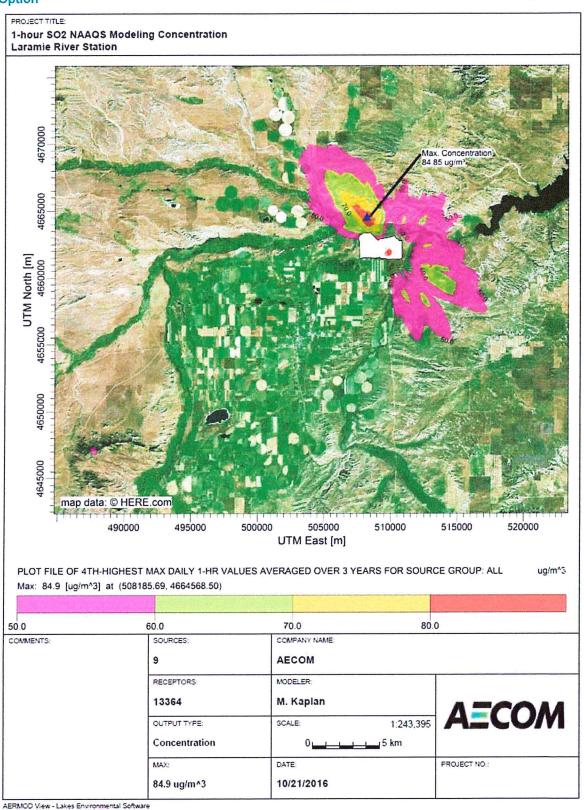
The modeled concentrations from the AERMOD modeling were calculated based on the form of the 1hour SO₂ NAAQS, with inclusion of regional background concentrations as agreed to in the final protocol. The modeling was conducted with the EPA default option and the concentration isopleths are plotted in **Figure 5-1**. The figure indicates that there is a peak area northwest of LRS. The areas of peak impact occur on relatively flat terrain approximately 3 kilometers NW of the fenceline in an area of 100-m spaced receptors.

Table 5-1 shows the NAAQS compliance modeling results of LRS and monitoring background combined. The total concentration is less than 50% of the NAAQS. This modeling analysis supports the designation of the area in the vicinity of LRS as being in attainment of the 1-hour SO₂ NAAQS by a wide margin. Due to the fact that the design value is less than 50% of the SO₂ NAAQs, the SO₂ DRR indicates that Section 51.1205(b) allows for termination of the WDEQ's reporting requirement for tracking ongoing SO₂ NAAQS compliance for LRS. However, since LRS reports emissions from its continuous emission monitors, WDEQ can continue to track LRS emission trends. Due to the large margin of modeled NAAQS attainment demonstrated in this report, future modeling is not expected to be required to verify maintenance of the SO₂ NAAQS attainment in the vicinity of LRS.

Table 5-1 AERMOD Modeled Design SO₂ Concentration from LRS including Background Concentration

Modeling Option	LRS Modeled Design Concentration (µg/m³)	Background Design Concentration from Cheyenne (μg/m ³)	Total Design Concentration (μg/m³)	NAAQS (μg/m³)
Default	78.48	6.37	84.85	196.5





Appendix A: BEPC Response to EPA Region 8 Comments

Basin Electric Power Cooperative Responses to EPA Region 8 Comments Dated June 28, 2016 on:

April 2016 Modeling Protocol for Basin Electric: SO2 Characterization for the Laramie River Station

EPA overarching comment:

We appreciate the opportunity to review and provide comments on the 1-hour Sulfur Dioxide (SO2) Data Requirements Rule (DRR) modeling protocol for the Basin Electric Laramie River Station (LRS). We have outlined some recommendations for consideration. Addressing these areas during the modeling protocol stage will assist us in determining whether all components of the analysis align with EPA guidance for the SO2 DRR modeling analysis. We look forward to continuing our discussions related to these areas and determining a path forward that works for all groups.

BEPC response: None needed.

EPA Comment #1:

Non-Regulatory Default Options [page 3-1]: The modeling protocol states that LRS will initially use default options, but reserves the right to amend the selection of AERMOD technical options to include low wind options if EPA incorporates these features in their finalization of the Appendix W changes. EPA supports and recommends the use of the default options. The finalization of the low wind options proposed in the Appendix W Revisions is unclear at this point. Therefore, if LRS decides to use the low wind options, or other non-regulatory default options, before the finalization of the Appendix W Revisions, EPA would like to note that the use of any non-regulatory default options requires review by the EPA Regional Office and concurrence with the Model Clearinghouse prior to approval. This process for approval and any changes to the modeling approach outlined in the modeling protocol would need to be completed prior to commencing the final modeling and before the January 13, 2017 deadline set for States to submit to EPA final modeling analyses for the DRR sources.¹

BEPC response: At the time of the protocol, it was expected that the final rule on Appendix W would be available in early July. With a several-month delay, it is likely that there will not be any timely action on EPA's part to add their proposed low wind options as default options to AERMOD. BEPC notes that the use of the low wind options is not critical for showing a satisfactory attainment demonstration, so with the use of AERMOD version 15181, the default options will be used and the protocol will be changed to reflect this, and will remove discussion of AERMOD low wind options. However, BEPC supports EPA's eventual adoption of the low wind options as proposed by EPA, especially with the favorable evaluation outcome for these options in an evaluation study for North Dakota sources as documented by Paine et al. (2015) in a peer-reviewed paper².

EPA Comment #2:

Status of AERMOIST [page 3-1]: The modeling protocol notes that another technical option that will not be initially used, but could be considered to account for stacks with moist plumes is "AERMOIST". The protocol explains that this option is a plume rise technique for stacks with moist plumes (i.e., those using wet or dry flue gas desulfurization, such as the LRS sources), and is a source characterization approach that does not change the model, but rather accounts for the increased heat of condensation inherent in these plumes. For these reasons, the protocol considers this approach as a source characterization rather than a non-guideline model application, thereby regarding AERMOIST as a refinement not subject to Appendix W Section 3.2.2 procedures which does not require agency approval. At this point, EPA does not agree with the description and status of AERMOIST included in the modeling protocol.

¹ See 40 CFR 51.1203(d)(3).

² Paine, R., O. Samani, M. Kaplan, E. Knipping and N. Kumar (2015) Evaluation of low wind modeling approaches for two tall-stack databases, Journal of the Air & Waste Management Association, 65:11, 1341-1353, DOI: 10.1080/10962247.2015.1085924

EPA has received multiple requests nationally, including the Laramie River Station request, to utilize AERMOIST in regulatory air quality modeling applications using AERMOD. As a result, EPA has been reviewing the various requests for its application and the impacts on the predicted results. While theoretically sensible, the application of AERMOIST does impact plume rise and dispersion. In some cases evaluated by EPA, AERMOIST significantly impacts the model predictions. Given the national implications, EPA has determined that AERMOIST warrants additional review by the EPA Regional Offices and concurrence with the Model Clearinghouse prior to approval. Until EPA completes its evaluation and subsequently approves it for regulatory use on a case-by-case basis, AERMOIST should not be used in a regulatory context.

Given this information, EPA recommends modifying the modeling protocol to exclude the use of AERMOIST at this time. AERMOIST may be considered if/when EPA's evaluation supports the approval for regulatory use in AERMOD.

BEPC response: The characterization of how EPA would treat AERMOIST was based upon verbal comments from OAQPS in the period leading up to the protocol development, as well as the written acceptance of a similar source characterization technique, "AERLIFT". Note that in Appendix C of the Laramie River Station protocol, we provided a Region IV approval of AERLIFT for Eastman Chemical. In that approval, EPA indicated that AERLIFT was a "source characterization technique" and not an integral part of the AERMOD modeling system. Therefore, according to EPA, AERLIFT was NOT subject to non-guideline provisions in Appendix W's Section 3.2.2. Therefore, it is puzzling as to why EPA Region VIII's position is inconsistent with this prior approval, and that change in position has not been adequately explained by EPA.

BEPC welcomes EPA's continued review of AERMOIST, which EPA admits is a "theoretically sensible" approach. Since none of the AERMOD evaluation databases documented in the evaluation report authored by Paine et al.³ involved a source with a moist plume, AERMOD's current treatment of moist plumes has important limitations.

Due to the importance of this feature for LRS and EPA's continued review of the procedure, BEPC elects not to remove this appropriate technique from the protocol. However, BEPC will provide conservative results without AERMOIST as an initial modeling approach and continues to reserve the right to also provide results with AERMOIST included to present more accurate modeling. BEPC remains hopeful that EPA will eventually approve AERMOIST as an appropriate source characterization technique and will work with the AERMOIST model developer to assist in its review.

EPA Comment #3:

Receptor Network [page 4-1]: We recommend providing spatial maps of the receptor networks to better understand the receptor locations and their positions relative to the sources, the fence lines, or other important features. We recommend providing this information with the modeling protocol to assist in better understanding the receptor layout and ensure that a proper receptor network is used for the modeling analysis.

BEPC response: The revised protocol has been changed to include the requested figures of the receptor networks.

EPA Comment #4:

Receptor Exclusions [page 4-1]: The protocol describes an initial receptor grid that does not exclude any receptors outside of the LRS property. We support this initial receptor grid, and recommend adding text to state that the results from this grid will be provided to the agency reviewers in the model assessment report. The protocol also states that "the receptor networks may be adjusted to remove receptors in areas where monitor placement would not be feasible, as discussed in Section 3." While we agree that receptors in

³ https://www3.epa.gov/ttn/scram/7thconf/aermod/aermod_mep.pdf.

areas where monitor placement would not be feasible can be excluded based on the current EPA SO₂ NAAQS Designations Modeling Technical Assistance Document [dated: February 2016], these exclusions should be discussed with the agency reviewers and justified in the modeling protocol prior to commencing the final modeling. Therefore, we recommend adding text to this section stating that these exclusions will be discussed with the agency reviewers and justified in the modeling protocol prior to commencing the final modeling and before the State deadline of January 13, 2017 to submit a final modeling analysis.

BEPC response: We agree that it would be appropriate to add the suggested text in the protocol to discuss and justify any receptor areas to be excluded with EPA prior to commencing the final modeling.

EPA Comment #5:

AERMET Data Processing [page 4-7]: The protocol states that the observed airport hourly wind direction will be randomized during the AERMET processing. It is not clear what this statement means. We recommend adding text to explain what this means and how it aligns with EPA's air quality modeling guidance.

BEPC response: In running AERMET, the observed airport hourly wind direction (if used to substitute for missing AERMINUTE data) will be randomized based on guidance from EPA's March 8, 2013 "Use of ASOS Meteorological Data in AERMOD Dispersion Modeling memo⁴. The randomization method addresses the lack of precision in the NWS wind direction observations, which are reported to the nearest 10 degrees. If the randomization method were not used, then the potential would exist for overly conservative model impacts to occur along wind directions that are multiples of 10 degrees.

EPA Comment #6:

Building Downwash [page 4-9]: We recommend providing the building dimensions during the model protocol stage to ensure that disparities do not occur during the modeling efforts.

BEPC response: The revised modeling protocol will contain the requested information about building dimensions to be used in the modeling.

3

⁴ Available at https://www3.epa.gov/scram001/guidance/clarification/20130308 Met Data Clarification.pdf.

Basin Electric Power Cooperative Responses to EPA Region 8 Comments Dated September 1, 2016 on:

Revised July 2016 Modeling Protocol for Basin Electric: SO2 Characterization for the Laramie River Station

EPA overarching comment:

We continue to appreciate the opportunity to review and provide comments on the 1-hour Sulfur Dioxide (SO₂) Data Requirements Rule (DRR) modeling protocol for the Basin Electric Laramie River Station (LRS). We have outlined some additional recommendations for consideration. We look forward to continuing our discussions related to these areas and determining a path forward that works for all groups.

BEPC response: None needed.

EPA Comment #1:

Applicable EPA Air Quality Modeling Guidance [pages 1-1, 1-2, 3-1, 4-1]: EPA has recently updated the SO₂ NAAQS Designations Modeling Technical Assistance Document (August 2016)1 (Modeling TAD) to clarify the placement of receptors (pages 8 to 9) and the minimum number of years for the emissions and meteorological data (page 10) for the modeling option of the DRR. In particular, the areas to consider for receptor placement are those areas that would be considered ambient air relative to each modeled facility, including other facilities' property. Further, a minimum of the most recent three years of emissions and meteorological data should be used for the modeling. Therefore, we recommend updating the reference to the Modeling TAD in sections 1.1, 3.0, and 4.2 of the modeling protocol to reflect the revised Modeling TAD guidance.

BEPC Response: Basin Electric is not excluding any receptors outside of the facility fenceline and we are using three years of meteorological data as stated in the TAD. Therefore, no changes to the proposed modeling procedures are required. The reference on page 1-1 to the newer version of the TAD will be updated.

EPA Comment #2:

Discussion of AERMOIST [page 3-1]: We continue to have concerns with the discussion of AERMOIST, and we continue to disagree with the description of AERMOIST that is included in the modeling protocol given the current status of EPA's review of this approach. If the inclusion of AERMOIST is necessary for the modeling protocol, we recommend excluding the current AERMOIST discussion and simply stating that: "AERMOIST may be considered in this modeling analysis if EPA's evaluation supports the approval for regulatory use in AERMOD. While the initial modeling is not considering AERMOIST, any changes to the modeling methodology to incorporate this approach will be documented and conducted in consultation with the reviewing agencies (the appropriate State and EPA Regional Representatives)."

BEPC response: Basin Electric will incorporate the second sentence, "While the initial modeling is not considering AERMOIST, any changes to the modeling methodology to incorporate this approach will be documented and conducted in consultation with the reviewing agencies (the appropriate State and EPA Regional Representatives)." into the 2nd paragraph on page 3-1.

EPA Comment #3:

Receptor Exclusions [page 4-1]: We continue to have concerns with the protocol's description of the receptor grid and potential receptor exclusions. Given the revised Modeling TAD (explained above) and the specific changes made to the receptor exclusion discussion, we recommend updating the text in the last paragraph of page 4-1 (Section 4.2) to reference and reflect the revised Modeling TAD regarding receptor exclusions. We also continue to recommend adding text to this section stating that any receptor exclusions will be discussed with the agency reviewers and justified in the modeling protocol prior to commencing the final modeling analysis.

BEPC response: Basin Electric will incorporate the suggested text into Section 4.2. At this point, we do not plan to exclude receptors outside the plant fenceline.

EPA Comment #4:

Description of ADJ_U* [page 4-10]: The modeling protocol states that AERMET will use default options, but reserves the right to use ADJ_U*. If finalized in the Appendix W changes later in 2016, we support the use of the ADJ_U* option. However, we recommend adding text to this paragraph stating that any changes to the proposed modeling approach, including model platforms, input assumptions, and configuration options, will be documented and conducted in consultation with the reviewing agencies (the appropriate State and EPA Regional Representatives).

BEPC response: Basin Electric will incorporate the suggested text into page 4-10.

Kaplan, Mary

From:	Cris Miller <cmiller@bepc.com></cmiller@bepc.com>	
Sent:	Wednesday, October 19, 2016 6:35 AM	
То:	Paine, Bob; Kaplan, Mary	
Subject:	Fwd: [External] Fwd: September 30 LRS Protocol	

With the approval of the revised modeling protocol, Please proceed with modeling LRS...Cris Sent from my iPhone

Begin forwarded message:

From: Josh Nall <josh.nall@wyo.gov> Date: October 18, 2016 at 5:02:54 PM EDT To: Cris Miller <<u>cmiller@bepc.com</u>> Cc: Nathan Henschel <<u>nathan.henschel@wyo.gov</u>> Subject: [External] Fwd: September 30 LRS Protocol

Cris, I've forwarded an e-mail from Rebecca M. at EPA Region 8 that indicates that the latest version of the LRS DRR modeling protocol aligns with EPA's guidance and that the dispersion modeling may proceed. Please let me know if you have any questions. We look forward to receiving your submittal of the final modeling analysis. Thanks, Josh.

James (Josh) Nall NSR Permitting Supervisor Wyoming Dept. of Environmental Quality – Air Quality Division 200 W. 17th Street, 3rd Floor Cheyenne, WY 82002 (307) 777-7816

------ Forwarded message ------From: **Matichuk, Rebecca** <<u>Matichuk.Rebecca@epa.gov</u>> Date: Tue, Oct 18, 2016 at 2:15 PM Subject: RE: September 30 LRS Protocol To: Josh Nall <<u>josh.nall@wyo.gov</u>> Cc: "Clark, Adam" <<u>Clark.Adam@epa.gov</u>>

Hi Josh,

Thank you for providing the additional information and updating the modeling protocol to address our comments on Wyoming's 1-hour SO2 DRR Modeling Protocol for the Laramie River Station. Based on our review of the Modeling Protocol dated September 2016, the State's approach to conducting the dispersion modeling for EPA's SO2 DRR aligns with EPA's guidance, and sufficient information has been

provided to EPA Region 8 for the State to proceed with the dispersion modeling using the methodology outlined in this document. Please keep us informed of any changes to current methodology.

Again, we appreciate the time taken to coordinate your efforts with us. Please let us know if you have any questions, or if any issues occur during the modeling efforts that you would like to discuss.

Thank you,

Rebecca

Rebecca Matichuk, PhD

U.S. Environmental Protection Agency

Region 8 - Air Program

Indoor Air, Transportation and Toxics Unit

1595 Wynkoop Street

Denver, CO 80202

Office Number: 303-312-6867

Fax Number: 303-312-6064

From: Josh Nall [mailto:josh.nall@wyo.gov] Sent: Friday, October 07, 2016 7:53 AM To: Clark, Adam <<u>Clark.Adam@epa.gov</u>> Subject: Re: September 30 LRS Protocol

Adam, I've attached the electronic version of the LRS protocol. Let me know if you need anything else. Thanks, Josh.

James (Josh) Nall

NSR Permitting Supervisor Wyoming Dept. of Environmental Quality – Air Quality Division 200 W. 17th Street, 3rd Floor Cheyenne, WY 82002 (307) 777-7816

On Thu, Oct 6, 2016 at 4:26 PM, Clark, Adam <<u>Clark.Adam@epa.gov</u>> wrote:

HI Josh – I received a physical copy of the new LRS protocol today. Thanks for sending that along. Do you have an electronic copy of it? If so, please email it to me. Thanks!

Adam Clark

Air Program

EPA Region 8

303.312.7104

E-Mail to and from me, in connection with the transaction of public business, is subject to the Wyoming Public Records Act and may be disclosed to third parties.

E-Mail to and from me, in connection with the transaction of public business, is subject to the Wyoming Public Records Act and may be disclosed to third parties. Revised Modeling Protocol for Basin Electric: SO2 Characterization for the Laramie River Station

X

Appendix B: Building Dimension Files used in Laramie River Station Dispersion Modeling Analysis

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8	-	509547.69	4661777.58
9		509556.15	4662019.72
10		509700.84	4662014.67
11		509692.38	4661772.53
12	4	30.94	
13		509547.69	4661777.58
14		509556.14	4662019.72
15		509664.28	4662015.95
16		509655.82	4661773.81
17	4	51.59	1001001
18		509587.52	4661941.81
19 20		509589.67 509663.84	4662003.49 4662000.90
20		509661.69	4661939.22
22	4	51.59	4001939.22
23	г	509585.19	4661865.27
24		509587.35	4661926.95
25		509661.52	4661924.36
26		509659.36	4661862.68
27	4	51.59	
28		509581.97	4661786.35
29		509584.12	4661848.03
30		509658.30	4661845.44
31		509656.14	4661783.76
32	4	77.34	
33		509587.52	4661941.81
34		509589.67	4662003.49
35		509643.89	4662001.60
36	4	509641.74	4661939.92
37	4	77.34 509585.19	4661865.27
38 39		509585.19	4661926.95
40		509641.57	4661925.06
41		509639.41	4661863.37
42	4	77.34	4001003.57
43	1	509581.97	4661786.35
44		509584.13	4661848.03
45		509638.35	4661846.14
46		509636.20	4661784.46
47	'BLD 2'	1 1390.50	
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49		509773.94	4661788.34

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51			509846.60	4661821.18		
52		-	509845.37	4661785.85		
53	'BLD_3'	1	1390.50			
54	4		44.20			
55			509777.12	4661873.19		
56			509778.35	4661908.53		
57			509849.78	4661906.04		
58			509848.55	4661870.70		
59	'BLD_4'	1	1390.50			
60	4		24.38			
61			509700.82	4661778.89		
62			509703.46	4661854.39		
63			509741.99	4661853.04		
64			509739.36	4661777.55		
65	'BLD_5'	1	1390.50			
66	4		24.38			
67			509703.96	4661859.16		
68			509706.59	4661934.65		
69			509745.13	4661933.31		
70			509742.49	4661857.81		
71	'BLD_6'	1	1 <mark>390.5</mark> 0			
72	$\overline{4}$		24.38			
73			509706.28	4661937.86		
74			509708.94	4662014.15		
75			509792.30	4662011.24		
76			509789.64	4661934.95		
77	'BLD_7'	1	1390.50			
78	4		12.80			
79			509795.99	4661957.00		
80			509797.12	4661989.34		
81			509839.68	4661987.85		
82			509838.55	4661955.51		
83	3					
84	'STCK1'		1391.11	182.12	509853.00	
	4661802.	71				
85	'STCK2'		1391.11	182.12	509855.01	
	4661887.	99				
86	'STCK3'		1391.11	182.12	509857.44	
	4661973.2	27				

J:\AQES\Projects\Basin Electric\Laramie 1 River\400-Technical\402-Lake 2 BPIP (Dated: 04274) 3 4 DATE : 9/26/2014 5 TIME : 10:16:34 J:\AQES\Projects\Basin Electric\Laramie 6 River\400-Technical\402-Lake 7 8 _____ 9 BPIP PROCESSING INFORMATION: 10 _____ 11 flag has been set for preparing downwash related data 12 The P for a model run utilizing the PRIME algorithm. 13 14 15 will be converted to meters using Inputs entered in METERS 1.0000. Output will be in meters. 16 a conversion factor of 17 18 The UTMP variable is set to UTMY. The input is assumed to be in 19 UTM coordinates. BPIP will move the UTM origin to the first pair of UTM coordinates read. The UTM coordinates of the new origin 20 will be subtracted from all the other UTM coordinates entered to 21 form 22 this new local coordinate system. 23 24 Plant north is set to 0.00 degrees with respect to True North. 25 26 27 J:\AQES\Projects\Basin Electric\Laramie River\400-Technical\402-Lake 28 29 30 PRELIMINARY* GEP STACK HEIGHT RESULTS TABLE 31 32 (Output Units: meters) 33 Preliminary* 34 Stack-Building 35 Base Elevation GEP** GEP Stack Stack Stack Height Value 36 Name Differences EQN1 Height 37 38 192.74 192.74 39 182.12 0.61 STCK1 192.74 192.74 40 STCK2 182.12 0.61 0.61 192.74 192.74 182.12 41 STCK3 42 43 * Results are based on Determinants 1 & 2 on pages 1 & 2 of the GEP

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44	Technical S for	upport Doc	ument.	Determina	ant 3 mag	y be inv	estigated
45 46	additional Determinant						after
							ma abaia a l
47	** Results wer						Technical
48	Support Doc stack-build		lues hav	e been ad	djusted :	for any	
49	base elevat		ences.				
50			011000.				
					to a Prote to a	C	
51		eria for d	etermini	ng stack	neights	ior mod	ering
	emission						
52	limitations	for a sou	rce can	be found	in Table	e 3.1 of	the
53	GEP Technic						
54		ar support	Documen				
55							
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	River\400-Techn	ical\402-L	ake				
65							
66	BPIP output is	in meters					
67							
68							
		CTCV1	44.20	44.20	44.20	44.20	44.20
69	SO BUILDHGT	SICKI	44.20	44.20	44.20	44.20	44.20
	44.20						
70	SO BUILDHGT	STCK1	44.20	77.34	77.34	77.34	77.34
	77.34						
71	SO BUILDHGT	STCK1	77.34	77.34	44.20	44.20	44.20
/ 1		DICIT	11.04	11.01	11.20	11.20	11.20
	44.20						
72	SO BUILDHGT	STCK1	44.20	44.20	44.20	44.20	44.20
	44.20						
73	SO BUILDHGT	STCK1	44.20	44.20	44.20	44.20	44.20
	44.20						
74		CILCIZ1	11 20	44.20	44.20	44.20	44.20
74	SO BUILDHGT	STCKI	44.20	44.20	44.20	44.20	44.20
	44.20						
75	SO BUILDWID	STCK1	75.70	78.91	79.71	78.09	74.10
	67.86						
76	SO BUILDWID	CTCK1	59.56	71.65	63.57	68.67	75.47
10		DICKI	55.50	11.00	03.57	00.07	10.11
	79.96						BB A A
77	SO BUILDWID	STCK1	82.04	81.61	79.35	79.51	77.26
	72.66						
78	SO BUILDWID	STCK1	75.70	78.91	79.71	78.09	74.10
	67.86						a second deservation
70		CIIICIZ 1		10 15	27 02	44.96	55.71
79	SO BUILDWID	STCKI	59.56	49.45	37.83	44.90	55./I

	64.77							
80	SO BUILDWID	STCK1	71.86	76.77	79.35	79.51	77.26	
81	72.66 SO BUILDLEN	STCK1	44.97	55.71	64.77	71.86	76.77	
82	79.35 SO BUILDLEN	STCK1	79.51	65.91	56.38	62.32	70.67	
83	76.88 SO BUILDLEN	STCK1	80.75	82.17	67.86	59.56	49.45	
84	37.83 SO BUILDLEN	STCK1	44.97	55.71	64.77	71.86	76.77	
85	79.35 SO BUILDLEN	STCK1	79.51	77.26	72.66	75.70	78.91	
86	79.71 SO BUILDLEN	STCK1	78.09	74.10	67.86	59.56	49.45	
87	37.83 SO XBADJ	STCK1	56.23	-40.54	-51.97	-61.83	-69.80	
88	-75.65 SO XBADJ	STCK1	-79.21	-269.75	-271.03	-272.65	-292.12	
89	-328.44 SO XBADJ	STCK1	-330.78	-323.07	-57.08	-46.32	-34.17	
90	-20.97 SO XBADJ	STCK1	-101.20	-15.17	-12.80	-10.03	-6.97	
91	-3.69 SO XBADJ	STCK1	-0.30	3.10	6.40	4.59	1.40	
92	-1.82 SO XBADJ	STCK1	-4.99	-8.01	-10.79	-13.23	-15.28	
93	-16.86 SO YBADJ	STCK1	54.04	40.86	38.03	34.05	29.04	
94	23.14 SO YBADJ	STCK1	16.55	55.50	13.53	-28.84	4.92	
95	27.71 SO YBADJ	STCK1	-23.07	-73.15	-35.98	-39.45	-41.72	
96	-42.73 SO YBADJ	STCK1	-54.04	-40.86	-38.03	-34.05	-29.04	
97	-23.14 SO YBADJ	STCK1	-16.55	-9.44	-2.05	5.40	12.69	
98	19.59 SO YBADJ	STCK1	25.90	31.42	35.98	39.45	41.72	
99	42.73							
100								
101	SO BUILDHGT 77.34	STCK2	44.20	44.20	44.20	44.20	44.20	
102	SO BUILDHGT 77.34	STCK2	77.34	77.34	77.34	77.34	77.34	
103	SO BUILDHGT 44.20	STCK2	44.20	44.20	44.20	44.20	44.20	
104	SO BUILDHGT 44.20	STCK2	44.20	44.20	44.20	44.20	44.20	
105	SO BUILDHGT	STCK2	44.20	44.20	44.20	44.20	44.20	

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		44.20							
1	06	SO BUILDHGT 44.20	STCK2	44.20	44.20	44.20	44.20	44.20	
1	07	SO BUILDWID	STCK2	75.70	78.91	79.71	78.09	74.10	
1	08	81.09 SO BUILDWID	STCK2	77.55	71.65	63.58	68.67	75.46	
1	09	79.96 SO BUILDWID	STCK2	71.87	76.78	79.35	79.51	77.26	
		72.66							
1	10	SO BUILDWID 67.86	STCK2	75.70	78.91	79.71	78.09	74.10	
1	11	SO BUILDWID 64.78	STCK2	59.56	49.45	37.83	44.97	55.72	
1	12	SO BUILDWID 72.66	STCK2	71.87	76.78	79.35	79.51	77.26	
1	13	SO BUILDLEN	STCK2	44.97	55.71	64.78	71.87	76.78	
1	14	78.72 SO BUILDLEN	STCK2	73.43	65.91	56.38	62.31	70.67	
1	15	76.88 SO BUILDLEN	STCK2	78.09	74.10	67.86	59.56	49.45	
		37.83							
1	16	SO BUILDLEN 79.35	STCK2	44.97	55.72	64.78	71.87	76.78	
1	17	SO BUILDLEN 79.71	STCK2	79.51	77.26	72.66	75.70	78.91	
1	18	SO BUILDLEN 37.83	STCK2	78.09	74.10	67.86	59.56	49.45	
1	19	SO XBADJ	STCK2	-28.10	-121.37	-51.76	-61.40	-69.18	
1	20	-287.28 SO XBADJ	STCK2	-291.34	-269.67	-269.82	-270.36	-288.84	
1:	21	-287.54 SO XBADJ	STCK2	-71.93	-65.01	-56.12	-45.52	49.47	
		64.31				10.00	10 45		
1:	22	SO XBADJ -4.50	STCK2	-16.87	-15.17	-13.02	-10.47	-7.60	
1:	23	SO XBADJ -3.05	STCK2	-1.26	2.02	5.23	3.36	0.16	
1:	24	SO XBADJ	STCK2	-6.17	-9.09	-11.74	-14.04	-98.91	
12	25	-102.14 SO YBADJ	STCK2	41.21	13.58	36.80	32.88	27.96	
12	26	60.29 SO YBADJ	STCK2	16.32	49.02	7.17	-34.89	-3.18	
12	27	-47.15 SO YBADJ	STCK2	-25.47	-30.79	-35.18	-38.50	-58.51	
		-44.74					~~ ~~	07 06	
1:	28	SO YBADJ -22.19	STCK2	-41.21	-39.61	-36.80	-32.88	-27.96	
12	29	SO YBADJ 19.37	STCK2	-15.74	-8.82	-1.62	5.62	12.69	
13	30	SO YBADJ	STCK2	25.47	30.79	35.18	38.50	58.51	

	44.74							
131								
132	SO BUILDHGT	amor 2	44 20	44 20	44 20	44 20	77.34	
133	77.34	STCKS	44.20	44.20	44.20	44.20	11.54	
134	SO BUILDHGT 24.38	STCK3	77.34	77.34	77.34	77.34	24.38	
135	SO BUILDHGT 44.20	STCK3	12.80	12.80		0.00	44.20	
136	SO BUILDHGT 44.20	STCK3	44.20	44.20	44.20	44.20	44.20	
137	SO BUILDHGT 24.38							
138	SO BUILDHGT 44.20					0.00		
139	SO BUILDWID 81.09							
140	SO BUILDWID 106.56							
141	SO BUILDWID 72.66					0.00		
142 143	SO BUILDWID 67.86							
143	SO BUILDWID 106.56 SO BUILDWID					0.00		
145	72.66 SO BUILDLEN						81.62	
146	78.72 SO BUILDLEN							
147	109.49 SO BUILDLEN					0.00		
148	37.83 SO BUILDLEN							
149	79.35 SO BUILDLEN				43.69	46.68	109.51	
150	109.49 SO BUILDLEN	STCK3	53.48	52.55	0.00	0.00	49.45	
151	37.83 SO XBADJ	STCK3	-112.51	-202.34	-126.83	-128.29	-331.17	
152	-332.02 SO XBADJ	STCK3	-322.79	-286.87	-269.92	-268.95	-153.53	
153	-149.04 SO XBADJ 64.74	STCK3	-56.54	-51.08	0.00	0.00	50.02	
154	64.74 SO XBADJ 40.25	STCK3	67.54	65.80	62.05	56.42	49.08	
155	40.25 SO XBADJ 39.56	STCK3	48.23	14.96	17.76	15.52	44.02	
156	SO XBADJ	STCK3	3.05	-1.46	0.00	0.00	-99.47	

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	-187.42							
157	SO YBADJ -12.35	STCK3	28.80	-13.31	-3.73	-20.07	38.66	
158	SO YBADJ -52.97	STCK3	-62.98	-34.54	-1.57	-43.52	-35.79	
159	SO YBADJ -43,99	STCK3	-26.10	-30.88	0.00	0.00	-57.85	
160	SO YBADJ	STCK3	-28.80	-12.73	3.73	20.07	35.81	
161	SO YBADJ 52.97	STCK3	-38.19	-6.05	0.85	7.71	111.41	
162	SO YBADJ 47.17	STCK3	26.10	30.88	0.00	0.00	57.85	

1 J:\AOES\Projects\Basin Electric\Laramie River\400-Technical\402-Lake 2 BPIP (Dated: 04274) 3 4 DATE : 9/26/2014 5 TIME : 10:16:34 J:\AQES\Projects\Basin Electric\Laramie 6 River\400-Technical\402-Lake 7 8 _____ 9 BPIP PROCESSING INFORMATION: 10 _____ 11 flag has been set for preparing downwash related data 12 The P 13 for a model run utilizing the PRIME algorithm. 14 15 will be converted to meters using Inputs entered in METERS a conversion factor of 1.0000. Output will be in meters. 16 17 18 The UTMP variable is set to UTMY. The input is assumed to be in UTM coordinates. BPIP will move the UTM origin to the first 19 pair of UTM coordinates read. The UTM coordinates of the new origin 20 will 21 be subtracted from all the other UTM coordinates entered to form 22 this new local coordinate system. 23 The new local coordinates will be displayed in parentheses just 24 below 25 the UTM coordinates they represent. 26 27 0.00 degrees with respect to True North. Plant north is set to 28 29 30 31 32 _____ 33 INPUT SUMMARY: 34 _____ 35 36 37 Number of buildings to be processed : 7 38 39 U1-U3 BU has 8 tier(s) with a base elevation of 1390.50 METERS 40 CORNER COORDINATES 41 BUILDING TIER BLDG-TIER TIER NO. OF NUMBER HEIGHT CORNERS Y 42 NAME NUMBER Х 43 12.80 44 U1-U3 BU 1 1 4

<pre>45 46 46 46 46 46 47 47 49 49 50 50 50 50 50 50 50 51 52 52 53 01-U3 BU 2 2 30.94 54 55 55 55 55 55 55 55 55 55 55 55 55</pre>		J.Jup	512012	.014/	10.10.00	1111			
46 (0.00 0.00) 47 meters 48 (8.46 242.14) 49 509756.15 4662014.67 50 509700.84 4662014.67 50 509700.84 4662014.67 51 509700.84 4662014.67 52 509692.38 4661772.53 53 01-03 BU 2 2 30.94 4 54 509556.14 4662019.72 55 (0.00 0.00) 56 509556.14 4662019.72 57 (8.45 242.14) 58 509556.14 4662019.72 59 (116.59 238.37) 60 8.45 242.14) meters 509664.28 4662015.95 59 (116.59 238.37) 61 509565.12 466177.81 62 01-03 BU 3 3 51.59 4 63 509587.52 4661941.81 64 509587.61 4662003.49 65 509589.67 4662003.49 66 (39.83 164.23) 67 50963.84 4662000.90 68 (116.15 223.32) 69 509661.69 466193.22 61 509661.69 466193.22 62 509661.69 466193.22<	45								4661777.58
47 509556.15 4662019.72 48 (8.46 242.14) 49 meters (153.15 237.09) 50 509502.38 4661772.53 meters 52 509592.38 4661777.58 53 01-03 BU 2 2 30.94 4 54 509547.69 4661777.58 meters 55 (144.69 -5.05) 56 509556.14 4662019.72 57 (8.45 242.14) 58 509556.14 4662015.95 59 (116.59 238.37) 60 509654.28 4662015.95 61 01-03 BU 3 51.59 62 01-03 BU 3 51.59 4 63 01-03 BU 3 51.59 4 64 (108.13 -3.77) 62 01-03 BU 3 51.59 4 63 01-03 BU 3 51.59 4 64 01-03 BU 3	46								0.00)
48 meters (8,46 242.14) 49 50970.84 4662014.67 50 (153.15 237.09) 51 509692.38 4661772.53 52 (144.69 -5.05) 53 U1-U3 BU 2 2 30.94 4 54 509507.38 4661777.58 meters 55 (0.00 0.00) meters 56 509565.14 4662019.72 57 6 (116.59 238.37) 60 509664.28 4662015.95 59 (116.59 238.37) 60 6 (108.13 -3.77) 61 meters (108.13 -3.77) 62 U1-U3 BU 3 51.59 4 63 509567.52 4661941.81 meters 64 509589.67 4662003.49 meters 65 509589.67 4662003.49 meters 66 (11.98 225.91) meters 509561.69 4662000.90 68 (11.915 223.32) m								meters	1660010 70
48 (8.46 242.14) 49 50 50 (153.15 237.09) 51 509602.38 4661772.53 52 (144.69 -5.05) 53 U1-U3 BU 2 2 30.94 4 54 509502.38 4661772.53 55 (0.00 0.00) 56 (0.00 0.00) 57 8.45 242.14) 58 (0.00 0.00) 59 (116.59 238.37) 60 509655.82 4661773.81 61 (116.59 238.37) 62 U1-U3 BU 3 3 51.59 4 63 509565.82 4661743.81 64 (9.83 164.23) 65 (39.83 164.23) 66 (9.983 164.23) 67 (116.15 223.32) 68 (116.15 223.32) 69 (114.00 161.64)	47								4662019.72
49 509700.84 4662014.67 50 (153.15) 237.09) 51 509692.38 4661772.53 52 (144.69) -5.05) 53 U1-U3 BU 2 230.94 509595.38 4661777.58 55 (144.69) -5.05) meters 509595.14 4662019.72 56 509555.14 4662019.72 meters 509555.14 4662019.72 57 (0.00) 0.00) meters 509556.14 4662019.72 58 509665.82 4661773.81 meters 509655.82 4661773.81 60 509555.82 4661773.81 meters (116.59) 238.37) 60 509565.82 4661773.81 meters (39.83) 164.23) 61 01-03 BU 3 51.59 4 509587.52 4661941.81 62 01-03 BU 3 51.59 4 509587.52 4661941.81 63 01-03 BU 3 51.59 4 509587.52 4661941.81 64 01-03 BU 3 51.59 4	48							(8.46	242.14)
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52 (144.69 -5.05) 53 U1-U3 BU 2 2 30.94 509547.69 4661777.58 55 55 (0.00 0.00) 0.00) 56 509556.14 4662019.72 meters 57 (8.45 242.14) 58 509642.8 4662015.95 59 (116.59 238.37) 60 509655.82 4661773.81 61 meters 509655.82 4661773.81 meters (108.13 -3.77) meters (39.83 164.23) 63 509587.52 4661941.81 64 509589.67 4662003.49 65 509589.67 4662003.49 66 (116.15 223.32) 67 509663.84 466200.90 68 (116.15 223.32) 69 (116.15 223.32) 69 (114.00 161.64)	51							509692.38	4661772.53
53 U1-U3 BU 2 30.94 4 54 54 509547.69 4661777.58 55 (0.00 0.00) 56 (0.00 0.00) 57 (8.45 242.14) 58 (16.59 238.37) 59 (116.59 238.37) 60 509655.82 4661773.81 61 509655.82 4661773.81 62 U1-U3 BU 3 51.59 63 509587.52 4661941.81 64 (39.83 164.23) 65 (39.83 164.23) 66 (41.98 225.91) 67 (41.98 225.91) 68 (116.15 223.32) 69 (116.15 223.32) 69 (116.10 4661939.22 70 (114.00 161.64)	52								-5.05)
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56 509556.14 4662019.72 57 (8.45 242.14) 58 509664.28 4662015.95 59 (116.59 238.37) 60 8.45 242.14) 61 509655.82 4661773.81 62 U1-U3 BU 3 51.59 4 63 509587.52 4661941.81 meters 64 509589.67 4662003.49 meters 65 509663.84 4662000.90 meters 66 (116.15 223.32) meters 67 509661.69 4661939.22 meters 69 (114.00 161.64) 161.64)	55							(0.00	0.00)
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60 509655.82 4661773.81 61 meters (108.13) -3.77) 62 U1-U3 BU 3 51.59 4 63 3 51.59 4 509587.52 4661941.81 64 509589.67 4662003.49 meters 65 509589.67 4662003.49 meters 66 (41.98) 225.91) meters 67 509663.84 4662000.90 meters 68 (116.15) 223.32) meters 69 509661.69 4661939.22 meters 70 (114.00) 161.64)	59							(116.59	238.37)
61 (108.13 -3.77) meters 62 U1-U3 BU 3 3 51.59 4 63 509587.52 4661941.81 meters 64 509589.67 4662003.49 meters 65 509589.67 4662003.49 meters 66 (41.98 225.91) meters 67 509663.84 4662000.90 meters 68 (116.15 223.32) meters 69 509661.69 4661939.22 meters 70 (114.00 161.64)	60							509655.82	4661773.81
62 U1-U3 BU 3 51.59 4 63 509587.52 4661941.81 64 (39.83) 164.23) 65 509589.67 4662003.49 66 (41.98) 225.91) 67 509663.84 4662000.90 68 (116.15) 223.32) 69 509661.69 4661939.22 70 (114.00) 161.64)	61							(108.13	-3.77)
64 meters 64 (39.83) 164.23) 65 509589.67 4662003.49 66 (41.98) 225.91) 67 509663.84 4662000.90 68 (116.15) 223.32) 69 509661.69 4661939.22 70 (114.00) 161.64)	62	U1-U3	B BU	3	3	51.59	4		
64 (39.83 164.23) meters 509589.67 4662003.49 meters (41.98 225.91) 66 (41.98 225.91) 67 509663.84 4662000.90 meters (116.15 223.32) 68 (116.15 461939.22 69 509661.69 4661939.22 70 (114.00 161.64)	63								4661941.81
65 509589.67 4662003.49 66 (41.98 225.91) 67 509663.84 4662000.90 68 (116.15 223.32) 69 509661.69 4661939.22 70 (114.00 161.64)	64							(39.83	164.23)
66 (41.98 225.91) meters 67 67 509663.84 4662000.90 meters 68 68 (116.15 223.32) meters 69 509661.69 4661939.22 meters 70 (114.00 161.64)	65							509589.67	4662003.49
67 509663.84 4662000.90 meters 68 (116.15 223.32) meters 69 509661.69 4661939.22 meters 70 (114.00 161.64)	66							(41.98	225.91)
68 (116.15 223.32) meters 69 509661.69 4661939.22 meters 70 (114.00 161.64)	67							509663.84	4662000.90
69 509661.69 4661939.22 meters 70 (114.00 161.64)	68							(116.15	223.32)
70 (114.00 161.64)	69							509661.69	4661939.22
	70							(114.00	161.64)

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•	T						
71	U1-U3 BU	4	4	51.59	4		
72						509585.19 meters	4661865.27
73							87.69)
74						509587.35	4661926.95
75						meters (39.66	149.37)
76							4661924.36
77						meters (113.83	146.78)
78						meters 509659.36	4661862.68
79						meters (111.67	85.10)
80	U1-U3 BU	5	5	51.59	4	meters	
81	01 00 20	U U	Ū.		-	509581.97 meters	4661786.35
82						(34.28 meters	8.77)
83						509584.12	4661848.03
84						meters (36.43	70.45)
85							4661845.44
86						meters (110.61	67.86)
87							4661783.76
88						meters (108.45	6.18)
89	U1-U3 BU	6	6	77.34	4	meters	
90						509587.52 meters	4661941.81
91						(39.83 meters	164.23)
92						509589.67 meters	4662003.49
93						(41.98 meters	225.91)
94						509643.89	4662001.60
95						meters (96.20	224.02)
96						meters 509641.74	4661939.92
97						meters (94.05	162.34)

	1999					and the second	
			-			meters	
98 99	U1-U3 BU	J 7	7	77.34	4	509585.19	4661865.27
100						•	87.69)
101						meters 509587.35	4661926.95
102							149.37)
103						meters 509641.57	4661925.06
104							147.48)
105						meters 509639.41	4661863.37
106							85.79)
107	U1-U3 BU	σ	8	77.34	4	meters	
107	01-03 BC) 0	0	11.54	4	509581.97 meters	4661786.35
109						(34.28	8.77)
110						meters 509584.13	4661848.03
111						•	70.45)
112						meters 509638.35	4661846.14
113						•	68.56)
114						meters 509636.20	4661784.46
115						meters (88.51	6.88)
116						meters	
117							
118						ation of 1390.50	
119	BUILDING	G TIER B			NO. OI		COORDINATES
120	NAME	NUMBER	NUMBER	HEIGHT	CORNE	RS X	Y
121							
122	BLD_2	1	9	44.20	4		
123						meters	4661788.34
124						(226.25 meters	
125						509775.17 meters	4661823.68
126						(227.48 meters	46.10)

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• • • • •			and the second of the second of				
127						509846.60	4661821.18
128					(meters 298.91	43.60)
129					m	eters	4661785.85
130					1	meters 297.68	
						eters	0.27)
131 132							
133						ion of 1390.5	
134						CORNER	
135 136	NAME	NUMBER	NUMBER	HEIGHT	CORNERS	Х	Y
137	BLD 3	1	17	44.20	4		
138	_					509777.12	4661873.19
100					,	meters	05 (1)
139						229.43 eters	95.61)
140					10		4661908.53
						meters	
141						230.66 eters	130.95)
142						509849.78	4661906.04
143						meters 302.09	128.46)
144					m	eters	4661870.70
144						meters	40010/0./0
145					(300.86	93.12)
					m	eters	
146 147							
147	BLD 4	has 1 ti	er(s) wi	th a bas	e elevat	ion of 1390.5	0 METERS
149						CORNER	
150	NAME	NUMBER	NUMBER	HEIGHT	CORNERS	Х	Y
151		-					
152 153	BLD_4	1	25	24.38	4		4661778.89
103						meters	4001//0.09
154						153.13	1.31)
155					m	eters 509703.46	4661854.39
156					(meters 155.77	76.81)
157					m	eters 509741.99	4661853.04
158					1	meters 194.30	75.46)
200						eters	,

159							4661777.55
160						meters 191.67 eters	-0.03
161 162							
163	BLD_5	has 1 ti	ler(s) wit	ch a bas	e elevat	ion of 1390.5	0 METERS
164						CORNER	
165	NAME	NUMBER	NUMBER	HEIGHT	CORNERS	Х	Y
166	DID E	1	22	24.38	4		
167 168	BLD_5	1	33	24.30	4	509703 96	4661859.10
100						meters	4001000.10
169					(156.27	81.58
109					m	eters	01.00
170					10		4661934.65
						meters	
171					(158.90	157.07
						eters	
172						509745.13	4661933.31
						meters	
173					(197.44	155.73
					m	eters	
.74							4661857.81
						meters	
175					(194.80	80.23
					m	eters	
176							
177		haa 1 44		-h n hng		ion of 1300 5	Ο ΜΕΨΕΡς
178 179	BTD_0	nas 1 ti	Ler(S) WI	n a pas	e erevar	ion of 1390.5 CORNER	COORDINATI
180	NAME		NUMBER				Y
181	NAME	NOMDER	NOMDER	IIGTOIIT	COMBIN	21	1
182	BLD 6	1	41	24.38	4		
		-	11	21.00	-	509706.28	4661937.80
83						meters	
83							160.28
					(158.59	100.20
					(m	158.59 eters	100.20
84					(m	eters	
84						eters 509708.94 meters	4662014.15
.84						eters 509708.94	4662014.15
.84					(eters 509708.94 meters 161.25 eters	4662014.15 236.57
.84 .85 .86					(eters 509708.94 meters 161.25 eters	4662014.15 236.57
.84 .85 .86					(m	eters 509708.94 meters 161.25 eters 509792.30 meters	4662014.15 236.57 4662011.24
184 185 186 187					(m	eters 509708.94 meters 161.25 eters 509792.30	4662014.15 236.57 4662011.24
L84 L85 L86 L87 L88					(m	eters 509708.94 meters 161.25 eters 509792.30 meters 244.61 eters	4662014.15 236.57 4662011.24 233.66
L84 L85 L86 L87 L88					(m	eters 509708.94 meters 161.25 eters 509792.30 meters 244.61 eters 509789.64	4662014.15 236.57 4662011.24
183 184 185 186 187 188					(m (m	eters 509708.94 meters 161.25 eters 509792.30 meters 244.61 eters 509789.64 meters	4662014.15 236.57 4662011.24 233.66 4661934.95
184 185 186 187 188					(m (m	eters 509708.94 meters 161.25 eters 509792.30 meters 244.61 eters 509789.64	4662014.15 236.57 4662011.24 233.66 4661934.95

a.

	± .						
191							
192							
193	BLD 7	has 1 tier(s) with a	a base e	elevatio	n of 1390.5	0 METERS
194							COORDINATES
195	NAME I	NUMBER NUM	IBER HE	IGHT CO	DRNERS	X	Y
196							
197	BLD_7	1 4	9 1:	2.80	4		
198						509795.99	4661957.00
						meters	
199					(179.42)
						ers	/
200							4661989.34
						meters	
201					(211.76)
201						ers	211.707
202					inc c.		4661987.85
202						meters	4001007.00
203							210.27)
200						ers	210.217
204					meet		4661955.51
204						meters	400100.01
205							177.93)
205						290.00 ers	111.93
206					met	els	
200	Number of	atacka to b		and .	2		
207	NUMBER OF	stacks to b	e proce	ssed :	5		
		C.T.	ACK		C T A C IZ	COODDINATE	c
209						COORDINATE Y	5
210	STACK NA	ME BASE	HEIGHI		Х	Ţ	
211	amow1	1201 11	100 10	MEREDO			
212	STCK1	1391.11	182.12			4661000 71	
213						4661802.71	
214	amarzo	1201 11	100 10		305.31	25.13) meters
215	STCK2	1391.11	182.12			4661007 00	
216				, 505		4661887.99	
217	amar/2	1391.11	100 10		307.32	110.41) meters
218	STCK3	1391.11	182.12			4661070 07	
219					9857.44	4661973.27	
220				(309.75	195.69) meters
221							
222	No sta	cks have bee	en detec	ted as b	peing at	op any stru	ctures.
223							
224						_	
225		C			nary Tab.	Le	
226			(Un	its: met	ters)		
227							
228	and the second second	Sant S		Value of a surveyor			
229	StkNo: 1	Stk Name:S	STCK1	Stk Ht	: 182.12	Prelim. GE	P Stk.Ht:
	192.74						
230		GEP: BH:	77.34	PBW:	77.43		*Eqn1 Ht:
		192.74					

231 *adjusted for a Stack-Building elevation difference of 0.61 No. of Tiers affecting Stk: 1 Direction occurred: 113.75 232 Bldg-Tier nos. contributing to GEP: 233 7 234 235 StkNo: 2 Stk Name:STCK2 Stk Ht: 182.12 Prelim. GEP Stk.Ht: 236 192.74 237 GEP: BH: 77.34 PBW: 77.43 *Eqn1 Ht: 192.74 *adjusted for a Stack-Building elevation difference of 238 0.61 70.25 No. of Tiers affecting Stk: 1 Direction occurred: 239 Bldg-Tier nos. contributing to GEP: 240 8 241 242 Stk Ht: 182.12 Prelim. GEP Stk.Ht: 243 StkNo: 3 Stk Name:STCK3 192.74 GEP: BH: 77.34 PBW: 77.43 *Eqn1 Ht: 244 192.74 *adjusted for a Stack-Building elevation difference of 245 0.61 No. of Tiers affecting Stk: 1 Direction occurred: 70.25 246 Bldg-Tier nos. contributing to GEP: 247 7 248 249 250 251 Summary By Direction Table 252 (Units: meters) 253 254 255 Dominate stand alone tiers: 256 257 258 Drtcn: 10.00 259 260 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 261 192.74 Single tier MAX: BH: 44.20 PBW: 75.70 PBL: 44.97 *Wake 262 109.89 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 263 54.04 56.23 YADJ: 264 *adjusted for a Stack-Building elevation difference of 265 0.61 BldNo: 3 Bld Name:BLD 3 TierNo: 1 266 Stack Ht: 267 2 Stk Name:STCK2 StkNo: 182.12

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77.43 268 GEP: BH: 77.34 PBW: *Equation 1 Ht: 192.74 269 44.20 PBW: 75.70 PBL: 44.97 *Wake Single tier MAX: BH: 109.89 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 270 -28.10 YADJ: 41.21 271 *adjusted for a Stack-Building elevation difference of 272 0.61 273 BldNo: 3 Bld Name:BLD 3 TierNo: 1 274 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 275 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 276 Single tier MAX: BH: 44.20 PBW: 75.70 PBL: 44.97 *Wake Effect Ht: 109.89 277 Relative Coordinates of Projected Width Mid-point: XADJ: -112.51 YADJ: 28.80 278 *adjusted for a Stack-Building elevation difference of 279 0.61 280 BldNo: 3 Bld Name:BLD 3 TierNo: 1 281 282 Drtcn: 20.00 283 StkNo: 1 Stk Name:STCK1 284 Stack Ht: 182.12 285 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 78.91 PBL: 55.71 *Wake 286 Single tier MAX: BH: 44.20 PBW: 109.89 Effect Ht: 287 Relative Coordinates of Projected Width Mid-point: XADJ: -40.54 YADJ: 40.86 288 289 *adjusted for a Stack-Building elevation difference of 0.61 290 BldNo: 2 Bld Name:BLD 2 TierNo: 1 Stack Ht: 291 StkNo: 2 Stk Name:STCK2 182.12 292 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 192.74 Single tier MAX: BH: 44.20 PBW: 78.91 PBL: 55.71 *Wake 293 Effect Ht: 109.89 294 Relative Coordinates of Projected Width Mid-point: XADJ: -121.37 YADJ: 13.58 295 296 *adjusted for a Stack-Building elevation difference of 0.61 297 BldNo: 2 Bld Name:BLD 2 TierNo: 1 Stack Ht: 298 StkNo: 3 Stk Name:STCK3

182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 299 192.74 Single tier MAX: BH: 44.20 PBW: 78.91 PBL: 55.71 *Wake 300 109.89 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 301 -202.34 YADJ: -13.31 302 303 *adjusted for a Stack-Building elevation difference of 0.61 BldNo: 2 Bld Name:BLD 2 304 TierNo: 1 305 306 Drtcn: 30.00 307 Stack Ht: StkNo: 1 Stk Name:STCK1 308 182.12 309 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 44.20 PBW: 79.71 PBL: 64.77 *Wake 310 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 311 -51.97 YADJ: 38.03 312 *adjusted for a Stack-Building elevation difference of 313 0.61 BldNo: 2 Bld Name:BLD 2 TierNo: 314 1 315 2 Stk Name:STCK2 Stack Ht: StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 316 192.74 Single tier MAX: BH: 44.20 PBW: 79.71 PBL: 64.78 *Wake 317 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 318 -51.76 YADJ: 36.80 319 *adjusted for a Stack-Building elevation difference of 320 0.61 BldNo: 3 Bld Name:BLD 3 TierNo: 1 321 Stack Ht: StkNo: 3 Stk Name:STCK3 322 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 323 192.74 Single tier MAX: BH: 44.20 PBW: 79.71 PBL: 64.78 *Wake 324 109.89 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 325 -126.83 YADJ: -3.73 326 *adjusted for a Stack-Building elevation difference of 327 0.61 BldNo: 3 Bld Name:BLD 3 TierNo: 1 328

329 330 Drtcn: 40.00 331 Stack Ht: 332 StkNo: 1 Stk Name:STCK1 182.12 333 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 44.20 PBW: 78.09 PBL: 71.86 *Wake 334 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 335 -61.83 YADJ: 34.05 336 *adjusted for a Stack-Building elevation difference of 337 0.61 338 BldNo: 2 Bld Name:BLD 2 TierNo: 1 Stack Ht: 339 StkNo: 2 Stk Name:STCK2 182.12 340 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 44.20 PBW: 78.09 PBL: 71.87 *Wake 341 Effect Ht: 109.89 342 Relative Coordinates of Projected Width Mid-point: XADJ: 32.88 -61.40 YADJ: 343 344 *adjusted for a Stack-Building elevation difference of 0.61 345 BldNo: 3 Bld Name:BLD 3 TierNo: 1 StkNo: 3 Stk Name:STCK3 Stack Ht: 346 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 347 192.74 348 Single tier MAX: BH: 44.20 PBW: 78.09 PBL: 71.87 *Wake Effect Ht: 109.89 349 Relative Coordinates of Projected Width Mid-point: XADJ: -128.29 YADJ: -20.07 350 351 *adjusted for a Stack-Building elevation difference of 0.61 352 BldNo: 3 Bld Name:BLD 3 TierNo: 1 353 50.00 354 Drtcn: 355 Stack Ht: 356 StkNo: 1 Stk Name:STCK1 182.12 357 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 74.10 PBL: 76.77 *Wake 358 Single tier MAX: BH: 44.20 PBW: Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 359 -69.80 YADJ: 29.04

360 *adjusted for a Stack-Building elevation difference of 361 0.61 362 BldNo: 2 Bld Name:BLD 2 TierNo: 1 Stack Ht: 363 2 Stk Name:STCK2 StkNo: 182.12 364 77.34 PBW: 77.43 *Equation 1 Ht: GEP: BH: 192.74 44.20 PBW: 74.10 PBL: 76.78 *Wake 365 Single tier MAX: BH: Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 366 -69.18 YADJ: 27.96 367 *adjusted for a Stack-Building elevation difference of 368 0.61 3 Bld Name:BLD 3 TierNo: 369 BldNo: 1 3 Stk Name:STCK3 Stack Ht: 370 StkNo: 182.12 77.43 *Equation 1 Ht: 371 GEP: BH: 77.34 PBW: 192.74 77.34 PBW: 82.17 PBL: 81.62 *Wake 372 Single tier MAX: BH: Effect Ht: 192.74 Relative Coordinates of Projected Width Mid-point: XADJ: 373 -331.17 YADJ: 38.66 374 *adjusted for a Stack-Building elevation difference of 375 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 8 376 377 378 Drtcn: 60.00 379 380 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 381 192.74 Single tier MAX: BH: 44.20 PBW: 67.86 PBL: 79.35 *Wake 382 Effect Ht: 109.89 383 Relative Coordinates of Projected Width Mid-point: XADJ: YADJ: 23.14 -75.65 384 *adjusted for a Stack-Building elevation difference of 385 0.61 386 BldNo: 2 Bld Name:BLD 2 TierNo: 1 2 Stk Name:STCK2 Stack Ht: 387 StkNo: 182.12 77.43 *Equation 1 Ht: 388 GEP: BH: 77.34 PBW: 192.74 Single tier MAX: BH: 77.34 PBW: 81.09 PBL: 78.72 *Wake 389 192.74 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 390

-287.28 YADJ: 60.29 391 *adjusted for a Stack-Building elevation difference of 392 0.61 393 BldNo: 1 Bld Name:U1-U3 BU TierNo: 8 394 3 Stk Name:STCK3 Stack Ht: StkNo: 182.12 77.34 77.43 *Equation 1 Ht: 395 GEP: BH: PBW: 192.74 81.09 PBL: 78.72 *Wake 396 Single tier MAX: BH: 77.34 PBW: Effect Ht: 192.74 Relative Coordinates of Projected Width Mid-point: XADJ: 397 -332.02 YADJ: -12.35 398 399 *adjusted for a Stack-Building elevation difference of 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 400 8 401 402 Drtcn: 70.00 403 404 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 77.34 PBW: 77.43 *Equation 1 Ht: 405 GEP: BH: 192.74 406 Single tier MAX: BH: 44.20 PBW: 59.56 PBL: 79.51 *Wake Effect Ht: 109.89 407 Relative Coordinates of Projected Width Mid-point: XADJ: -79.21 YADJ: 16.55 408 409 *adjusted for a Stack-Building elevation difference of 0.61 410 BldNo: 2 Bld Name:BLD 2 TierNo: 1 Stack Ht: 411 StkNo: 2 Stk Name:STCK2 182.12 412 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 77.34 PBW: 77.55 PBL: 73.43 *Wake 413 192.74 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 414 -291.34 YADJ: 16.32 415 *adjusted for a Stack-Building elevation difference of 416 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 417 8 Stack Ht: 418 StkNo: 3 Stk Name:STCK3 182.12 419 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 420 Single tier MAX: BH: 77.34 PBW: 77.55 PBL: 73.43 *Wake Effect Ht: 192.74

PIP\LRS.sup 9/26/2014, 10:16:35 AM Relative Coordinates of Projected Width Mid-point: XADJ: 421 -322.79 YADJ: -62.98 422 *adjusted for a Stack-Building elevation difference of 423 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 8 424 425 426 Drtcn: 80.00 427 Stack Ht: 428 StkNo: 1 Stk Name:STCK1 182.12 *Equation 1 Ht: 429 GEP: BH: 77.34 PBW: 77.43 192.74 71.65 PBL: 65.91 *Wake Single tier MAX: BH: 77.34 PBW: 430 Effect Ht: 184.20 Relative Coordinates of Projected Width Mid-point: XADJ: 431 55.50 -269.75 YADJ: 432 *adjusted for a Stack-Building elevation difference of 433 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 8 434 2 Stk Name:STCK2 Stack Ht: 435 StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 436 192.74 Single tier MAX: BH: 71.65 PBL: 65.91 *Wake 77.34 PBW: 437 Effect Ht: 184.21 Relative Coordinates of Projected Width Mid-point: XADJ: 438 49.02 -269.67 YADJ: 439 *adjusted for a Stack-Building elevation difference of 440 0.61 441 BldNo: 1 Bld Name:U1-U3 BU TierNo: 7 Stack Ht: 3 Stk Name:STCK3 442 StkNo: 182.12 *Equation 1 Ht: 77.43 GEP: BH: 77.34 PBW: 443 192.74 Single tier MAX: BH: 77.34 PBW: PBL: 65.91 *Wake 444 71.65 Effect Ht: 184.21 Relative Coordinates of Projected Width Mid-point: XADJ: 445 -286.87 YADJ: -34.54 446 *adjusted for a Stack-Building elevation difference of 447 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 7 448 449 450 Drtcn: 90.00 451 StkNo: 1 Stk Name:STCK1 Stack Ht: 452 182.12

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77.34 77.43 453 GEP: BH: PBW: *Equation 1 Ht: 192.74 63.57 PBL: 56.38 *Wake 454 77.34 PBW: Single tier MAX: BH: Effect Ht: 172.08 Relative Coordinates of Projected Width Mid-point: XADJ: 455 -271.03 YADJ: 13.53 456 *adjusted for a Stack-Building elevation difference of 457 0.61 458 BldNo: 1 Bld Name:U1-U3 BU TierNo: 8 459 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 460 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 461 Single tier MAX: BH: 77.34 PBW: 63.58 PBL: 56.38 *Wake Effect Ht: 172.10 462 Relative Coordinates of Projected Width Mid-point: XADJ: -269.82 YADJ: 7.17 463 464 *adjusted for a Stack-Building elevation difference of 0.61 465 BldNo: 1 Bld Name:U1-U3 BU TierNo: 7 Stk Name:STCK3 Stack Ht: 466 3 StkNo: 182.12 467 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 77.34 PBW: 63.57 PBL: 56.37 *Wake 468 Effect Ht: 172.08 469 Relative Coordinates of Projected Width Mid-point: XADJ: -1.57-269.92 YADJ: 470 *adjusted for a Stack-Building elevation difference of 471 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 6 472 473 474 Drtcn: 100.00 475 Stack Ht: 476 StkNo: 1 Stk Name:STCK1 182.12 477 77.34 77.43 *Equation 1 Ht: GEP: BH: PBW: 192.74 Single tier MAX: BH: 77.34 PBW: 68.67 PBL: 62.32 *Wake 478 Effect Ht: 179.74 479 Relative Coordinates of Projected Width Mid-point: XADJ: -272.65 YADJ: -28.84 480 *adjusted for a Stack-Building elevation difference of 481 0.61 482 BldNo: 1 Bld Name:U1-U3 BU TierNo: 8 2 Stk Name:STCK2 Stack Ht: 483 StkNo:

182.12 77.43 GEP: BH: 77.34 PBW: *Equation 1 Ht: 484 192.74 Single tier MAX: BH: 77.34 PBW: 68.67 PBL: 62.31 *Wake 485 Effect Ht: 179.74 Relative Coordinates of Projected Width Mid-point: XADJ: 486 -270.36 YADJ: -34.89 487 *adjusted for a Stack-Building elevation difference of 488 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 7 489 3 Stk Name:STCK3 Stack Ht: 490 StkNo: 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 491 192.74 68.67 PBL: 62.32 *Wake Single tier MAX: BH: 77.34 PBW: 492 Effect Ht: 179.74 Relative Coordinates of Projected Width Mid-point: XADJ: 493 -268.95 YADJ: -43.52 494 *adjusted for a Stack-Building elevation difference of 495 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 6 496 497 498 Drtcn: 110.00 499 Stack Ht: 500 StkNo: 1 Stk Name:STCK1 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 501 192.74 Single tier MAX: BH: 77.34 PBW: 75.47 PBL: 70.67 *Wake 502 Effect Ht: 189.93 Relative Coordinates of Projected Width Mid-point: XADJ: 503 4.92 -292.12 YADJ: 504 *adjusted for a Stack-Building elevation difference of 505 0.61 506 BldNo: 1 Bld Name:U1-U3 BU TierNo: 7 2 Stk Name:STCK2 Stack Ht: 507 StkNo: 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 508 192.74 PBL: 70.67 *Wake 509 Single tier MAX: BH: 77.34 PBW: 75.46 189.93 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 510 -288.84 YADJ: -3.18 511 *adjusted for a Stack-Building elevation difference of 512 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 6 513

514 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 *Equation 1 Ht: 515 GEP: BH: 77.34 PBW: 77.43 192.74 Single tier MAX: BH: 24.38 PBW: 98.38 PBL: 102.92 *Wake 516 Effect Ht: 60.34 517 Relative Coordinates of Projected Width Mid-point: XADJ: -153.53 YADJ: -35.79 518 519 *adjusted for a Stack-Building elevation difference of 0.61 520 BldNo: 6 Bld Name:BLD 6 TierNo: 1 521 522 Drtcn: 120.00 523 524 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 525 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 526 Single tier MAX: BH: 77.34 PBW: 79.96 PBL: 76.88 *Wake Effect Ht: 192.74 527 Relative Coordinates of Projected Width Mid-point: XADJ: -328.44 YADJ: 27.71 528 529 *adjusted for a Stack-Building elevation difference of 0.61 530 BldNo: 1 Bld Name:U1-U3 BU TierNo: 6 Stack Ht: StkNo: 2 Stk Name:STCK2 531 182.12 532 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 533 Single tier MAX: BH: 77.34 PBW: 79.96 PBL: 76.88 *Wake Effect Ht: 192.74 534 Relative Coordinates of Projected Width Mid-point: XADJ: -287.54 YADJ: -47.15 535 536 *adjusted for a Stack-Building elevation difference of 0.61 537 BldNo: 1 Bld Name:U1-U3 BU TierNo: 6 StkNo: 3 Stk Name:STCK3 538 Stack Ht: 182.12 539 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 24.38 PBW: 106.56 PBL: 109.49 *Wake 540 Effect Ht: 60.34 541 Relative Coordinates of Projected Width Mid-point: XADJ: -149.04 YADJ: -52.97 542 *adjusted for a Stack-Building elevation difference of 543 0.61

544 BldNo: 6 Bld Name:BLD 6 TierNo: 1 545 546 Drtcn: 130.00 547 Stack Ht: 548 StkNo: 1 Stk Name:STCK1 182.12 549 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 77.34 PBW: 82.04 PBL: 80.75 *Wake 550 Effect Ht: 192.74 Relative Coordinates of Projected Width Mid-point: XADJ: 551 -330.78 YADJ: -23.07 552 *adjusted for a Stack-Building elevation difference of 553 0.61 554 BldNo: 1 Bld Name:U1-U3 BU TierNo: 6 Stack Ht: 555 2 Stk Name:STCK2 StkNo: 182.12 77.34 PBW: 77.43 *Equation 1 Ht: 556 GEP: BH: 192.74 71.87 PBL: 78.09 *Wake Single tier MAX: 44.20 PBW: 557 BH: Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 558 -71.93 YADJ: -25.47 559 *adjusted for a Stack-Building elevation difference of 560 0.61 561 BldNo: 3 Bld Name:BLD 3 TierNo: 1 Stack Ht: 3 Stk Name:STCK3 562 StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 563 192.74 51.72 PBL: 53.48 *Wake 564 Single tier MAX: BH: 12.80 PBW: 31.39 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 565 -56.54 YADJ: -26.10 566 *adjusted for a Stack-Building elevation difference of 567 0.61 TierNo: 1 BldNo: 7 Bld Name:BLD 7 568 569 570 Drtcn: 140.00 571 StkNo: 1 Stk Name:STCK1 Stack Ht: 572 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 573 192.74 Single tier MAX: BH: 77.34 PBW: 81.61 PBL: 82.17 *Wake 574 192.74 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 575

-323.07 YADJ: -73.15 576 *adjusted for a Stack-Building elevation difference of 577 0.61 BldNo: 1 Bld Name:U1-U3 BU TierNo: 578 6 Stack Ht: 579 StkNo: 2 Stk Name:STCK2 182.12 *Equation 1 Ht: 580 GEP: BH: 77.34 PBW: 77.43 192.74 76.78 PBL: 74.10 *Wake Single tier MAX: 44.20 PBW: 581 BH: Effect Ht: 109.89 582 Relative Coordinates of Projected Width Mid-point: XADJ: -65.01 YADJ: -30.79 583 *adjusted for a Stack-Building elevation difference of 584 0.61 585 BldNo: 3 Bld Name:BLD 3 TierNo: 1 StkNo: 3 Stk Name:STCK3 Stack Ht: 586 182.12 GEP: BH: 77.34 77.43 *Equation 1 Ht: 587 PBW: 192.74 588 Single tier MAX: BH: 12.80 PBW: 53.30 PBL: 52.55 *Wake 31.39 Effect Ht: 589 Relative Coordinates of Projected Width Mid-point: XADJ: -51.08 YADJ: -30.88 590 *adjusted for a Stack-Building elevation difference of 591 0.61 592 BldNo: 7 Bld Name:BLD 7 TierNo: 1 593 594 Drtcn: 150.00 595 596 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 597 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 44.20 PBW: 79.35 PBL: 67.86 *Wake 598 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 599 -57.08 YADJ: -35.98 600 *adjusted for a Stack-Building elevation difference of 601 0.61 602 BldNo: 2 Bld Name:BLD 2 TierNo: 1 Stack Ht: 603 2 Stk Name:STCK2 StkNo: 182.12 604 77.43 *Equation 1 Ht: GEP: BH: 77.34 PBW: 192.74 Single tier MAX: BH: 44.20 PBW: 79.35 67.86 *Wake 605 PBL: Effect Ht: 109.89

PIP\LRS.sup 9/26/2014, 10:16:35 AM 606 Relative Coordinates of Projected Width Mid-point: XADJ: -56.12 YADJ: -35.18 607 *adjusted for a Stack-Building elevation difference of 608 0.61 609 BldNo: 3 Bld Name:BLD 3 TierNo: 1 Stack Ht: StkNo: 3 Stk Name:STCK3 610 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 611 192.74 No single tier affects this stack for this direction. 612 613 614 Drtcn: 160.00 615 Stack Ht: 616 StkNo: 1 Stk Name:STCK1 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 617 192.74 Single tier MAX: BH: 44.20 PBW: 79.51 PBL: 59.56 *Wake 618 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 619 -46.32 YADJ: -39.45 620 *adjusted for a Stack-Building elevation difference of 621 0.61 TierNo: 622 BldNo: 2 Bld Name:BLD 2 1 623 2 Stk Name:STCK2 Stack Ht: StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 624 192.74 Single tier MAX: BH: 44.20 PBW: 79.51 PBL: 59.56 *Wake 625 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 626 -45.52 YADJ: -38.50 627 628 *adjusted for a Stack-Building elevation difference of 0.61 BldNo: 3 Bld Name:BLD 3 TierNo: 629 1 Stack Ht: 630 StkNo: 3 Stk Name:STCK3 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 631 192.74 No single tier affects this stack for this direction. 632 633 634 Drtcn: 170.00 635 StkNo: 1 Stk Name:STCK1 Stack Ht: 636 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 637 192.74

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Single tier MAX: BH: 44.20 PBW: 77.26 PBL: 49.45 *Wake 638 109.89 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 639 -34.17 YADJ: -41.72 640 *adjusted for a Stack-Building elevation difference of 641 0.61 BldNo: 2 Bld Name:BLD 2 TierNo: 1 642 2 Stk Name:STCK2 Stack Ht: 643 StkNo: 182.12 644 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 44.20 PBW: 77.26 PBL: 49.45 *Wake Single tier MAX: BH: 645 Effect Ht: 109.89 646 Relative Coordinates of Projected Width Mid-point: XADJ: 49.47 YADJ: -58.51 647 *adjusted for a Stack-Building elevation difference of 648 0.61 649 BldNo: 2 Bld Name:BLD 2 TierNo: 1 StkNo: 3 Stk Name:STCK3 Stack Ht: 650 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 651 192.74 77.26 PBL: 49.45 *Wake Single tier MAX: BH: 44.20 PBW: 652 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 653 50.02 YADJ: -57.85 654 *adjusted for a Stack-Building elevation difference of 655 0.61 BldNo: 3 Bld Name:BLD 3 656 TierNo: 1 657 658 Drtcn: 180.00 659 Stack Ht: 660 StkNo: 1 Stk Name:STCK1 182.12 77.34 PBW: 77.43 *Equation 1 Ht: GEP: BH: 661 192.74 72.66 PBL: 37.83 *Wake 662 Single tier MAX: BH: 44.20 PBW: Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 663 -20.97 YADJ: -42.73 664 *adjusted for a Stack-Building elevation difference of 665 0.61 BldNo: 2 Bld Name:BLD 2 TierNo: 666 1 Stack Ht: 667 StkNo: 2 Stk Name:STCK2 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 668

192.74 Single tier MAX: BH: 44.20 PBW: 72.66 PBL: 37.83 *Wake 669 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 670 64.31 YADJ: -44.74 671 *adjusted for a Stack-Building elevation difference of 672 0.61 673 BldNo: 2 Bld Name:BLD 2 TierNo: 1 Stack Ht: 674 3 Stk Name:STCK3 StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 675 192.74 Single tier MAX: BH: 44.20 PBW: 72.66 PBL: 37.83 *Wake 676 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 677 64.74 YADJ: -43.99 678 *adjusted for a Stack-Building elevation difference of 679 0.61 BldNo: 3 Bld Name:BLD 3 TierNo: 1 680 681 682 Drtcn: 190.00 683 Stack Ht: StkNo: 1 Stk Name:STCK1 684 182.12 *Equation 1 Ht: 685 GEP: BH: 77.34 PBW: 77.43 192.74 Single tier MAX: BH: 44.20 PBW: PBL: 44.97 *Wake 75.70 686 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 687 -101.20 YADJ: -54.04 688 *adjusted for a Stack-Building elevation difference of 689 0.61 BldNo: 3 Bld Name:BLD 3 TierNo: 690 1 Stack Ht: 691 StkNo: 2 Stk Name:STCK2 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 692 192.74 Single tier MAX: BH: 44.20 PBW: 75.70 PBL: 44.97 *Wake 693 Effect Ht: 109.89 694 Relative Coordinates of Projected Width Mid-point: XADJ: -16.87 YADJ: -41.21 695 *adjusted for a Stack-Building elevation difference of 696 0.61 BldNo: 3 Bld Name:BLD 3 TierNo: 1 697 3 Stk Name:STCK3 Stack Ht: 698 StkNo: 182.12

77.43 *Equation 1 Ht: 699 GEP: BH: 77.34 PBW: 192.74 75.70 PBL: 44.97 *Wake 700 44.20 PBW: Single tier MAX: BH: 109.89 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 701 67.54 YADJ: -28.80 702 *adjusted for a Stack-Building elevation difference of 703 0.61 704 BldNo: 3 Bld Name:BLD 3 TierNo: 1 705 706 Drtcn: 200.00 707 Stack Ht: 708 StkNo: 1 Stk Name:STCK1 182.12 709 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 78.91 PBL: 55.71 *Wake 710 Single tier MAX: BH: 44.20 PBW: Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 711 -15.17 YADJ: -40.86 712 *adjusted for a Stack-Building elevation difference of 713 0.61 714 BldNo: 2 Bld Name:BLD 2 TierNo: 1 715 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 *Equation 1 Ht: 716 GEP: BH: 77.34 PBW: 77.43 192.74 Single tier MAX: BH: 44.20 PBW: 78.91 PBL: 55.72 *Wake 717 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 718 -15.17 YADJ: -39.61 719 720 *adjusted for a Stack-Building elevation difference of 0.61 721 BldNo: 3 Bld Name:BLD 3 TierNo: 1 Stack Ht: 722 StkNo: 3 Stk Name:STCK3 182.12 723 77.34 PBW: 77.43 *Equation 1 Ht: GEP: BH: 192.74 Single tier MAX: BH: 44.20 PBW: 78.91 PBL: 55.72 *Wake 724 Effect Ht: 109.89 725 Relative Coordinates of Projected Width Mid-point: XADJ: 65.80 YADJ: -12.73 726 *adjusted for a Stack-Building elevation difference of 727 0.61 BldNo: 3 Bld Name:BLD 3 TierNo: 1 728 729

730 Drtcn: 210.00 731 Stack Ht: 732 StkNo: 1 Stk Name:STCK1 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 733 192.74 Single tier MAX: BH: 44.20 PBW: 79.71 PBL: 64.77 *Wake 734 Effect Ht: 109.89 735 Relative Coordinates of Projected Width Mid-point: XADJ: -12.80 YADJ: -38.03 736 *adjusted for a Stack-Building elevation difference of 737 0.61 BldNo: 2 Bld Name:BLD 2 TierNo: 738 1 Stack Ht: 739 2 Stk Name:STCK2 StkNo: 182.12 740 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 79.71 PBL: 64.78 *Wake Single tier MAX: BH: 44.20 PBW: 741 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 742 -13.02 YADJ: -36.80 743 *adjusted for a Stack-Building elevation difference of 744 0.61 BldNo: 3 Bld Name:BLD 3 745 TierNo: 1 746 3 Stk Name:STCK3 Stack Ht: StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 747 192.74 Single tier MAX: BH: 44.20 PBW: 79.71 PBL: 64.78 *Wake 748 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 749 3.73 62.05 YADJ: 750 *adjusted for a Stack-Building elevation difference of 751 0.61 752 BldNo: 3 Bld Name:BLD 3 TierNo: 1 753 Drtcn: 220.00 754 755 StkNo: 1 Stk Name:STCK1 Stack Ht: 756 182.12 77.43 *Equation 1 Ht: 757 GEP: BH: 77.34 PBW: 192.74 78.09 PBL: 71.86 *Wake Single tier MAX: BH: 44.20 PBW: 758 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 759 -10.03 YADJ: -34.05 760

761 *adjusted for a Stack-Building elevation difference of 0.61 762 BldNo: 2 Bld Name:BLD 2 TierNo: 1 763 Stk Name:STCK2 Stack Ht: StkNo: 2 182.12 764 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 44.20 PBW: 78.09 PBL: 71.87 *Wake 765 Effect Ht: 109.89 766 Relative Coordinates of Projected Width Mid-point: XADJ: -10.47 YADJ: -32.88 767 768 *adjusted for a Stack-Building elevation difference of 0.61 769 BldNo: 3 Bld Name:BLD 3 TierNo: 1 770 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 771 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 192.74 772 Single tier MAX: BH: 44.20 PBW: 78.09 PBL: 71.87 *Wake Effect Ht: 109.89 773 Relative Coordinates of Projected Width Mid-point: XADJ: 20.07 56.42 YADJ: 774 775 *adjusted for a Stack-Building elevation difference of 0.61 776 BldNo: 3 Bld Name:BLD 3 TierNo: 1 777 778 Drtcn: 230.00 779 780 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 781 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 44.20 PBW: 74.10 PBL: 76.77 *Wake 782 Single tier MAX: BH: Effect Ht: 109.89 783 Relative Coordinates of Projected Width Mid-point: XADJ: -6.97 YADJ: -29.04 784 *adjusted for a Stack-Building elevation difference of 785 0.61 786 BldNo: 2 Bld Name:BLD 2 TierNo: 1 787 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 788 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 44.20 PBW: 74.10 PBL: 76.78 *Wake 789 Single tier MAX: BH: Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 790 -7.60 YADJ: -27.96

791 *adjusted for a Stack-Building elevation difference of 792 0.61 793 BldNo: 3 Bld Name:BLD 3 TierNo: 1 Stack Ht: 794 3 Stk Name:STCK3 StkNo: 182.12 795 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 44.20 PBW: 74.10 PBL: 76.78 *Wake 796 Single tier MAX: BH: Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 797 49.08 YADJ: 35.81 798 *adjusted for a Stack-Building elevation difference of 799 0.61 800 BldNo: 3 Bld Name:BLD 3 TierNo: 1 801 802 Drtcn: 240.00 803 Stack Ht: 804 StkNo: 1 Stk Name:STCK1 182.12 77.43 *Equation 1 Ht: 805 GEP: BH: 77.34 PBW: 192.74 Single tier MAX: BH: 44.20 PBW: 67.86 PBL: 79.35 *Wake 806 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 807 -3.69 YADJ: -23.14 808 *adjusted for a Stack-Building elevation difference of 809 0.61 BldNo: 2 Bld Name:BLD 2 TierNo: 1 810 Stack Ht: 811 StkNo: 2 Stk Name:STCK2 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 812 192.74 Single tier MAX: BH: 44.20 PBW: 67.86 PBL: 79.35 *Wake 813 Effect Ht: 109.89 814 Relative Coordinates of Projected Width Mid-point: XADJ: -4.50 YADJ: -22.19 815 *adjusted for a Stack-Building elevation difference of 816 0.61 817 BldNo: 3 Bld Name:BLD 3 TierNo: 1 StkNo: 3 Stk Name:STCK3 Stack Ht: 818 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 819 192.74 Single tier MAX: BH: 44.20 PBW: 67.86 PBL: 79.35 *Wake 820 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 821

40.25 YADJ: 50.45 822 823 *adjusted for a Stack-Building elevation difference of 0.61 824 BldNo: 3 Bld Name:BLD 3 TierNo: 1 825 826 Drtcn: 250.00 827 828 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 829 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 830 Single tier MAX: BH: 44.20 PBW: 59.56 PBL: 79.51 *Wake Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 831 -0.30 YADJ: -16.55 832 833 *adjusted for a Stack-Building elevation difference of 0.61 834 BldNo: 2 Bld Name:BLD 2 TierNo: 1 835 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 836 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 44.20 PBW: 59.56 PBL: 79.51 *Wake 837 Single tier MAX: BH: Effect Ht: 109.89 838 Relative Coordinates of Projected Width Mid-point: XADJ: -1.26 YADJ: -15.74 839 840 *adjusted for a Stack-Building elevation difference of 0.61 841 BldNo: 3 Bld Name:BLD 3 TierNo: 1 Stack Ht: 842 StkNo: 3 Stk Name:STCK3 182.12 843 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 24.38 PBW: 102.02 PBL: 105.93 *Wake 844 Single tier MAX: BH: 60.34 Effect Ht: 845 Relative Coordinates of Projected Width Mid-point: XADJ: 48.23 YADJ: -38.19 846 847 *adjusted for a Stack-Building elevation difference of 0.61 848 BldNo: 6 Bld Name:BLD 6 TierNo: 1 849 850 Drtcn: 260.00 851 852 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 853 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht:

192.74 Single tier MAX: BH: 44.20 PBW: 49.45 PBL: 77.26 *Wake 854 109.89 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 855 YADJ: -9.443.10 856 *adjusted for a Stack-Building elevation difference of 857 0.61 BldNo: 2 Bld Name:BLD 2 TierNo: 1 858 Stack Ht: 859 2 Stk Name:STCK2 StkNo: 182.12 77.34 PBW: 77.43 *Equation 1 Ht: 860 GEP: BH: 192.74 44.20 PBW: 49.45 PBL: 77.26 *Wake Single tier MAX: BH: 861 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 862 -8.82 2.02 YADJ: 863 *adjusted for a Stack-Building elevation difference of 864 0.61 865 BldNo: 3 Bld Name:BLD 3 TierNo: 1 Stack Ht: 3 Stk Name:STCK3 866 StkNo: 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 867 192.74 40.51 PBL: 48.38 *Wake 868 Single tier MAX: BH: 12.80 PBW: Effect Ht: 31.39 Relative Coordinates of Projected Width Mid-point: XADJ: 869 -6.05 14.96 YADJ: 870 *adjusted for a Stack-Building elevation difference of 871 0.61 BldNo: 7 Bld Name:BLD 7 TierNo: 1 872 873 Drtcn: 270.00 874 875 StkNo: 1 Stk Name:STCK1 Stack Ht: 876 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 877 192.74 37.83 PBL: 72.66 *Wake Single tier MAX: BH: 44.20 PBW: 878 Effect Ht: 100.33 Relative Coordinates of Projected Width Mid-point: XADJ: 879 -2.05 6.40 YADJ: 880 *adjusted for a Stack-Building elevation difference of 881 0.61 TierNo: 1 882 BldNo: 2 Bld Name:BLD 2 Stack Ht: 2 Stk Name:STCK2 883 StkNo: 182.12

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884 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 885 44.20 PBW: 37.83 PBL: 72.66 *Wake Single tier MAX: BH: Effect Ht: 100.33 886 Relative Coordinates of Projected Width Mid-point: XADJ: 5.23 YADJ: -1.62 887 888 *adjusted for a Stack-Building elevation difference of 0.61 889 BldNo: 3 Bld Name:BLD 3 TierNo: 1 890 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 891 77.34 PBW: 77.43 *Equation 1 Ht: GEP: BH: 192.74 33.83 PBL: 43.69 *Wake 892 Single tier MAX: BH: 12.80 PBW: Effect Ht: 31.39 893 Relative Coordinates of Projected Width Mid-point: XADJ: 17.76 YADJ: 0.85 894 895 *adjusted for a Stack-Building elevation difference of 0.61 896 BldNo: 7 Bld Name:BLD 7 TierNo: 1 897 898 Drtcn: 280.00 899 900 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 901 77.34 PBW: *Equation 1 Ht: GEP: BH: 77.43 192.74 Single tier MAX: BH: 902 44.20 PBW: 44.96 PBL: 75.70 *Wake 109.89 Effect Ht: 903 Relative Coordinates of Projected Width Mid-point: XADJ: 4.59 YADJ: 5.40 904 905 *adjusted for a Stack-Building elevation difference of 0.61 906 BldNo: 2 Bld Name:BLD 2 TierNo: 1 907 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 908 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 PBL: 75.70 *Wake 909 Single tier MAX: BH: 44.20 PBW: 44.97 Effect Ht: 109.89 910 Relative Coordinates of Projected Width Mid-point: XADJ: 3.36 YADJ: 5.62 911 912 *adjusted for a Stack-Building elevation difference of 0.61 913 BldNo: 3 Bld Name:BLD 3 TierNo: 1 914 3 Stk Name:STCK3 Stack Ht: StkNo:

182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 915 192.74 Single tier MAX: BH: 12.80 PBW: 37.97 PBL: 46.68 *Wake 916 Effect Ht: 31.39 917 Relative Coordinates of Projected Width Mid-point: XADJ: 7.71 15.52 YADJ: 918 *adjusted for a Stack-Building elevation difference of 919 0.61 BldNo: 7 Bld Name:BLD 7 TierNo: 1 920 921 Drtcn: 290.00 922 923 Stack Ht: 924 StkNo: 1 Stk Name:STCK1 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 925 192.74 55.71 PBL: 78.91 *Wake Single tier MAX: BH: 44.20 PBW: 926 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 927 1.40 YADJ: 12.69 928 *adjusted for a Stack-Building elevation difference of 929 0.61 BldNo: 2 Bld Name:BLD 2 TierNo: 930 1 931 2 Stk Name:STCK2 Stack Ht: StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 932 192.74 Single tier MAX: BH: 44.20 PBW: 55.72 PBL: 78.91 *Wake 933 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 934 12.69 0.16 YADJ: 935 *adjusted for a Stack-Building elevation difference of 936 0.61 BldNo: 3 Bld Name:BLD 3 TierNo: 937 1 Stack Ht: StkNo: 3 Stk Name:STCK3 938 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 939 192.74 Single tier MAX: BH: 12.80 PBW: 43.93 PBL: 50.50 *Wake 940 31.39 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 941 11.68 YADJ: 14.34 942 *adjusted for a Stack-Building elevation difference of 943 0.61 BldNo: 7 Bld Name:BLD 7 TierNo: 1 944

945 946 Drtcn: 300.00 947 Stack Ht: 948 StkNo: 1 Stk Name:STCK1 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 949 192.74 44.20 PBW: 64.77 PBL: 79.71 *Wake Single tier MAX: BH: 950 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 951 -1.82 YADJ: 19.59 952 *adjusted for a Stack-Building elevation difference of 953 0.61 BldNo: 2 Bld Name:BLD 2 TierNo: 954 1 955 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 956 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 44.20 PBW: 64.78 PBL: 79.71 *Wake 957 Effect Ht: 109.89 958 Relative Coordinates of Projected Width Mid-point: XADJ: 19.37 -3.05 YADJ: 959 *adjusted for a Stack-Building elevation difference of 960 0.61 961 BldNo: 3 Bld Name:BLD 3 TierNo: 1 Stack Ht: StkNo: 3 Stk Name:STCK3 962 182.12 *Equation 1 Ht: 963 GEP: BH: 77.34 PBW: 77.43 192.74 Single tier MAX: BH: 24.38 PBW: 106.56 PBL: 109.49 *Wake 964 60.34 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 965 39.56 YADJ: 52.97 966 *adjusted for a Stack-Building elevation difference of 967 0.61 BldNo: 6 Bld Name:BLD 6 968 TierNo: 1 969 970 Drtcn: 310.00 971 Stack Ht: 972 StkNo: 1 Stk Name:STCK1 182.12 77.34 PBW: 77.43 *Equation 1 Ht: 973 GEP: BH: 192.74 44.20 PBW: 71.86 PBL: 78.09 *Wake 974 Single tier MAX: BH: Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 975 -4.99 YADJ: 25.90

976 *adjusted for a Stack-Building elevation difference of 977 0.61 978 BldNo: 2 Bld Name:BLD 2 TierNo: 1 Stack Ht: 979 2 Stk Name:STCK2 StkNo: 182.12 *Equation 1 Ht: 980 77.34 PBW: 77.43 GEP: BH: 192.74 44.20 PBW: 71.87 PBL: 78.09 *Wake 981 Single tier MAX: BH: Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 982 -6.17 YADJ: 25.47 983 *adjusted for a Stack-Building elevation difference of 984 0.61 985 3 Bld Name:BLD 3 TierNo: BldNo: 1 986 3 Stk Name:STCK3 Stack Ht: StkNo: 182.12 77.34 PBW: 77.43 *Equation 1 Ht: 987 GEP: BH: 192.74 12.80 PBW: 51.72 PBL: 53.48 *Wake 988 Single tier MAX: BH: Effect Ht: 31.39 Relative Coordinates of Projected Width Mid-point: XADJ: 989 26.10 3.05 YADJ: 990 *adjusted for a Stack-Building elevation difference of 991 0.61 992 BldNo: 7 Bld Name:BLD 7 TierNo: 1 993 994 Drtcn: 320.00 995 996 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 997 192.74 Single tier MAX: 44.20 PBW: 76.77 PBL: 74.10 *Wake 998 BH: Effect Ht: 109.89 999 Relative Coordinates of Projected Width Mid-point: XADJ: -8.01 YADJ: 31.42 1000 *adjusted for a Stack-Building elevation difference of 1001 0.61 1002 BldNo: 2 Bld Name:BLD 2 TierNo: 1 2 Stk Name:STCK2 Stack Ht: 1003 StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1004 192.74 1005 Single tier MAX: BH: 44.20 PBW: 76.78 PBL: 74.10 *Wake 109.89 Effect Ht: Relative Coordinates of Projected Width Mid-point: XADJ: 1006

-9.09 YADJ: 30.79 1007 1008 *adjusted for a Stack-Building elevation difference of 0.61 1009 BldNo: 3 Bld Name:BLD 3 TierNo: 1 1010 3 Stk Name:STCK3 Stack Ht: StkNo: 182.12 1011 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 12.80 PBW: 53.30 PBL: 52.55 *Wake 1012 Effect Ht: 31.39 1013 Relative Coordinates of Projected Width Mid-point: XADJ: 30.88 -1.46 YADJ: 1014 1015 *adjusted for a Stack-Building elevation difference of 0.61 1016 BldNo: 7 Bld Name:BLD 7 TierNo: 1 1017 1018 Drtcn: 330.00 1019 1020 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 1021 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1022 Single tier MAX: BH: 44.20 PBW: 79.35 PBL: 67.86 *Wake 109.89 Effect Ht: 1023 Relative Coordinates of Projected Width Mid-point: XADJ: -10.79 YADJ: 35.98 1024 1025 *adjusted for a Stack-Building elevation difference of 0.61 1026 BldNo: 2 Bld Name:BLD 2 TierNo: 1 Stack Ht: 1027 StkNo: 2 Stk Name:STCK2 182.12 1028 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 44.20 PBW: 79.35 PBL: 67.86 *Wake 1029 Effect Ht: 109.89 1030 Relative Coordinates of Projected Width Mid-point: XADJ: -11.74 YADJ: 35.18 1031 1032 *adjusted for a Stack-Building elevation difference of 0.61 1033 BldNo: 3 Bld Name:BLD 3 TierNo: 1 1034 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 1035 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1036 No single tier affects this stack for this direction. 1037

1038 Drtcn: 340.00 1039 Stack Ht: 1040 StkNo: 1 Stk Name:STCK1 182.12 77.43 *Equation 1 Ht: 1041 GEP: BH: 77.34 PBW: 192.74 Single tier MAX: BH: 44.20 PBW: 79.51 PBL: 59.56 *Wake 1042 Effect Ht: 109.89 1043 Relative Coordinates of Projected Width Mid-point: XADJ: -13.23 YADJ: 39.45 1044 *adjusted for a Stack-Building elevation difference of 1045 0.61 BldNo: 2 Bld Name:BLD 2 TierNo: 1046 1 Stack Ht: 1047 2 Stk Name:STCK2 StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1048 192.74 79.51 PBL: 59.56 *Wake Single tier MAX: BH: 44.20 PBW: 1049 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 1050 -14.04 YADJ: 38.50 1051 *adjusted for a Stack-Building elevation difference of 1052 0.61 BldNo: 3 Bld Name:BLD 3 1053 TierNo: 1 1054 3 Stk Name:STCK3 Stack Ht: StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1055 192.74 No single tier affects this stack for this direction. 1056 1057 1058 Drtcn: 350.00 1059 Stack Ht: StkNo: 1 Stk Name:STCK1 1060 182.12 *Equation 1 Ht: 1061 GEP: BH: 77.34 PBW: 77.43 192.74 44.20 PBW: 77.26 PBL: 49.45 *Wake Single tier MAX: BH: 1062 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 1063 -15.28 YADJ: 41.72 1064 *adjusted for a Stack-Building elevation difference of 1065 0.61 2 Bld Name:BLD 2 1066 TierNo: 1 BldNo: Stack Ht: 1067 StkNo: 2 Stk Name:STCK2 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1068 192.74

Single tier MAX: BH: 44.20 PBW: 77.26 PBL: 49.45 *Wake 1069 Effect Ht: 109.89 1070 Relative Coordinates of Projected Width Mid-point: XADJ: -98.91 YADJ: 58.51 1071 1072 *adjusted for a Stack-Building elevation difference of 0.61 BldNo: 2 Bld Name:BLD 2 1073 TierNo: 1 StkNo: 3 Stk Name:STCK3 Stack Ht: 1074 182.12 1075 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 44.20 PBW: 77.26 PBL: 49.45 *Wake 1076 Effect Ht: 109.89 1077 Relative Coordinates of Projected Width Mid-point: XADJ: -99.47 YADJ: 57.85 1078 1079 *adjusted for a Stack-Building elevation difference of 0.61 1080 BldNo: 3 Bld Name:BLD 3 TierNo: 1 1081 1082 Drtcn: 360.00 1083 1084 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 1085 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 44.20 PBW: 72.66 PBL: 37.83 *Wake 1086 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 1087 42.73 -16.86 YADJ: 1088 *adjusted for a Stack-Building elevation difference of 1089 0.61 1090 BldNo: 2 Bld Name:BLD 2 TierNo: 1 1091 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1092 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Single tier MAX: BH: 44.20 PBW: 72.66 PBL: 37.83 *Wake 1093 Effect Ht: 109.89 1094 Relative Coordinates of Projected Width Mid-point: XADJ: -102.14 YADJ: 44.74 1095 1096 *adjusted for a Stack-Building elevation difference of 0.61 1097 BldNo: 2 Bld Name:BLD 2 TierNo: 1 StkNo: 3 Stk Name:STCK3 1098 Stack Ht: 182.12 1099 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht:

PIP\LRS.sup 9/26/2014, 10:16:35 AM 192.74 Single tier MAX: BH: 44.20 PBW: 72.66 PBL: 37.83 *Wake 1100 Effect Ht: 109.89 Relative Coordinates of Projected Width Mid-point: XADJ: 1101 -187.42 YADJ: 47.17 1102 *adjusted for a Stack-Building elevation difference of 1103 0.61 BldNo: 2 Bld Name:BLD 2 TierNo: 1 1104 1105 1106 Dominant combined buildings: 1107 1108 Drtcn: 10.00 1109 1110 Stack Ht: StkNo: 1 Stk Name:STCK1 1111 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1112 192.74 No combined tiers affect this stack for this direction. 1113 1114 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1115 192.74 No combined tiers affect this stack for this direction. 1116 Stack Ht: StkNo: 3 Stk Name:STCK3 1117 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1118 192.74 No combined tiers affect this stack for this direction. 1119 1120 Drtcn: 20.00 1121 1122 Stack Ht: StkNo: 1 Stk Name:STCK1 1123 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1124 192.74 No combined tiers affect this stack for this direction. 1125 Stack Ht: StkNo: 2 Stk Name:STCK2 1126 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1127 192.74 No combined tiers affect this stack for this direction. 1128 Stack Ht: StkNo: 3 Stk Name:STCK3 1129 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1130 192.74 No combined tiers affect this stack for this direction. 1131 1132 1133 Drtcn: 30.00

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1134 1135 Stack Ht: StkNo: 1 Stk Name:STCK1 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1136 192.74 No combined tiers affect this stack for this direction. 1137 1138 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1139 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1140 No combined tiers affect this stack for this direction. StkNo: 3 Stk Name:STCK3 1141 Stack Ht: 182.12 1142 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 192.74 1143 Combined tier MAX: BH: 24.38 PBW: 106.93 PBL: 155.89 *WE Ht: 60.34 1144 Relative Coordinates of Projected Width Mid-point: XADJ: -246.65 YADJ: 57.87 1145 1146 *adjusted for a Stack-Building elevation difference of 0.61 No. of Tiers affecting Stk: 2 1147 1148 Bldg-Tier nos. contributing to MAX: 25 33 1149 1150 Drtcn: 40.00 1151 1152 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 1153 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1154 1155 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1156 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1157 1158 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 1159 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 24.38 PBW: 126.09 PBL: 146.77 *WE Ht: 1160 Combined tier MAX: BH: 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1161 -249.58 YADJ: 27.69 1162 *adjusted for a Stack-Building elevation difference of 1163 0.61 1164 No. of Tiers affecting Stk: 2 1165 Bldg-Tier nos. contributing to MAX: 25 33

1166 1167 Drtcn: 50.00 1168 StkNo: 1 Stk Name:STCK1 Stack Ht: 1169 182.12 1170 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1171 StkNo: 2 Stk Name:STCK2 Stack Ht: 1172 182.12 1173 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 24.38 PBW: 141.41 PBL: 133.20 *WE Ht: 1174 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1175 -188.24 YADJ: 60.44 1176 *adjusted for a Stack-Building elevation difference of 1177 0.61 No. of Tiers affecting Stk: 2 1178 Bldg-Tier nos. contributing to MAX: 25 33 1179 StkNo: 3 Stk Name:STCK3 Stack Ht: 1180 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 1181 192.74 Combined tier MAX: BH: 24.38 PBW: 141.33 PBL: 165.43 *WE Ht: 1182 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1183 -190.92 YADJ: 56.11 1184 *adjusted for a Stack-Building elevation difference of 1185 0.61 No. of Tiers affecting Stk: 2 1186 Bldg-Tier nos. contributing to MAX: 41 33 1187 1188 1189 Drtcn: 60.00 1190 1 Stk Name:STCK1 Stack Ht: 1191 StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1192 192.74 No combined tiers affect this stack for this direction. 1193 Stack Ht: 1194 StkNo: 2 Stk Name:STCK2 182.12 *Equation 1 Ht: 77.34 PBW: 77.43 1195 GEP: BH: 192.74 Combined tier MAX: BH: 24.38 PBW: 152.44 PBL: 115.58 *WE Ht: 1196 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1197 -188.08 YADJ: 38.40

1198 1199 *adjusted for a Stack-Building elevation difference of 0.61 No. of Tiers affecting Stk: 2 1200 1201 Bldg-Tier nos. contributing to MAX: 25 33 Stack Ht: 1202 StkNo: 3 Stk Name:STCK3 182.12 1203 77.34 PBW: 77.43 *Equation 1 Ht: GEP: BH: 192.74 Combined tier MAX: BH: 24.38 PBW: 152.17 PBL: 152.54 *WE Ht: 1204 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1205 -189.97 YADJ: 33.57 1206 *adjusted for a Stack-Building elevation difference of 1207 0.61 1208 No. of Tiers affecting Stk: 2 1209 Bldg-Tier nos. contributing to MAX: 41 33 1210 1211 Drtcn: 70.00 1212 1213 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 1214 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1215 No combined tiers affect this stack for this direction. 1216 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1217 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1218 Combined tier MAX: BH: 24.38 PBW: 158.39 PBL: 135.03 *WE Ht: 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1219 -151.80 YADJ: 89.32 1220 *adjusted for a Stack-Building elevation difference of 1221 0.61 1222 No. of Tiers affecting Stk: 2 Bldg-Tier nos. contributing to MAX: 41 1223 33 Stack Ht: 1224 StkNo: 3 Stk Name:STCK3 182.12 1225 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 24.38 PBW: 158.39 PBL: 135.03 *WE Ht: 1226 60.34 1227 Relative Coordinates of Projected Width Mid-point: XADJ: -183.25 YADJ: 10.01 1228 1229 *adjusted for a Stack-Building elevation difference of 0.61

PIP\LRS.sup 9/26/2014, 10:16:35 AM 1230 No. of Tiers affecting Stk: 2 1231 Bldg-Tier nos. contributing to MAX: 41 33 1232 Drtcn: 80.00 1233 1234 1235 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 GEP: BH: 77.34 PBW: 77.43 1236 *Equation 1 Ht: 192.74 1237 Combined tier MAX: BH: 24.38 PBW: 160.40 PBL: 70.45 *WE Ht: 60.34 1238 Relative Coordinates of Projected Width Mid-point: XADJ: -154.00 YADJ: 75.16 1239 *adjusted for a Stack-Building elevation difference of 1240 0.61 1241 No. of Tiers affecting Stk: 2 1242 Bldg-Tier nos. contributing to MAX: 25 33 1243 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1244 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1245 24.38 PBW: 159.79 PBL: 113.41 *WE Ht: Combined tier MAX: BH: 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1246 -153.76 YADJ: 69.71 1247 *adjusted for a Stack-Building elevation difference of 1248 0.61 1249 No. of Tiers affecting Stk: 2 Bldg-Tier nos. contributing to MAX: 41 1250 33 1251 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 1252 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 24.38 PBW: 159.79 1253 PBL: 113.41 *WE Ht: 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1254 -170.96 YADJ: -13.85 1255 1256 *adjusted for a Stack-Building elevation difference of 0.61 1257 No. of Tiers affecting Stk: 2 Bldg-Tier nos. contributing to MAX: 41 33 1258 1259 1260 Drtcn: 90.00 1261 Stack Ht: 1262 1 Stk Name:STCK1 StkNo: 182.12 77.43 *Equation 1 Ht: 1263 GEP: BH: 77.34 PBW:

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192.74 24.38 PBW: 157.10 PBL: 44.31 *WE Ht: 1264 Combined tier MAX: BH: 60.34 1265 Relative Coordinates of Projected Width Mid-point: XADJ: -152.18 YADJ: 53.39 1266 1267 *adjusted for a Stack-Building elevation difference of 0.61 1268 No. of Tiers affecting Stk: 2 Bldg-Tier nos. contributing to MAX: 25 33 1269 1270 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1271 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 24.38 PBW: 156.34 PBL: 88.34 *WE Ht: 1272 60.34 1273 Relative Coordinates of Projected Width Mid-point: XADJ: -151.05 YADJ: 47.99 1274 1275 *adjusted for a Stack-Building elevation difference of 0.61 1276 No. of Tiers affecting Stk: 2 1277 Bldg-Tier nos. contributing to MAX: 41 33 Stack Ht: 1278 StkNo: 3 Stk Name:STCK3 182.12 1279 77.34 PBW: *Equation 1 Ht: GEP: BH: 77.43 192.74 1280 24.38 PBW: 156.34 PBL: 88.34 *WE Ht: Combined tier MAX: BH: 60.34 1281 Relative Coordinates of Projected Width Mid-point: XADJ: -153.48 YADJ: -37.29 1282 *adjusted for a Stack-Building elevation difference of 1283 0.61 No. of Tiers affecting Stk: 2 1284 1285 Bldg-Tier nos. contributing to MAX: 41 33 1286 1287 Drtcn: 100.00 1288 1289 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 GEP: BH: 77.34 PBW: 77.43 1290 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 24.38 PBW: 159.77 PBL: 59.55 *WE Ht: 1291 60.34 1292 Relative Coordinates of Projected Width Mid-point: XADJ: -167.10 YADJ: 30.00 1293 1294 *adjusted for a Stack-Building elevation difference of 0.61

No. of Tiers affecting Stk: 2 1295 25 33 Bldg-Tier nos. contributing to MAX: 1296 Stack Ht: 1297 StkNo: 2 Stk Name:STCK2 182.12 77.43 *Equation 1 Ht: 77.34 PBW: 1298 GEP: BH: 192.74 Combined tier MAX: BH: 24.38 PBW: 159.77 PBL: 59.55 *WE Ht: 1299 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1300 -154.27 YADJ: -54.33 1301 *adjusted for a Stack-Building elevation difference of 1302 0.61 1303 No. of Tiers affecting Stk: 2 Bldg-Tier nos. contributing to MAX: 25 33 1304 Stack Ht: 1305 StkNo: 3 Stk Name:STCK3 182.12 77.43 *Equation 1 Ht: GEP: BH: 77.34 PBW: 1306 192.74 Combined tier MAX: BH: 24.38 PBW: 165.11 PBL: 93.23 *WE Ht: 1307 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1308 -153.34 YADJ: -56.47 1309 *adjusted for a Stack-Building elevation difference of 1310 0.61 No. of Tiers affecting Stk: 2 1311 Bldg-Tier nos. contributing to MAX: 41 33 1312 1313 Drtcn: 110.00 1314 1315 Stack Ht: 1316 StkNo: 1 Stk Name:STCK1 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1317 192.74 Combined tier MAX: BH: 24.38 PBW: 160.26 84.53 *WE Ht: PBL: 1318 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1319 -182.71 YADJ: 5.70 1320 *adjusted for a Stack-Building elevation difference of 1321 0.61 No. of Tiers affecting Stk: 2 1322 Bldg-Tier nos. contributing to MAX: 25 33 1323 Stack Ht: StkNo: 2 Stk Name:STCK2 1324 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1325 192.74 Combined tier MAX: BH: 24.38 PBW: 160.26 PBL: 84.53 *WE Ht: 1326 60.34

File: P:\AQES\Projects\Basin Electric\Laramie River\400-Technical\Archive\B PIP\LRS.sup 9/26/2014, 10:16:35 AM Relative Coordinates of Projected Width Mid-point: XADJ: 1327 -155.43 YADJ: -75.13 1328 1329 *adjusted for a Stack-Building elevation difference of 0.61 No. of Tiers affecting Stk: 2 1330 1331 Bldg-Tier nos. contributing to MAX: 25 33 Stack Ht: 1332 StkNo: 3 Stk Name:STCK3 182.12 77.43 1333 GEP: BH: 77.34 PBW: *Equation 1 Ht: 192.74 1334 Combined tier MAX: BH: 24.38 PBW: 173.12 PBL: 102.92 *WE Ht: 60.34 1335 Relative Coordinates of Projected Width Mid-point: XADJ: -153.53 YADJ: -73.16 1336 1337 *adjusted for a Stack-Building elevation difference of 0.61 1338 No. of Tiers affecting Stk: 2 1339 Bldg-Tier nos. contributing to MAX: 41 33 1340 1341 Drtcn: 120.00 1342 1343 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 1344 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1345 24.38 PBW: 155.89 PBL: 106.93 *WE Ht: Combined tier MAX: BH: 60.34 1346 Relative Coordinates of Projected Width Mid-point: XADJ: -192.76 YADJ: -18.78 1347 1348 *adjusted for a Stack-Building elevation difference of 0.61 1349 No. of Tiers affecting Stk: 2 1350 Bldg-Tier nos. contributing to MAX: 25 33 1351 Stack Ht: StkNo: 2 Stk Name:STCK2 182.12 1352 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1353 Combined tier MAX: BH: 24.38 PBW: 175.88 PBL: 109.49 *WE Ht: 60.34 1354 Relative Coordinates of Projected Width Mid-point: XADJ: -189.58 YADJ: -12.55 1355 1356 *adjusted for a Stack-Building elevation difference of 0.61 No. of Tiers affecting Stk: 2 1357 Bldg-Tier nos. contributing to MAX: 41 33 1358 StkNo: 3 Stk Name:STCK3 Stack Ht: 1359

182.12 *Equation 1 Ht: 1360 GEP: BH: 77.34 PBW: 77.43 192.74 24.38 PBW: 175.88 PBL: 109.49 *WE Ht: Combined tier MAX: BH: 1361 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1362 -149.04 YADJ: -87.62 1363 *adjusted for a Stack-Building elevation difference of 1364 0.61 No. of Tiers affecting Stk: 2 1365 Bldg-Tier nos. contributing to MAX: 41 33 1366 1367 Drtcn: 130.00 1368 1369 Stack Ht: StkNo: 1 Stk Name:STCK1 1370 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1371 192.74 Combined tier MAX: BH: 24.38 PBW: 146.77 PBL: 126.09 *WE Ht: 1372 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1373 -196.97 YADJ: -42.68 1374 *adjusted for a Stack-Building elevation difference of 1375 0.61 No. of Tiers affecting Stk: 2 1376 Bldg-Tier nos. contributing to MAX: 25 33 1377 Stack Ht: StkNo: 2 Stk Name:STCK2 1378 182.12 1379 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 24.38 PBW: 173.28 PBL: 126.19 *WE Ht: 1380 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1381 -192.99 YADJ: -32.54 1382 *adjusted for a Stack-Building elevation difference of 1383 0.61 No. of Tiers affecting Stk: 1384 2 Bldg-Tier nos. contributing to MAX: 41 1385 33 StkNo: 3 Stk Name:STCK3 Stack Ht: 1386 182.12 77.43 *Equation 1 Ht: GEP: BH: 77.34 PBW: 1387 192.74 Combined tier MAX: BH: 12.80 PBW: 124.04 PBL: 136.98 *WE Ht: 1388 31.39 Relative Coordinates of Projected Width Mid-point: XADJ: 1389 -140.03 YADJ: -62.27 1390

*adjusted for a Stack-Building elevation difference of 1391 0.61 1392 No. of Tiers affecting Stk: 2 1393 Bldg-Tier nos. contributing to MAX: 49 41 1394 1395 Drtcn: 140.00 1396 1397 Stack Ht: StkNo: 1 Stk Name:STCK1 182.12 1398 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 24.38 PBW: 133.20 PBL: 141.41 *WE Ht: 1399 Combined tier MAX: BH: 60.34 1400 Relative Coordinates of Projected Width Mid-point: XADJ: -195.18 YADJ: -65.29 1401 1402 *adjusted for a Stack-Building elevation difference of 0.61 1403 No. of Tiers affecting Stk: 2 1404 Bldg-Tier nos. contributing to MAX: 25 33 Stack Ht: 1405 StkNo: 2 Stk Name:STCK2 182.12 *Equation 1 Ht: 1406 GEP: BH: 77.34 PBW: 77.43 192.74 Combined tier MAX: BH: 24.38 PBW: 165.43 PBL: 141.33 *WE Ht: 1407 60.34 1408 Relative Coordinates of Projected Width Mid-point: XADJ: -190.54 YADJ: -51.53 1409 *adjusted for a Stack-Building elevation difference of 1410 0.61 1411 No. of Tiers affecting Stk: 2 Bldg-Tier nos. contributing to MAX: 41 33 1412 Stack Ht: 1413 StkNo: 3 Stk Name:STCK3 182.12 1414 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 12.80 PBW: 134.32 PBL: 128.23 *WE Ht: 1415 31.39 1416 Relative Coordinates of Projected Width Mid-point: XADJ: -126.77 YADJ: -71.39 1417 *adjusted for a Stack-Building elevation difference of 1418 0.61 1419 No. of Tiers affecting Stk: 2 1420 Bldg-Tier nos. contributing to MAX: 49 41 1421 1422 Drtcn: 150.00 1423 Stack Ht: 1424 StkNo: 1 Stk Name:STCK1

182.12 *Equation 1 Ht: 1425 GEP: BH: 77.34 PBW: 77.43 192.74 Combined tier MAX: BH: 24.38 PBW: 195.40 PBL: 220.11 *WE Ht: 1426 60.34 1427 Relative Coordinates of Projected Width Mid-point: XADJ: -255.14 YADJ: -46.00 1428 *adjusted for a Stack-Building elevation difference of 1429 0.61 1430 No. of Tiers affecting Stk: 3 Bldg-Tier nos. contributing to MAX: 33 25 41 1431 Stack Ht: StkNo: 2 Stk Name:STCK2 1432 182.12 77.43 GEP: BH: 77.34 PBW: *Equation 1 Ht: 1433 192.74 Combined tier MAX: BH: 24.38 PBW: 152.54 PBL: 152.17 *WE Ht: 1434 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1435 -182.29 YADJ: -68.96 1436 1437 *adjusted for a Stack-Building elevation difference of 0.61 No. of Tiers affecting Stk: 2 1438 Bldg-Tier nos. contributing to MAX: 41 33 1439 Stack Ht: 1440 StkNo: 3 Stk Name:STCK3 182.12 77.43 *Equation 1 Ht: GEP: BH: 77.34 PBW: 1441 192.74 No combined tiers affect this stack for this direction. 1442 1443 1444 Drtcn: 160.00 1445 Stack Ht: 1 Stk Name:STCK1 1446 StkNo: 182.12 *Equation 1 Ht: 1447 GEP: BH: 77.34 PBW: 77.43 192.74 Combined tier MAX: BH: 24.38 PBW: 165.43 PBL: 232.74 *WE Ht: 1448 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1449 -247.96 YADJ: -68.43 1450 *adjusted for a Stack-Building elevation difference of 1451 0.61 No. of Tiers affecting Stk: 3 1452 Bldg-Tier nos. contributing to MAX: 33 25 41 1453 Stack Ht: StkNo: 2 Stk Name:STCK2 1454 182.12 *Equation 1 Ht: 1455 GEP: BH: 77.34 PBW: 77.43 192.74

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PIP\LRS.sup 9/26/2014, 10:16:35 AM No combined tiers affect this stack for this direction. 1456 1457 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1458 192.74 No combined tiers affect this stack for this direction. 1459 1460 1461 Drtcn: 170.00 1462 1463 Stack Ht: StkNo: 1 Stk Name:STCK1 182.12 1464 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction 1465 StkNo: 2 Stk Name:STCK2 Stack Ht: 1466 182.12 1467 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1468 Stack Ht: 1469 StkNo: 3 Stk Name:STCK3 182.12 1470 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1471 No combined tiers affect this stack for this direction. 1472 1473 Drtcn: 180.00 1474 Stack Ht: 1475 StkNo: 1 Stk Name:STCK1 182.12 GEP: BH: 77.34 PBW: 77.43 1476 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction 1477 1478 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1479 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1480 Stack Ht: 1481 StkNo: 3 Stk Name:STCK3 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1482 192.74 No combined tiers affect this stack for this direction. 1483 1484 1485 Drtcn: 190.00 1486 StkNo: 1 Stk Name:STCK1 1487 Stack Ht: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1488 192.74 No combined tiers affect this stack for this direction 1489

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Stack Ht: 1490 StkNo: 2 Stk Name:STCK2 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1491 192.74 No combined tiers affect this stack for this direction. 1492 Stack Ht: 1493 StkNo: 3 Stk Name:STCK3 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1494 192.74 No combined tiers affect this stack for this direction. 1495 1496 Drtcn: 200.00 1497 1498 StkNo: 1 Stk Name:STCK1 Stack Ht: 1499 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1500 192.74 No combined tiers affect this stack for this direction 1501 Stack Ht: 1502 StkNo: 2 Stk Name:STCK2 182.12 GEP: BH: 77.34 PBW: 77.43 1503 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1504 Stack Ht: 1505 StkNo: 3 Stk Name:STCK3 182.12 1506 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1507 1508 1509 Drtcn: 210.00 1510 StkNo: 1 Stk Name:STCK1 Stack Ht: 1511 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1512 192.74 1513 No combined tiers affect this stack for this direction. StkNo: 2 Stk Name:STCK2 Stack Ht: 1514 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 1515 192.74 No combined tiers affect this stack for this direction. 1516 StkNo: 3 Stk Name:STCK3 Stack Ht: 1517 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1518 192.74 Combined tier MAX: BH: 24.38 PBW: 144.64 PBL: 246.96 *WE Ht: 1519 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1520 -0.31 YADJ: -76.72 1521

*adjusted for a Stack-Building elevation difference of 1522 0.61 1523 No. of Tiers affecting Stk: 3 1524 Bldg-Tier nos. contributing to MAX: 33 25 41 1525 1526 Drtcn: 220.00 1527 Stack Ht: 1528 StkNo: 1 Stk Name:STCK1 182.12 1529 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1530 2 Stk Name:STCK2 Stack Ht: 1531 StkNo: 182.12 1532 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1533 1534 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 1535 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 24.38 PBW: 175.39 PBL: 236.79 *WE Ht: 1536 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1537 12.78 YADJ: -52.34 1538 1539 *adjusted for a Stack-Building elevation difference of 0.61 1540 No. of Tiers affecting Stk: 3 Bldg-Tier nos. contributing to MAX: 33 25 41 1541 1542 1543 Drtcn: 230.00 1544 StkNo: 1 Stk Name:STCK1 Stack Ht: 1545 182.12 1546 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1547 No combined tiers affect this stack for this direction. 1548 Stack Ht: StkNo: 2 Stk Name:STCK2 182.12 1549 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 24.38 PBW: 200.80 PBL: 219.43 *WE Ht: 1550 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1551 -31.18 YADJ: -90.14 1552 *adjusted for a Stack-Building elevation difference of 1553 0.61 1554 No. of Tiers affecting Stk: 3

Bldg-Tier nos. contributing to MAX: 33 25 41 1555 StkNo: 3 Stk Name:STCK3 Stack Ht: 1556 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1557 192.74 Combined tier MAX: BH: 24.38 PBW: 141.33 PBL: 165.43 *WE Ht: 1558 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1559 25.49 YADJ: -56.11 1560 *adjusted for a Stack-Building elevation difference of 1561 0.61 No. of Tiers affecting Stk: 2 1562 Bldg-Tier nos. contributing to MAX: 41 33 1563 1564 1565 Drtcn: 240.00 1566 Stack Ht: StkNo: 1 Stk Name:STCK1 1567 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 1568 192.74 No combined tiers affect this stack for this direction. 1569 StkNo: 2 Stk Name:STCK2 Stack Ht: 1570 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 1571 192.74 Combined tier MAX: BH: 24.38 PBW: 220.11 PBL: 195.40 *WE Ht: 1572 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1573 -7.32 YADJ: -72.24 1574 *adjusted for a Stack-Building elevation difference of 1575 0.61 No. of Tiers affecting Stk: 3 1576 Bldg-Tier nos. contributing to MAX: 33 25 41 1577 StkNo: 3 Stk Name:STCK3 Stack Ht: 1578 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1579 192.74 Combined tier MAX: BH: 24.38 PBW: 152.17 PBL: 152.54 *WE Ht: 1580 60.34 1581 Relative Coordinates of Projected Width Mid-point: XADJ: 37.43 YADJ: -33.57 1582 *adjusted for a Stack-Building elevation difference of 1583 0.61 No. of Tiers affecting Stk: 2 1584 Bldg-Tier nos. contributing to MAX: 41 33 1585 1586 1587 Drtcn: 250.00

1588 1589 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 1590 192.74 No combined tiers affect this stack for this direction. 1591 Stack Ht: 1592 StkNo: 2 Stk Name:STCK2 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1593 192.74 Combined tier MAX: BH: 24.38 PBW: 158.39 PBL: 135.03 *WE Ht: 1594 60.34 1595 Relative Coordinates of Projected Width Mid-point: XADJ: 16.77 YADJ: -89.32 1596 *adjusted for a Stack-Building elevation difference of 1597 0.61 No. of Tiers affecting Stk: 2 1598 Bldg-Tier nos. contributing to MAX: 41 33 1599 Stack Ht: 1600 StkNo: 3 Stk Name:STCK3 182.12 1601 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 24.38 PBW: 158.39 PBL: 135.03 *WE Ht: 1602 60.34 1603 Relative Coordinates of Projected Width Mid-point: XADJ: 48.23 YADJ: -10.01 1604 *adjusted for a Stack-Building elevation difference of 1605 0.61 1606 No. of Tiers affecting Stk: 2 1607 Bldg-Tier nos. contributing to MAX: 41 33 1608 1609 Drtcn: 260.00 1610 1611 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 1612 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 24.38 PBW: 238.29 PBL: 130.44 *WE Ht: 1613 Combined tier MAX: BH: 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1614 23.57 YADJ: -114.10 1615 *adjusted for a Stack-Building elevation difference of 1616 0.61 1617 No. of Tiers affecting Stk: 3 Bldg-Tier nos. contributing to MAX: 33 25 41 1618 1619 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12

1620 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 Combined tier MAX: BH: 24.38 PBW: 159.79 PBL: 113.41 *WE Ht: 1621 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1622 40.36 YADJ: -69.71 1623 *adjusted for a Stack-Building elevation difference of 1624 0.61 No. of Tiers affecting Stk: 1625 2 1626 Bldg-Tier nos. contributing to MAX: 41 33 Stack Ht: 1627 StkNo: 3 Stk Name:STCK3 182.12 77.43 *Equation 1 Ht: 1628 GEP: BH: 77.34 PBW: 192.74 12.80 PBW: 92.01 PBL: 140.05 *WE Ht: 1629 Combined tier MAX: BH: 31.39 Relative Coordinates of Projected Width Mid-point: XADJ: 1630 14.96 YADJ: -20.04 1631 *adjusted for a Stack-Building elevation difference of 1632 0.61 No. of Tiers affecting Stk: 2 1633 Bldg-Tier nos. contributing to MAX: 49 41 1634 1635 1636 Drtcn: 270.00 1637 Stack Ht: StkNo: 1 Stk Name:STCK1 1638 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1639 192.74 No combined tiers affect this stack for this direction. 1640 StkNo: 2 Stk Name:STCK2 Stack Ht: 1641 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1642 192.74 1643 No combined tiers affect this stack for this direction. StkNo: 3 Stk Name:STCK3 Stack Ht: 1644 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 1645 192.74 Combined tier MAX: BH: 12.80 PBW: 79.20 PBL: 133.40 *WE Ht: 1646 31.39 Relative Coordinates of Projected Width Mid-point: XADJ: 1647 17.76 YADJ: -1.28 1648 *adjusted for a Stack-Building elevation difference of 1649 0.61 No. of Tiers affecting Stk: 2 1650 Bldg-Tier nos. contributing to MAX: 49 41 1651

1652 1653 Drtcn: 280.00 1654 StkNo: 1 Stk Name:STCK1 1655 Stack Ht: 182.12 1656 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1657 No combined tiers affect this stack for this direction. 1658 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1659 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1660 No combined tiers affect this stack for this direction. 1661 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 1662 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1663 Combined tier MAX: BH: 12.80 PBW: 87.20 PBL: 137.82 *WE Ht: 31.39 1664 Relative Coordinates of Projected Width Mid-point: XADJ: 15.52 YADJ: 17.52 1665 *adjusted for a Stack-Building elevation difference of 1666 0.61 1667 No. of Tiers affecting Stk: 2 1668 Bldg-Tier nos. contributing to MAX: 49 41 1669 Drtcn: 290.00 1670 1671 StkNo: 1 Stk Name:STCK1 Stack Ht: 1672 182.12 1673 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1674 1675 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1676 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1677 No combined tiers affect this stack for this direction. 1678 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 1679 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 192.74 Combined tier MAX: BH: 24.38 PBW: 249.63 PBL: 109.51 *WE Ht: 1680 60.34 1681 Relative Coordinates of Projected Width Mid-point: XADJ: 44.02 YADJ: 111.41 1682 1683 *adjusted for a Stack-Building elevation difference of 0.61

File: P:\AQES\Projects\Basin Electric\Laramie River\400-Technical\Archive\B PIP\LRS.sup 9/26/2014, 10:16:35 AM 1684 No. of Tiers affecting Stk: 3 Bldg-Tier nos. contributing to MAX: 33 25 41 1685 1686 Drtcn: 300.00 1687 1688 Stack Ht: 1689 StkNo: 1 Stk Name:STCK1 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 1690 192.74 No combined tiers affect this stack for this direction. 1691 2 Stk Name:STCK2 Stack Ht: 1692 StkNo: 182.12 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 1693 192.74 Combined tier MAX: BH: 24.38 PBW: 246.96 PBL: 144.64 *WE Ht: 1694 60.34

44.94 YADJ: 48.10 1696 *adjusted for a Stack-Building elevation difference of 1697 0.61 1698 No. of Tiers affecting Stk: 3 Bldg-Tier nos. contributing to MAX: 33 25 41 1699 Stack Ht: StkNo: 3 Stk Name:STCK3 1700 182.12 77.34 PBW: 77.43 *Equation 1 Ht: 1701 GEP: BH: 192.74 PBL: 109.49 *WE Ht: Combined tier MAX: BH: 24.38 PBW: 175.88 1702 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1703 87.62 39.56 YADJ: 1704

Relative Coordinates of Projected Width Mid-point: XADJ:

1705 *adjusted for a Stack-Building elevation difference of 0.61
1706 No. of Tiers affecting Stk: 2
1707 Bldg-Tier nos, contributing to MAX: 41 33

1707 Bldg-Tier nos. contributing to MAX: 41 3 1708

1709 Drtcn: 310.00

1695

1710 1711 StkNo: 1 Stk Name:STCK1 182.12

*Equation 1 Ht: 1712 GEP: BH: 77.34 PBW: 77.43 192.74 No combined tiers affect this stack for this direction. 1713 Stack Ht: StkNo: 2 Stk Name:STCK2 1714 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 1715 192.74 Combined tier MAX: BH: 24.38 PBW: 236.79 PBL: 175.39 *WE Ht: 1716 60.34

Stack Ht:

PIP\LRS.sup 9/26/2014, 10:16:35 AM 1717 Relative Coordinates of Projected Width Mid-point: XADJ: 17.60 YADJ: 64.29 1718 1719 *adjusted for a Stack-Building elevation difference of 0.61 1720 No. of Tiers affecting Stk: 3 1721 Bldg-Tier nos. contributing to MAX: 33 25 41 StkNo: 3 Stk Name:STCK3 Stack Ht: 1722 182.12 1723 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 192.74 Combined tier MAX: BH: 12.80 PBW: 124.04 PBL: 136.98 *WE Ht: 1724 31.39 1725 Relative Coordinates of Projected Width Mid-point: XADJ: 3.05 YADJ: 62.27 1726 1727 *adjusted for a Stack-Building elevation difference of 0.61 No. of Tiers affecting Stk: 2 1728 1729 Bldg-Tier nos. contributing to MAX: 49 41 1730 1731 Drtcn: 320.00 1732 Stack Ht: 1733 StkNo: 1 Stk Name:STCK1 182.12 1734 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1735 No combined tiers affect this stack for this direction. StkNo: 2 Stk Name:STCK2 Stack Ht: 1736 182.12 1737 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1738 Combined tier MAX: BH: 24.38 PBW: 219.43 PBL: 200.80 *WE Ht: 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1739 -10.26 YADJ: 78.53 1740 1741 *adjusted for a Stack-Building elevation difference of 0.61 No. of Tiers affecting Stk: 1742 3 Bldg-Tier nos. contributing to MAX: 33 25 41 1743 1744 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 1745 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 12.80 PBW: 134.32 PBL: 128.23 *WE Ht: 1746 Combined tier MAX: BH: 31.39 1747 Relative Coordinates of Projected Width Mid-point: XADJ: -1.46 YADJ: 71.39 1748

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*adjusted for a Stack-Building elevation difference of 1749 0.61 No. of Tiers affecting Stk: 2 1750 Bldg-Tier nos. contributing to MAX: 49 41 1751 1752 Drtcn: 330.00 1753 1754 StkNo: 1 Stk Name:STCK1 Stack Ht: 1755 182.12 77.34 PBW: 77.43 *Equation 1 Ht: 1756 GEP: BH: 192.74 24.38 PBW: 195.40 PBL: 220.11 *WE Ht: Combined tier MAX: BH: 1757 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1758 35.03 YADJ: 46.00 1759 *adjusted for a Stack-Building elevation difference of 1760 0.61 1761 No. of Tiers affecting Stk: 3 Bldg-Tier nos. contributing to MAX: 33 25 41 1762 Stack Ht: 1763 StkNo: 2 Stk Name:STCK2 182.12 *Equation 1 Ht: GEP: BH: 77.34 PBW: 77.43 1764 192.74 24.38 PBW: 152.54 PBL: 152.17 *WE Ht: Combined tier MAX: BH: 1765 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1766 30.12 YADJ: 68.96 1767 *adjusted for a Stack-Building elevation difference of 1768 0.61 No. of Tiers affecting Stk: 2 1769 33 Bldg-Tier nos. contributing to MAX: 41 1770 Stack Ht: StkNo: 3 Stk Name:STCK3 1771 182.12 *Equation 1 Ht: 1772 GEP: BH: 77.34 PBW: 77.43 192.74 No combined tiers affect this stack for this direction. 1773 1774 1775 Drtcn: 340.00 1776 1 Stk Name:STCK1 Stack Ht: 1777 StkNo: 182.12 *Equation 1 Ht: 77.43 GEP: BH: 77.34 PBW: 1778 192.74 24.38 PBW: 165.43 PBL: 232.74 *WE Ht: Combined tier MAX: BH: 1779 60.34 Relative Coordinates of Projected Width Mid-point: XADJ: 1780 15.22 YADJ: 68.43 1781

1782 *adjusted for a Stack-Building elevation difference of 0.61 No. of Tiers affecting Stk: 3 1783 Bldg-Tier nos. contributing to MAX: 33 25 41 1784 1785 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1786 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1787 No combined tiers affect this stack for this direction. 1788 StkNo: 3 Stk Name:STCK3 Stack Ht: 182.12 1789 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1790 No combined tiers affect this stack for this direction. 1791 1792 Drtcn: 350.00 1793 1794 StkNo: 1 Stk Name:STCK1 Stack Ht: 182.12 1795 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 1796 No combined tiers affect this stack for this direction 1797 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1798 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1799 StkNo: 3 Stk Name:STCK3 1800 Stack Ht: 182.12 *Equation 1 Ht: 1801 GEP: BH: 77.34 PBW: 77.43 192.74 1802 No combined tiers affect this stack for this direction. 1803 1804 Drtcn: 360.00 1805 1806 Stack Ht: StkNo: 1 Stk Name:STCK1 182.12 1807 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction 1808 1809 StkNo: 2 Stk Name:STCK2 Stack Ht: 182.12 1810 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1811 1812 3 Stk Name:STCK3 Stack Ht: StkNo: 182.12 1813 GEP: BH: 77.34 PBW: 77.43 *Equation 1 Ht: 192.74 No combined tiers affect this stack for this direction. 1814